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New Synthesis Methods for Subambient Processes such as LNG

by

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Motivation (1)

Characteristics of Subambient Processes

- External Cooling provided by **Refrigeration** \Rightarrow Power
- Pressure and Fluid Phase are important Design Variables (pressurized streams have cooling "stored")
- Single Component Refrigerants evaporate at constant Temperature, resulting in large Exergy Losses
- Multicomponent Refrigerants provide gliding Temperatures with reduced Exergy Losses, but they also introduce two-phase Flow Distribution Problems
- ♦ Extremely tight Driving Forces in Heat Exchangers ⇒ Rigorous Simulation and Advanced Thermo Packages

Motivation (2)

LNG – The fastest growing Energy Carrier

- Our "Test Site" for new Methodologies while trying to develop new Innovative Process Concepts
- From large Scale Base Load to smaller Scale Plants
- Floating LNG investigated by several Companies
- Natural Gas Liquefaction is a mature Process, but there may still be some Scope for Improvements:
 - Thermodynamic Minimum: ≈ 115 kWh/tonne LNG
 - Snøhvit MFC[®]LNG Process¹: 234 kWh/tonne LNG
 - Niche with precooling²: ≈ 270 kWh/tonne LNG
 - Dual N2 process (BHP)²: ≈ 350 kWh/tonne LNG
 - ¹ Roy Scott Heiersted. Presentation at NTNU Alumni, June 2007

² Knut Arild Maråk, "Gas Phase Cycles for Liquefaction of Natural Gas – Status and Outlook", Trial Lecture, NTNU, 11 June 2009

Motivation (3)

Limitations in existing Design Methodologies

Pinch Analysis has been extensively and successfully applied in a broad Variety of Industries for > 25 years



• **Exergy** Considerations have been included

- But: Only **Temperature** is used as Design variable
 - **Pressure**, Composition and Fluid **Phase** <u>not</u> considered

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Background: Liquefied Energy Chain



Key Features of the "LEC" Concept

- Utilization of **Stranded** Natural Gas for Power Production
- Elegant and Cost Effective solution to the **CCS** Problem
- CO₂ replaces Natural Gas injection for EOR
- **Combined** Energy Chain (LNG) and Transport Chain (CO₂)

Need for Design Methods identified

The Offshore Process was Designed by

- Trial & Error
- Thermodynamic Insight
- Process Knowledge (LNG)
- Rigorous Steady-State Simulation

The Design Process resulted in Insight

- Set of 10 Heuristic Rules were developed for
 - Pressure Manipulations
 - Fluid Phase Considerations
 - Design Actions in General

No Systematic Design Method available

Must Consider Pressure and Fluid Phase

Extended Problem Definition for Heat Recovery Systems





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"Given a set of Process Streams with a Supply State (Temperature, **Pressure** and the resulting **Phase**) and a Target State, as well as Utilities for **Power**, Heating and Cooling; Design a System of Heat Exchangers, *Expanders*, *Pumps* and **Compressors** such that the **Irreversibilities** (or a **Cost** related **Objective Function such as Total Annualized Cost) is minimized**"

The "Path" from Supply to Target State is <u>not</u> fixed

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Expanding a pressurized Cold Stream

Given a "Cold" Stream with $T_s = -120^{\circ}C$, $T_t = 0^{\circ}C$, $p_s = 5$ bar, $p_t = 1$ bar

Basic PA and the 2 "extreme" Cases are given below:



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Composite Curves can be manipulated

Given a pressurized Cold Stream

• $T_s = -120^{\circ}$ C, $T_t = 0^{\circ}$ C, $p_s = 5$ bar, $p_t = 1$ bar

Attainable Region for 1 Stream



Appropriate Placement Concept of PA revisited for Compressors and Expanders

Appropriate Placement (Integration) established for

- Chemical Reactors, Distillation Columns and Evaporators
- Heat Engines, Heat Pumps and Refrigeration Cycles

In the "Stand-Alone" Case

- **Compressors** should operate at **low** Temperature possibly with interstage Coolers to reduce Power Requirements
- **Expanders** should operate at **high** Temperature, possibly with reheat to increase Power Production

As Part of a Heat Recovery Problem

- Compressors provide additional Heat and should be placed above the Pinch Temperature (where there is Heat Deficit)
- Expanders provide additional Cooling and should be placed below the Pinch Temperature (where there is Heat Surplus)

Appropriate Placement of Compressors A very simple "Experimental Setup"

Example 1

- One Hot, two Cold Streams, H1 to be compressed
- Key Q: What is the Optimal Compressor inlet Temperature?
- Objective: Maximize **Exergy** Efficiency

Example 2

- Two Hot, two Cold Streams, H2 to be compressed
- Key Q: Effect of $T_{\text{comp,in}}$ on the Process **Pinch**?
- Assuming Ideal Gases and Isentropic Expansion

$$Compressor: \quad \frac{T_2}{T_1} = \left(\frac{p_2}{p_1}\right)^{\frac{k-1}{k}}$$
$$\Delta \dot{E}_x = \dot{m} \cdot c_p \cdot \left(T_t - T_s - T_0 \cdot \ln \frac{T_t}{T_s}\right) + \dot{m} \cdot c_p \cdot \frac{k-1}{k} \cdot T_0 \cdot \ln \frac{p_t}{p_s}$$

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Key Information for Example 1

Table 1 Stream Data for Example 1

Stream	$T_{s}(^{\circ}C)$	T_t (°C)	$\dot{m} \cdot c_p \; (kW/^{\circ}C)$	\dot{Q} (kW)	p_s (bar)	p_t (bar)
H1	130	-75	2.0	410	1.0	2.0
C1	15	140	5.0	625	-	-
C2	-50	140	1.0	190	-	-
LP	150	150	-	-	-	-
R	-85	-85	-	-	-	-

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Traditional Targeting

- $\Delta T_{\text{min}} = 10^{\circ}\text{C}$, $T_{\text{Pinch}} = 25^{\circ}\text{C}/15^{\circ}\text{C}$
- $Q_{\rm H,min} = 540 \, \rm kW$, $Q_{\rm C,min} = 135 \, \rm kW$
- Parameter Values (also for Example 2)
 - $c_{\rm p} = 1.0 \text{ kJ/kg}^{\circ}\text{C}$, $k = c_{\rm p} / c_{\rm v} = 1.4$, $T_0 = 298 \text{ K}$
- Variation of Compressor inlet Temperature
 - $T_{\text{comp,in}}$ from -75°C to +125°C

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Calculation Results for Example 1



Regions for Compressor inlet Temperature

- ◆ From -75°C to -28.5°C: Compression entirely **below** Pinch
- From -28.5°C to +25°C: Compression moves gradually into the above Pinch Region
- ♦ From +25°C to +125°C: Compression entirely above Pinch

Appropriate Placement is exactly at the Pinch

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Key Information for Example 2

Table 2 Stream Data for Example 2

Stream	$T_s(^{\circ}C)$	T_t (°C)	$\dot{m} \cdot c_p \; (kW/^{\circ}C)$	\dot{Q} (kW)	p_s (bar)	p_t (bar)
H1	50	-160	1.5	315	-	-
H2	0	-120	2.5	300	1.0	2.0
C1	-180	-20	2.0	320	-	-
C2	-60	30	4.0	360	-	-

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No Utility Data provided

- Focus is on Pinch Changes
- No Exergy Calculations

Traditional Targeting

• $\Delta T_{\text{min}} = 10^{\circ}\text{C}$, $T_{\text{Pinch}} = -50^{\circ}\text{C}/-60^{\circ}\text{C}$

•
$$Q_{\rm H,min} = 165 \text{ kW}$$
, $Q_{\rm C,min} = 100 \text{ kW}$

- Variation of Compressor inlet Temperature
 - $T_{\text{comp,in}}$ from -120°C to 0°C

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Calculation Results for Example 2



Regions for Compressor inlet Temperature

- ◆ From -120°C to -90.1°C: Compression entirely **below** Pinch
- For Compressor inlet at -90.1°C, the outlet is -50°C (Pinch)
- From -90.1°C to about -60°C: Pinch follows Compressor outlet Temperature until it reaches 0°C, when the Supply Temperature of H2 (also 0°C) takes over as Pinch
- At $T_{\text{comp,in}}$ of about -32°C Pinch jumps back to -50°C/-60°C

Compressor affects Pinch Temperature



Appropriate Placement vs. a moving Pinch ??

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Compressor affects Composite Curves



Insights obtained from the Examples

From Example 1

- Appropriate Placement of a Compressor is "at the Pinch", meaning Compressor inlet Temperature at the Pinch Temperature, thus delivering Heat <u>above</u> Pinch
- Similar (opposite) Conclusions can be made for **Expanders**

From Example 2

- With multiple Streams some of which are subject to Pressure Changes, Stream Data will be Floating, not fixed
- The Pinch (constantly changing) becomes less important, and it is impossible to refer to Appropriate Placement of Compressors and Expanders relative to a moving Pinch

The true Value of the new Insight

 A new Superstructure can be developed for Heat Recovery Problems where Compression and Expansions is included

Superstructure for the Extended Heat Recovery Problem



Consider a Hot Stream

- If the Supply Temperature is above Pinch, it should be cooled to Pinch or Target Temperature (if above Pinch)
- If/when the Stream is at Pinch it should be compressed according to the new Insight (outlet Pressure free)
- Next, it should be cooled to Pinch, where the next Option according to the new Insight is to expand the Stream (outlet Pressure free)
- The Stream should then be heated to Pinch or the Target Temperature
- A 2nd and final compression can be considered before cooling the Hot Stream to Target Temperature

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Application of the new Superstructure: A novel Offshore LNG Process



Resulting Composite Curves



The Nitrogen "Path" Offshore



Concluding Remarks

- Subambient Processes have special Characteristics that require new Design Methodologies where Pressure and Fluid Phase are considered important Design Variables
- In Subambient Processes, external Cooling is provided by Compression and Expansion (Refrigeration Cycles)
- Not a big Surprise then that Compression and Expansion of
 Process Streams reduce the Need for Refrigeration
- With Compressors & Expanders, Stream Data becomes
 Floating, and the Pinch Concept as well as the Appropriate
 Placement of Compressors & Expanders are less useful
- A new Superstructure for simultaneous Heating, Cooling, Compression and Expansion has been developed
- This new Superstructure has been successfully applied to design an Offshore Natural Gas Liquefaction Process

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Opportunities for using Optimization

Many challenging Tasks

- **Structural** Design of Single Process of a Production Chain
- Optimizing **Operating** Variables in entire Production Chains
- Optimization of Mixed Refrigerants Composition

Mathematical Programming ("deterministic")

- Strength in **Synthesis** if a clever Superstructure is available
- Suffers from Combinatorial Explosion (binary variables) and Local Optima (non-Linearities are often non-Convex)

Stochastic Algorithms ("non-deterministic")

- Examples are many: Simulated Annealing, Genetic Algorithms, Evolutionary Search, Tabu Search, etc.
- Can be **combined** with rigorous Process Simulation
- Successfully applied for **Mixed Refrigerant** Optimization