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*Non-uniformly coarsened grid models and a mixed multiscale FEM for reservoir simulation on a geological scale.*

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# Motivation

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We have seen (in earlier talks) that the Mixed Multiscale FEM (MMsFEM) is a robust alternative to upscaling, and has the potential for large geomodels.

*Why use the MMsFEM with non-uniform coarsened grids?*

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*Why use the MMsFEM with non-uniform coarsened grids?*

- Motivated from the non-uniform coarsening approach in upscaling.
- Potential of reducing the number of grid blocks needed to obtain satisfactory solutions (increased speed).
- The MMsFEM handles arbitrary gridblocks  $\Rightarrow$  (almost) no limitation on grids.

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# Outline of talk:

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- Introduction.

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- Discussion on criteria for refining/coarsening grids.
- Numerical experiments.
- Conclusion / further work.

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# Model equations

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Elliptic pressure equation:

$$v = -\lambda(S)K\nabla p$$

$$\nabla \cdot v = q$$

Hyperbolic saturation equation:

$$\phi \frac{\partial S}{\partial t} + \nabla \cdot (vf(S)) = q_w$$

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$$\nabla \cdot v = q$$

Hyperbolic saturation equation:

$$\phi \frac{\partial S}{\partial t} + \nabla \cdot (vf(S)) = q_w$$

• Total velocity:

$$v = v_o + v_w$$

• Total mobility:

$$\begin{aligned}\lambda &= \lambda_w(S) + \lambda_o(S) \\ &= k_{rw}(S)/\mu_w + k_{ro}(S)/\mu_o\end{aligned}$$

• Saturation water:  $S$

• Fractional flow water:

$$f(S) = \lambda_w(S)/\lambda(S)$$

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## Mixed formulation of the pressure equation:

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Find  $(v, p) \in H_0^{1,\text{div}} \times L^2$  such that

$$\int (\lambda K)^{-1} u \cdot v dx - \int p \nabla \cdot v dx = 0, \quad \forall u \in H_0^{1,\text{div}},$$
$$\int l \nabla \cdot v dx = \int q l dx, \quad \forall l \in L^2.$$

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**Multiscale discretisation:** Seek solutions in low-dimensional subspaces

$$U^{ms} \subset H_0^{1,\text{div}} \text{ and } V \in L^2,$$

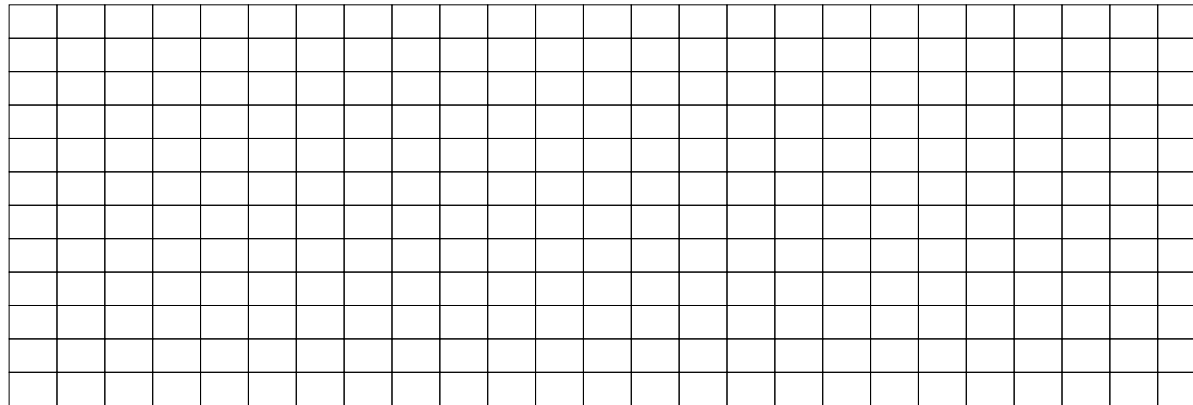
where local fine scale properties are incorporated into the basis functions.

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# Grids and basis functions

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We assume we are given a *fine* grid with permeability and porosity attached to each fine grid block.

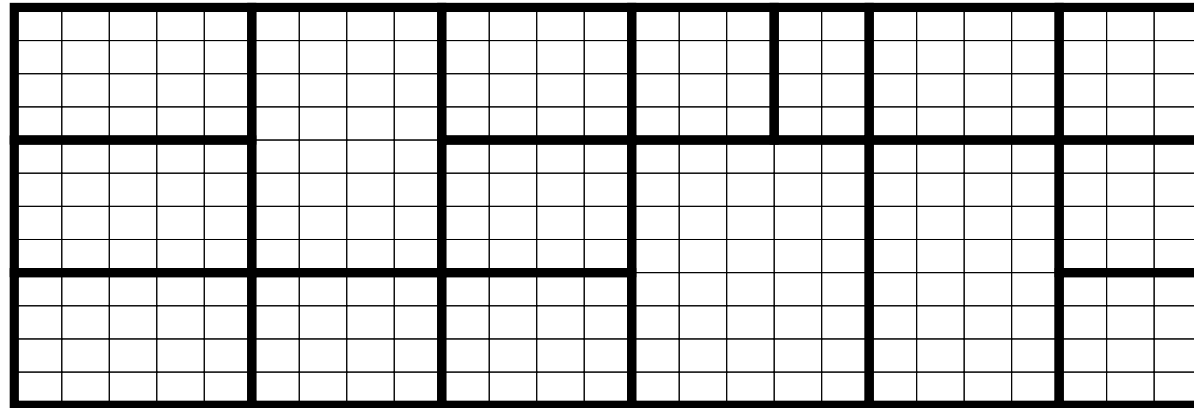


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We construct a *coarse* grid, and choose the discretisation spaces  $V$  and  $U^{ms}$  such that:

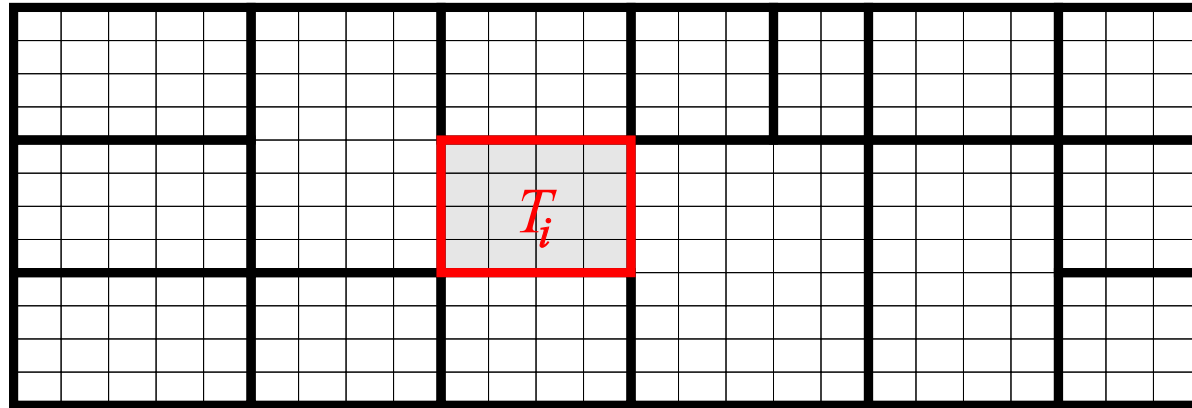


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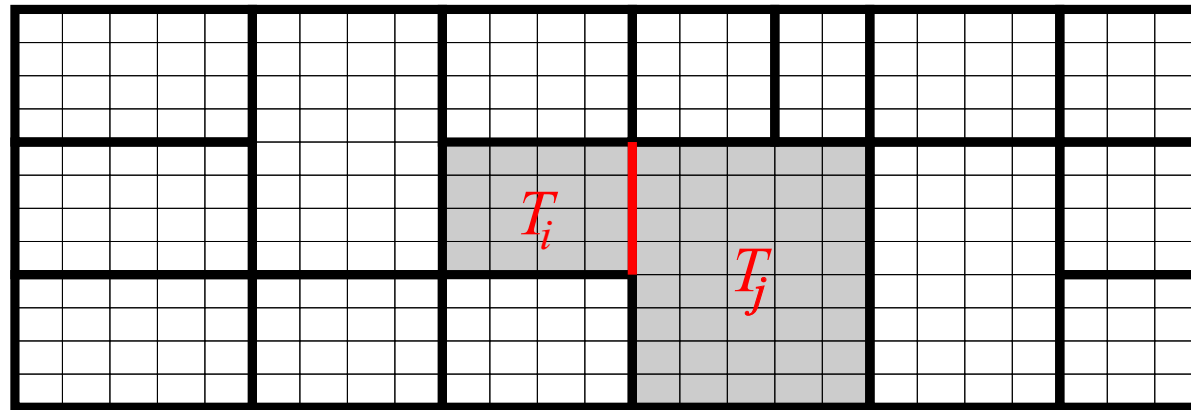


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We construct a *coarse* grid, and choose the discretisation spaces  $V$  and  $U^{ms}$  such that:

- For each coarse block  $T_i$ , there is a basis function  $\phi_i \in V$ .
- For each coarse edge  $\Gamma_{ij}$ , there is a basis function  $\psi_{ij} \in U^{ms}$ .

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## Basis functions for the velocity field

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For each coarse edge  $\Gamma_{ij}$  define a basis function

$$\psi_{ij} : T_i \cup T_j \rightarrow R^2$$

with unit flux through  $\Gamma_{ij}$ , and no flow across  $\partial(T_i \cup T_j)$ .

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with unit flux through  $\Gamma_{ij}$ , and no flow across  $\partial(T_i \cup T_j)$ .  
We use  $\psi_{ij} = -\lambda K \nabla \phi_{ij}$  with

$$\nabla \cdot \psi_{ij} = \begin{cases} f_i(x) / \int_{T_i} f_i(x) dx & \text{for } x \in T_i, \\ -f_j(x) / \int_{T_j} f_j(x) dx & \text{for } x \in T_j, \\ 0 & \text{otherwise,} \end{cases}$$

with BCs  $\psi_{ij} \cdot n = 0$  on  $\partial(T_i \cup T_j)$ .

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## Basis functions for the velocity field cont.

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If  $\int_{T_i} q dx \neq 0$  ( $T_i$  contains a source), then

$$f_i(x) = q(x).$$

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## Basis functions for the velocity field cont.

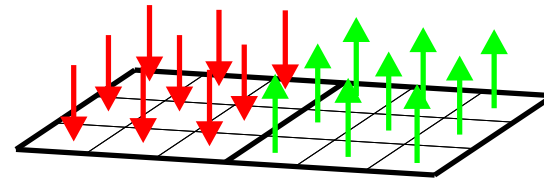
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If  $\int_{T_i} q dx \neq 0$  ( $T_i$  contains a source), then

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Otherwise we may choose

$$f_i(x) = 1,$$



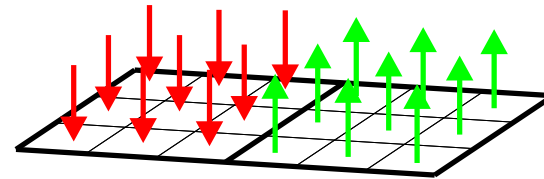
## Basis functions for the velocity field cont.

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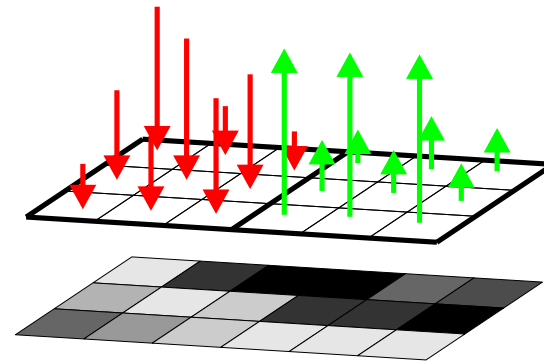
Otherwise we may choose

$$f_i(x) = 1,$$



or to avoid high flow through low-perm regions

$$f_i(x) = (\det(K(x)))^{\frac{1}{d}}.$$



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## Non uniform grids - for upscaling and the MMsFEM

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- In the non-uniform coarsening approach for upscaling, the domain is modelled in greater detail in regions of potential high velocity.



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- **However:** the MMsFEM can represent such regions correctly even on a very coarse scale.

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## Non uniform grids - for upscaling and the MMsFEM

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- In the non-uniform coarsening approach for upscaling, the domain is modelled in greater detail in regions of potential high velocity.
- **However:** the MMsFEM can represent such regions correctly even on a very coarse scale.
- Why bother refining?

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# When is refinement required?

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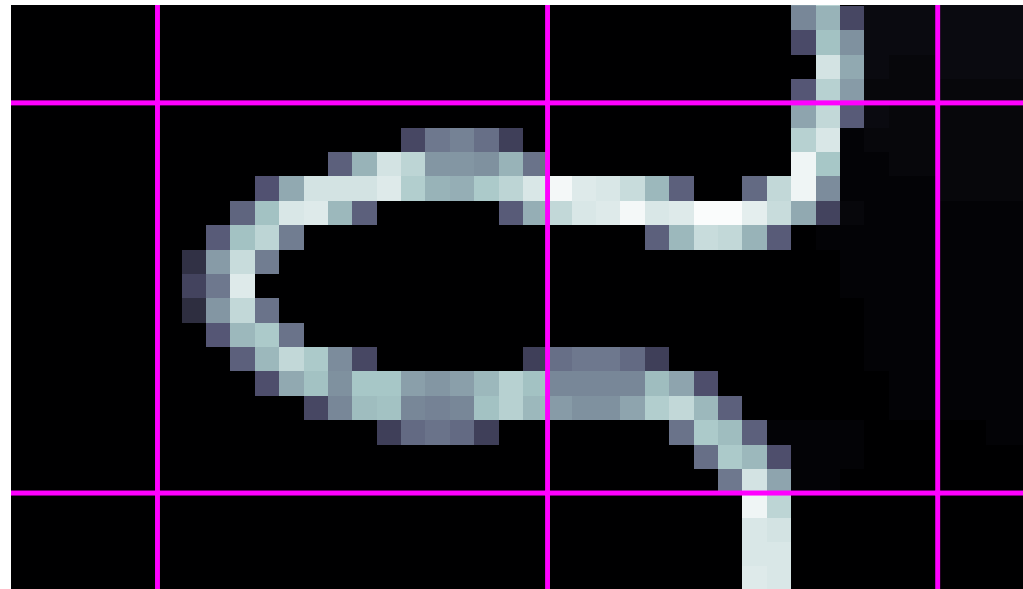
***Case 1: Non uniform direction of flux across coarse edges.***

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# When is refinement required?

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**Case 1: Non uniform direction of flux across coarse edges.**  
Consider the following fine grid velocity field:

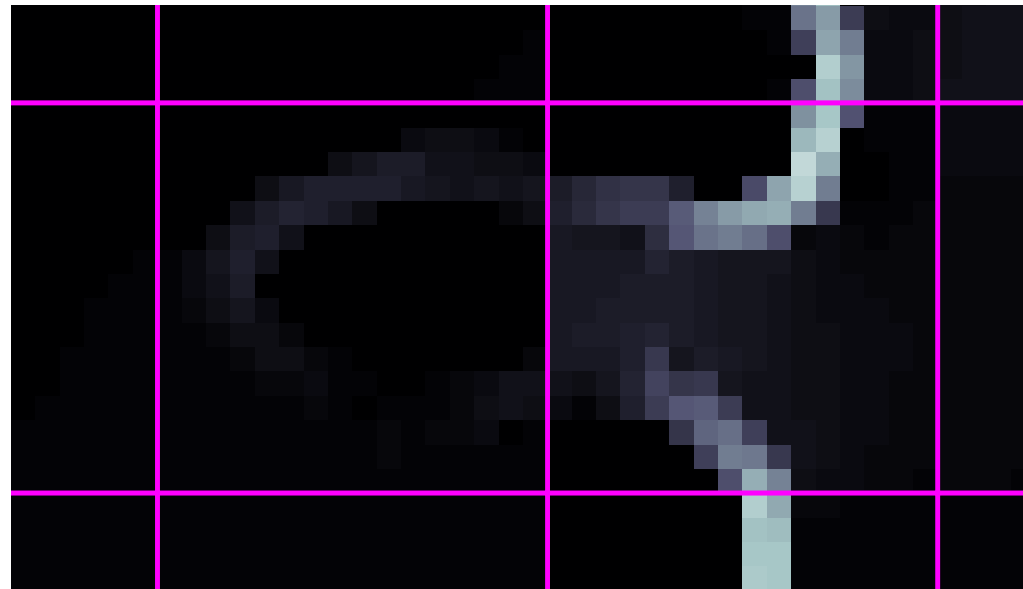


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# When is refinement required?

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**Case 1: Non uniform direction of flux across coarse edges.**  
Solving on the coarse grid, we obtain

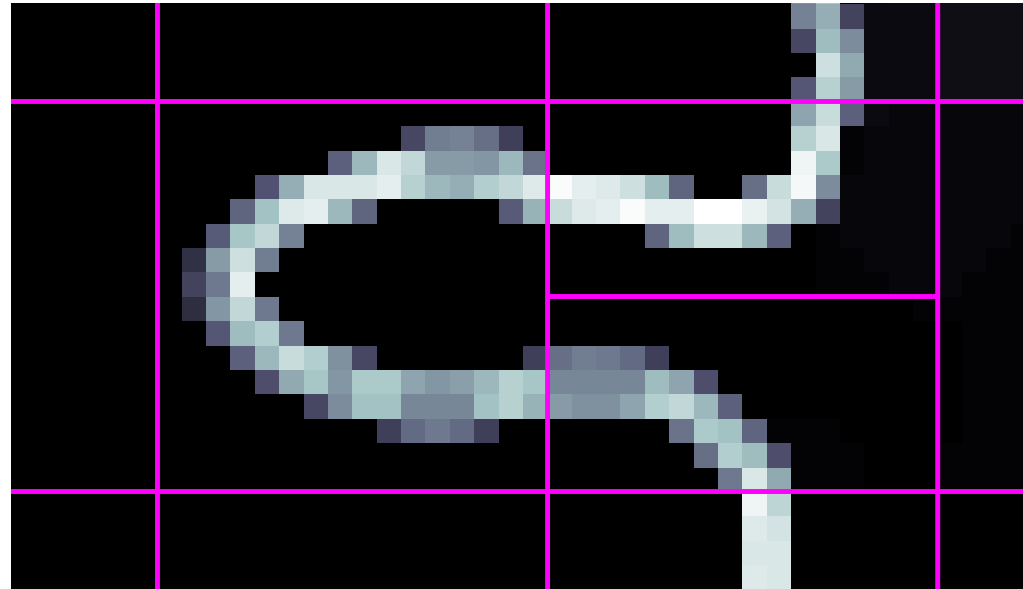


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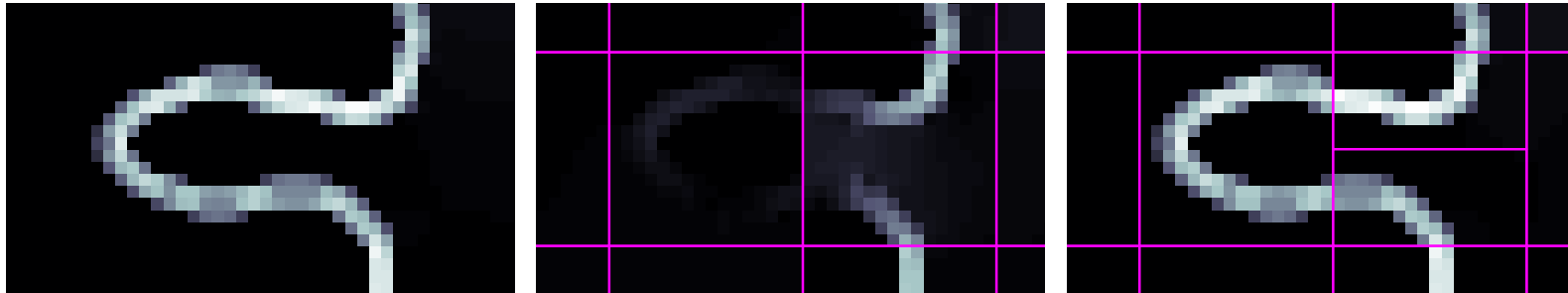
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**Case 1: Non uniform direction of flux across coarse edges.**  
After a local refinement , we obtain



# When is refinement required?

## Case 1: Non uniform direction of flux across coarse edges.



**Criteria:** Given an initial fine grid velocity field  $v_0$ , we modify the coarse grid such that

$$\frac{\int_{\Gamma} |v_0 \cdot n| ds}{\left| \int_{\Gamma} (v_0 \cdot n) ds \right|}$$

is close to 1 for every coarse edge  $\Gamma$ .

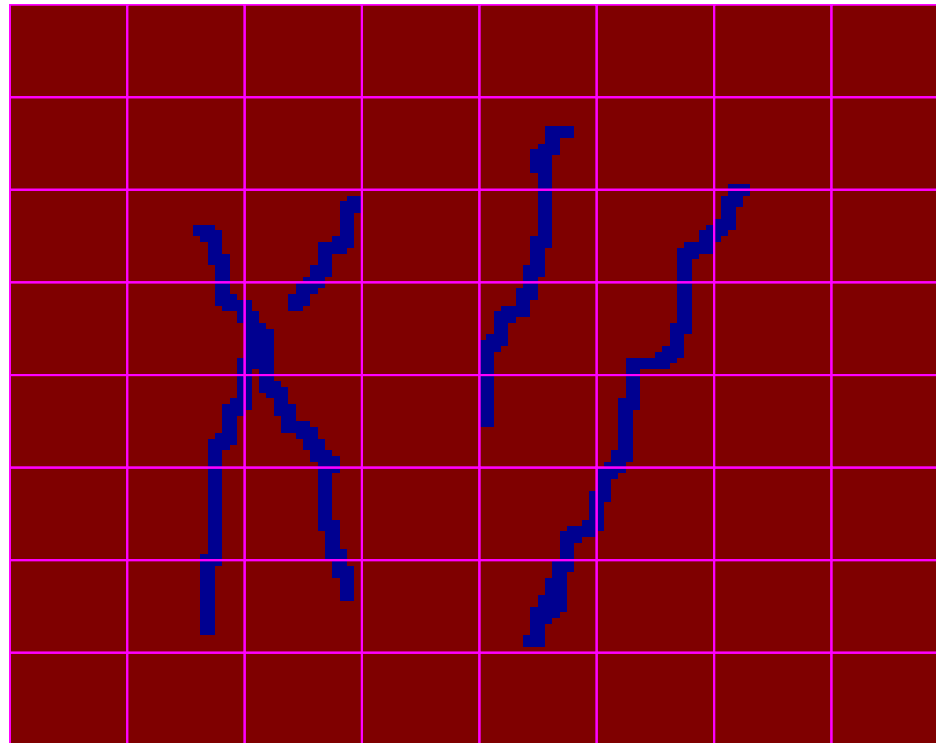
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## When is refinement required?

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### **Case2: Flow of basis functions is forced through barriers.**

Consider the following permeability field with everywhere  $K = 1$ , except barriers (blue) with  $K = 10^{-10}$ .

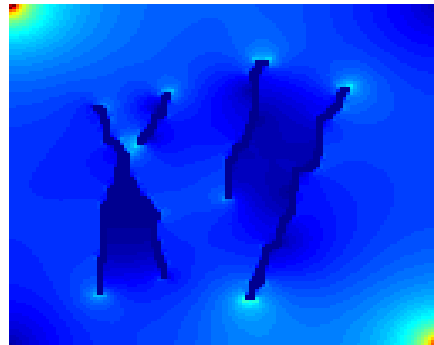




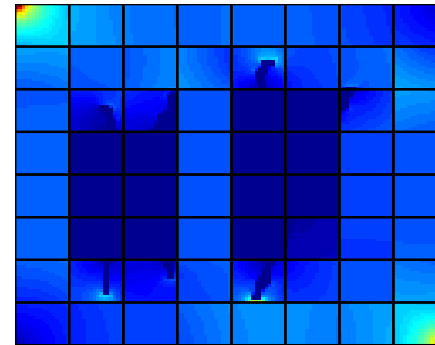
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**Case2: Flow of basis functions is forced through barriers.**  
With the MMsFEM on the coarse grid we obtain the following velocity fields:

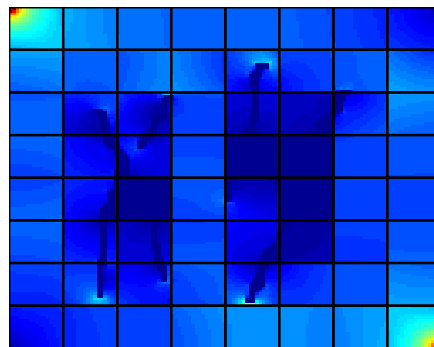
Fine grid



Coarse – constant source



Coarse – varying source



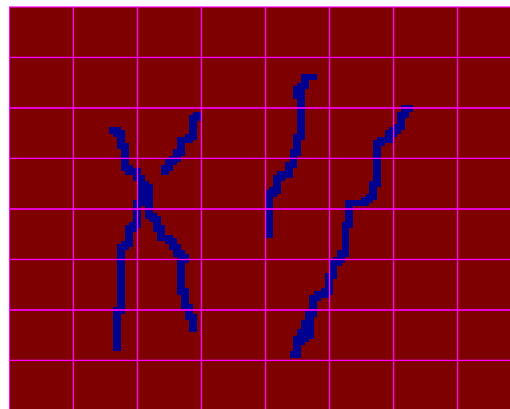
# When is refinement required?

**Case2: Flow of basis functions is forced through barriers.**

**Criteria for refinement:** For every basis function  $\psi_{ij}$  we monitor

$$\psi_{ij}^T K^{-1} \psi_{ij}.$$

If for some  $x \in T_i$ , say,  $\psi_{ij}(x)K(x)^{-1}\psi_{ij}(x)$  achieves an *unnatural* high value, then  $\psi_{ij}(x)$  is trashed and  $T_i$  is split in two new blocks.





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## When is refinement required?

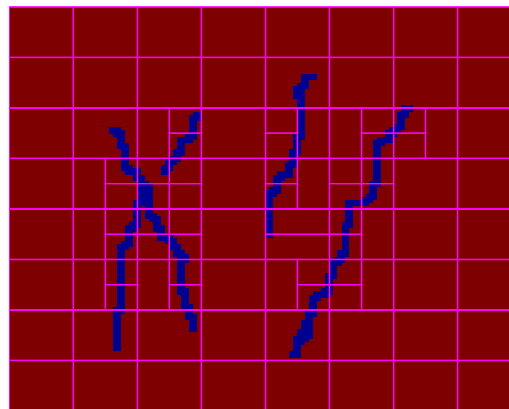
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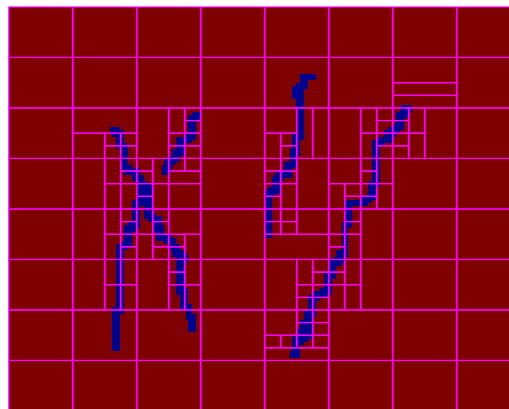
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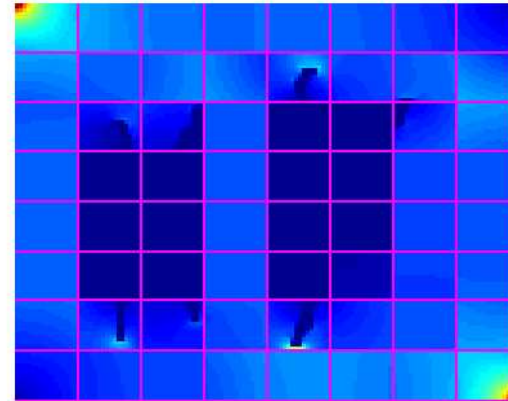
# When is refinement required?

**Case2: Flow of basis functions is forced through barriers.**  
Velocity fields for all four cases:

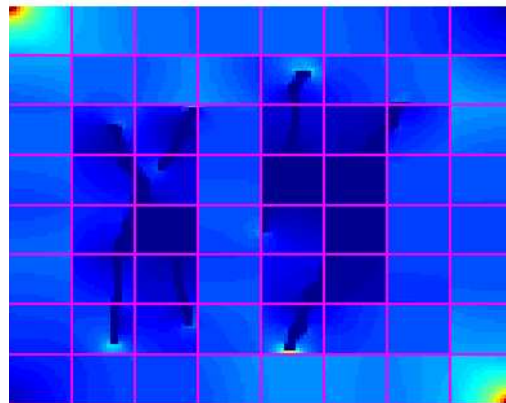
Fine grid



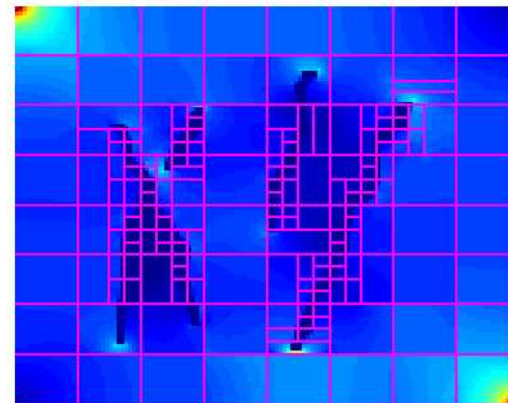
Coarse - constant source



Coarse - varying source



Non-uniform grid



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## Remarks

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The first refinement criterion is based on a global velocity field, while the second on local properties of the permeability field.

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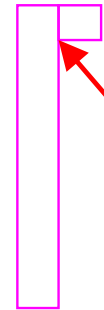
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### *Regularization*

- Long/thin grid blocks might give rise to nonphysical flow.



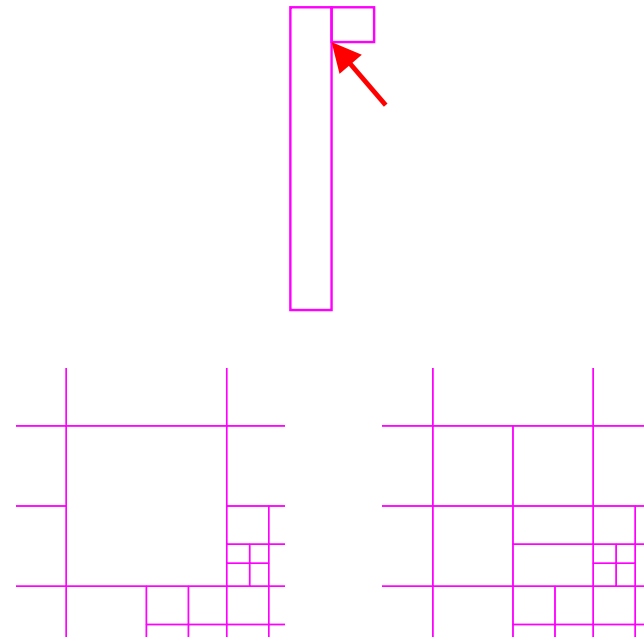


# Remarks

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## *Regularization*

- Long/thin grid blocks might give rise to nonphysical flow.
- The number of edges associated with each grid block determines the sparsity pattern of the discretization matrix.



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## Numerical experiments-grid construction

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- An initial fine grid (single phase) velocity field  $v_0$  is computed on the fine grid.

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- For any coarse edge  $\Gamma$  if

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then one of the neighboring (randomly chosen) blocks are split.

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then one of the neighboring (randomly chosen) blocks are split.

- Further splitting is performed according to

$$\psi^T K^{-1} \psi > \text{condition}$$

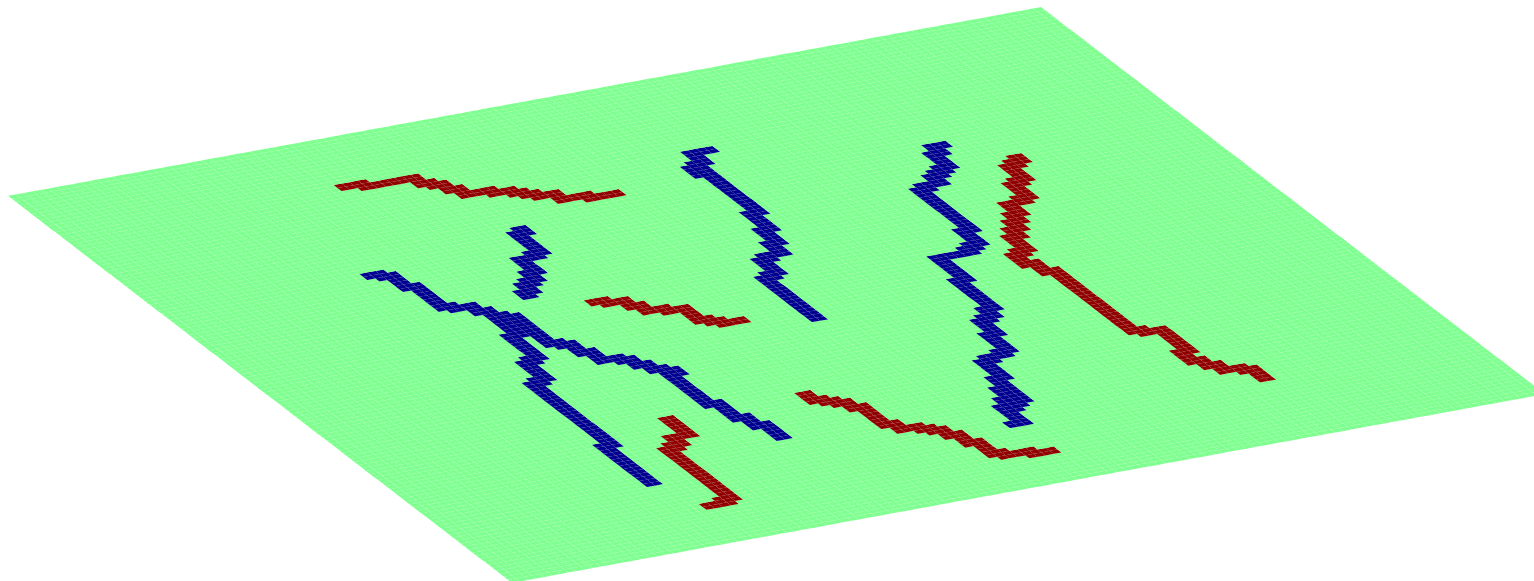
# Numerical experiments 1

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*A model problem with barriers/ high permeability channels*

The fine scale ( $128 \times 128$ ) permeability field consists of

- channels:  $K = 10^4$ ,
- barriers:  $K = 10^{-4}$ ,
- everywhere else  $K = 1$ .



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## Numerical experiments 1, cont.

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The simulation is run with unit mobility  $\lambda = 1 \Rightarrow f(S) = S$  (the velocity is computed only once).

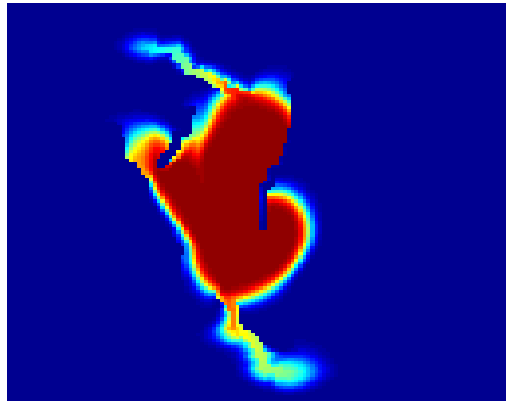
We apply four different grids:

- Fine grid,  $128 \times 128$  blocks.
- Coarse grid,  $8 \times 8$ .
- Finer coarse grid,  $32 \times 32$
- Non-uniform grid, 230 blocks.

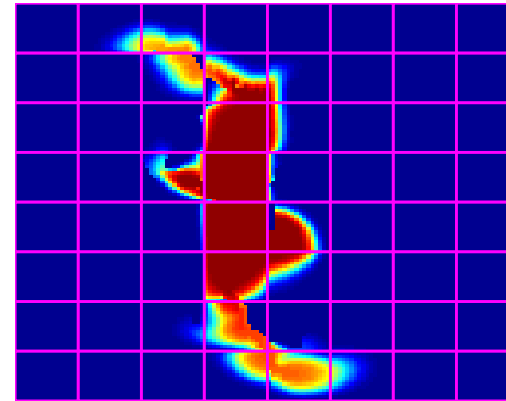
# Numerical experiments 1, cont.

Saturation profiles at  $t = 0.12$ .

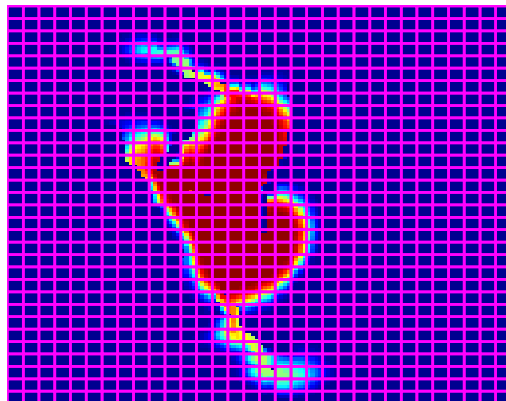
Fine grid



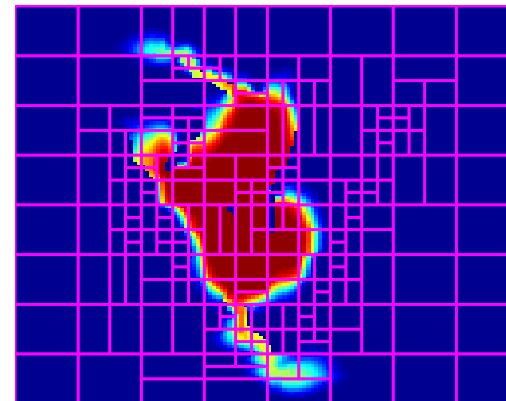
Initial coarse grid



Finer coarse grid



Non-uniform grid

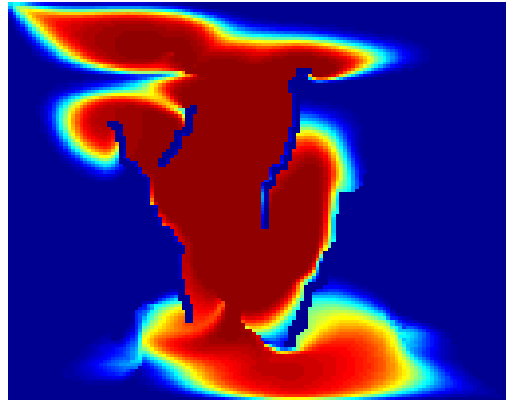




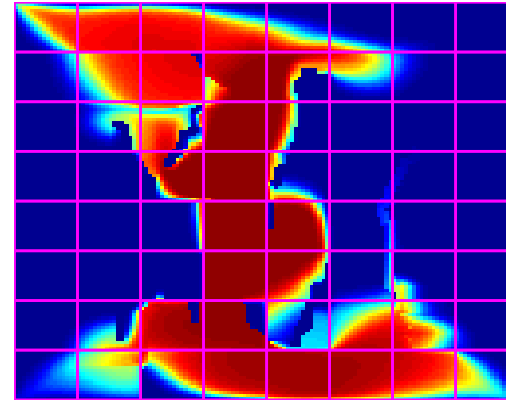
# Numerical experiments 1, cont.

Saturation profiles at  $t = 0.36$ .

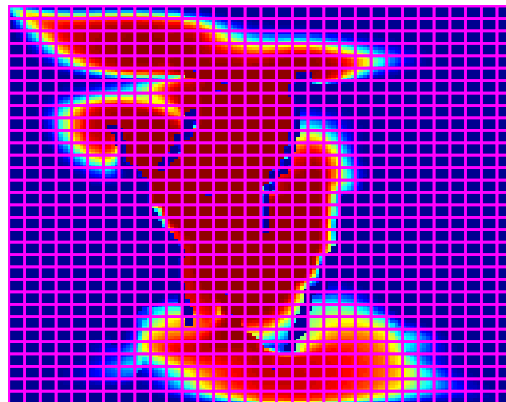
Fine grid



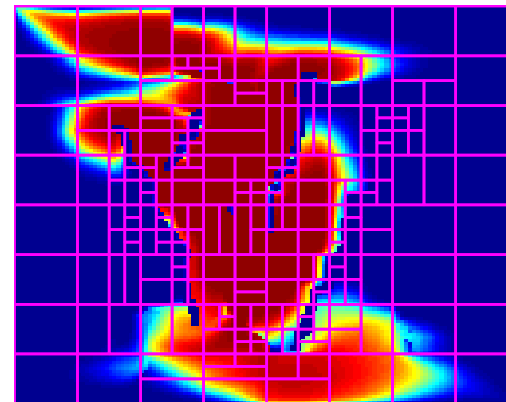
Initial coarse grid



Finer coarse grid



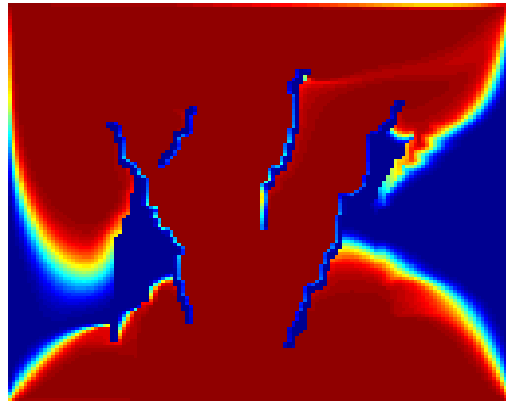
Non-uniform grid



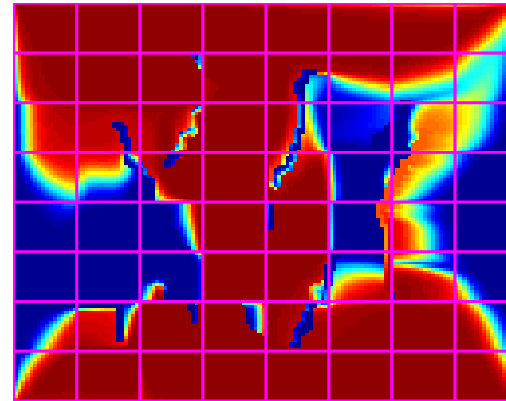
# Numerical experiments 1, cont.

Saturation profiles at  $t = 1.2$ .

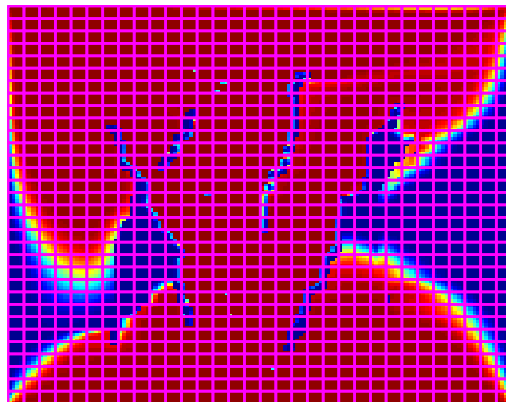
Fine grid



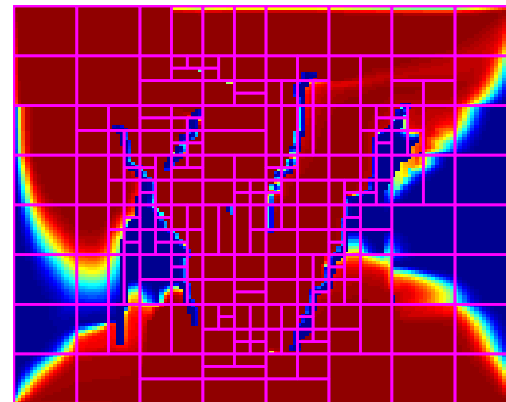
Initial coarse grid



Finer coarse grid

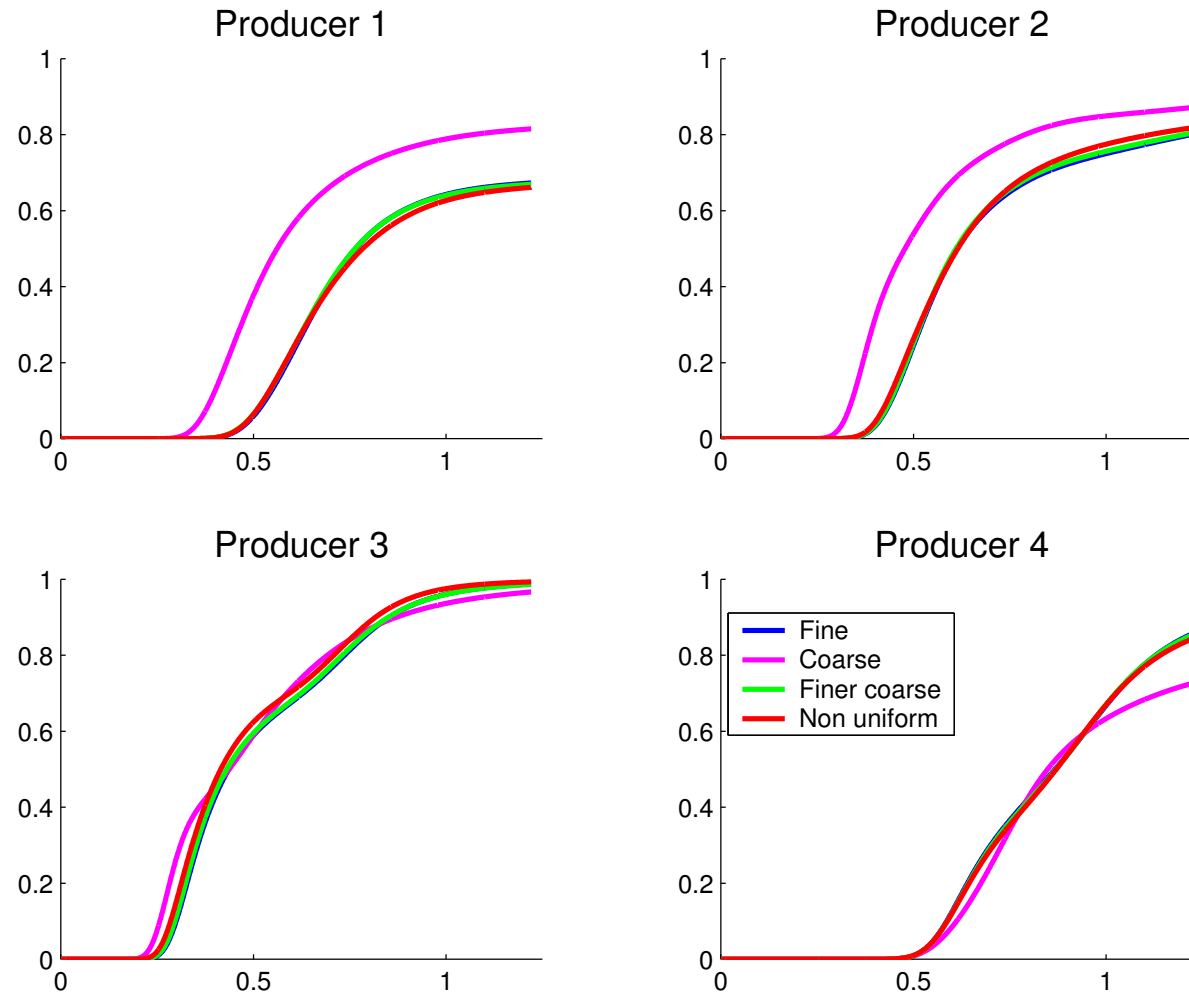


Non-uniform grid



# Numerical experiments 1, cont.

Water cut curves:



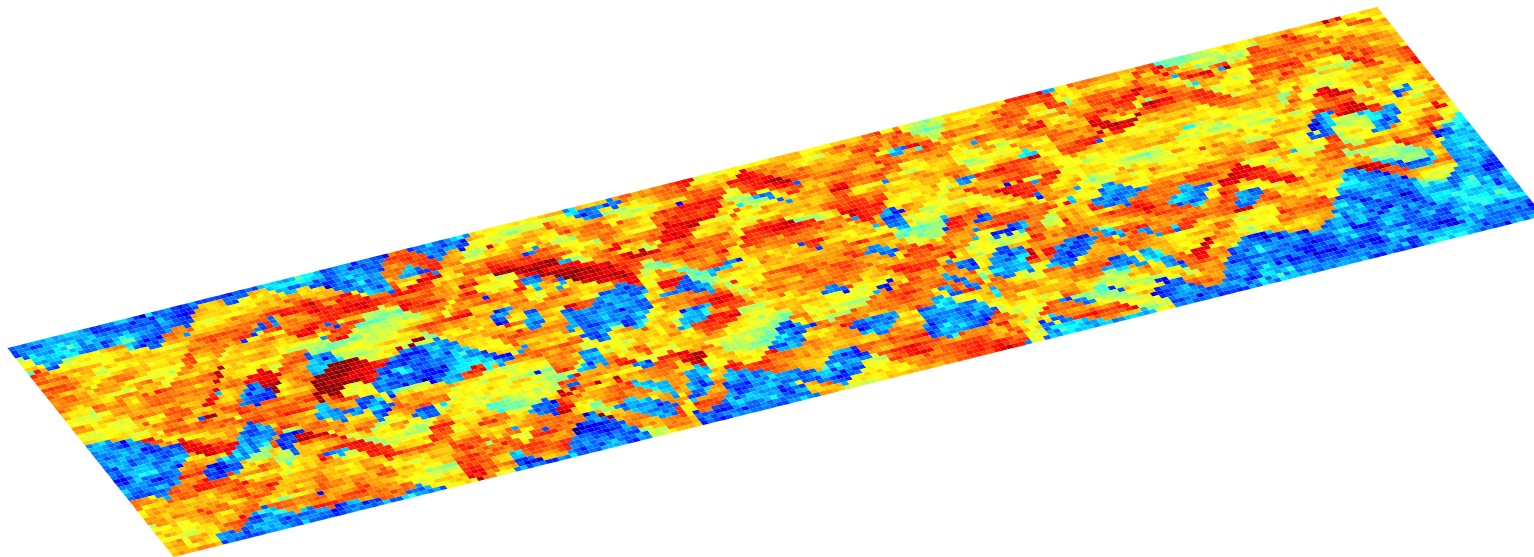
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## Numerical experiments 2

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*The bottom layer of the 10. SPE comparative solution project.*

**Note:** The second criteria does not apply to this case (it doesn't find any barriers).



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## Numerical experiments 2, cont.

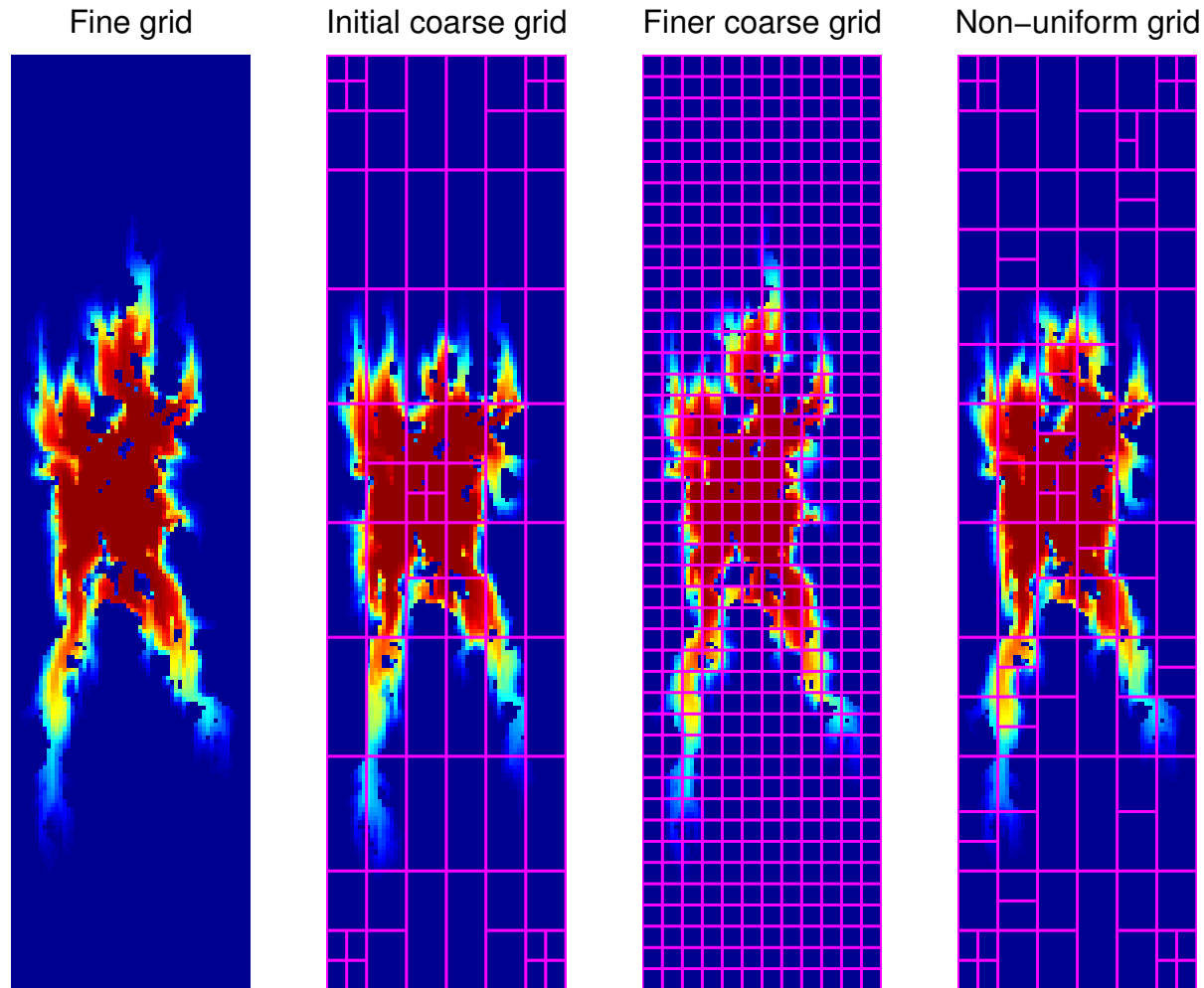
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We apply four different grids:

- Fine grid,  $60 \times 220$  blocks.
- Coarse grid, with some refinement around the wells  
 $6 \times 8 + 12$  blocks.
- Finer coarse grid,  $12 \times 44$  blocks.
- Non-uniform grid, 110 blocks.

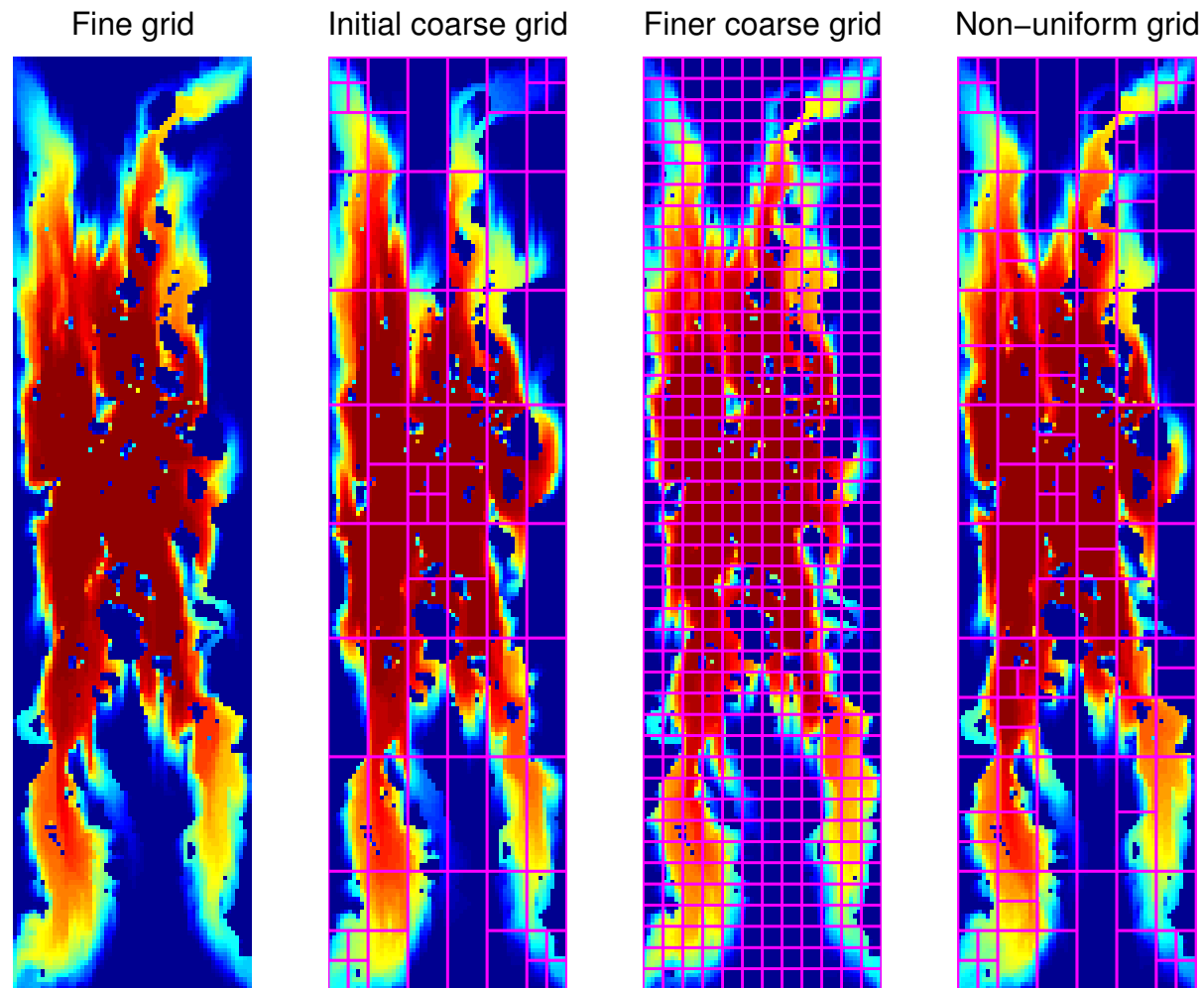
# Numerical experiments 2, cont.

Saturation profiles at  $t = 0.15$ .



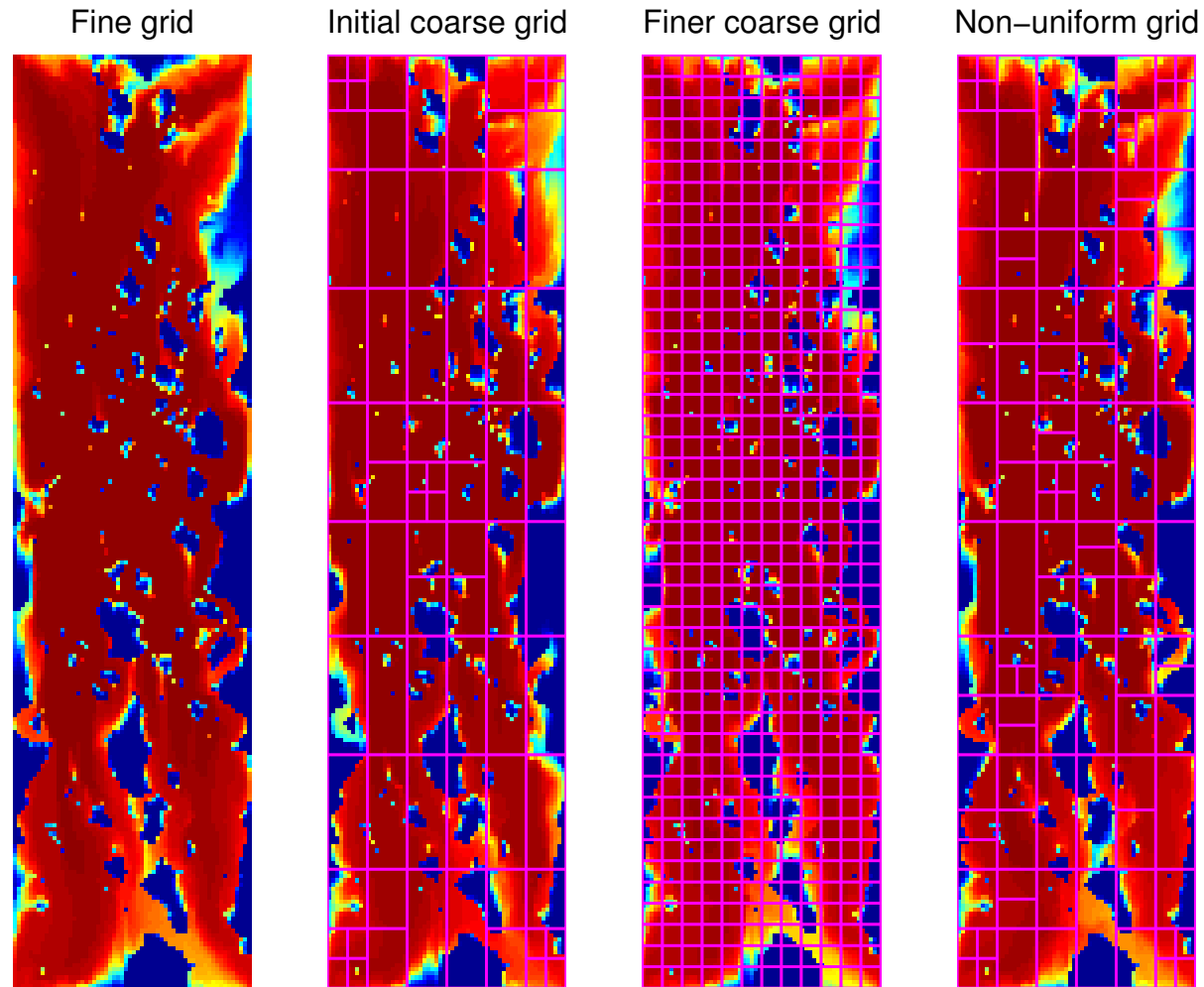
# Numerical experiments 2, cont.

Saturation profiles at  $t = 0.45$ .



# Numerical experiments 2, cont.

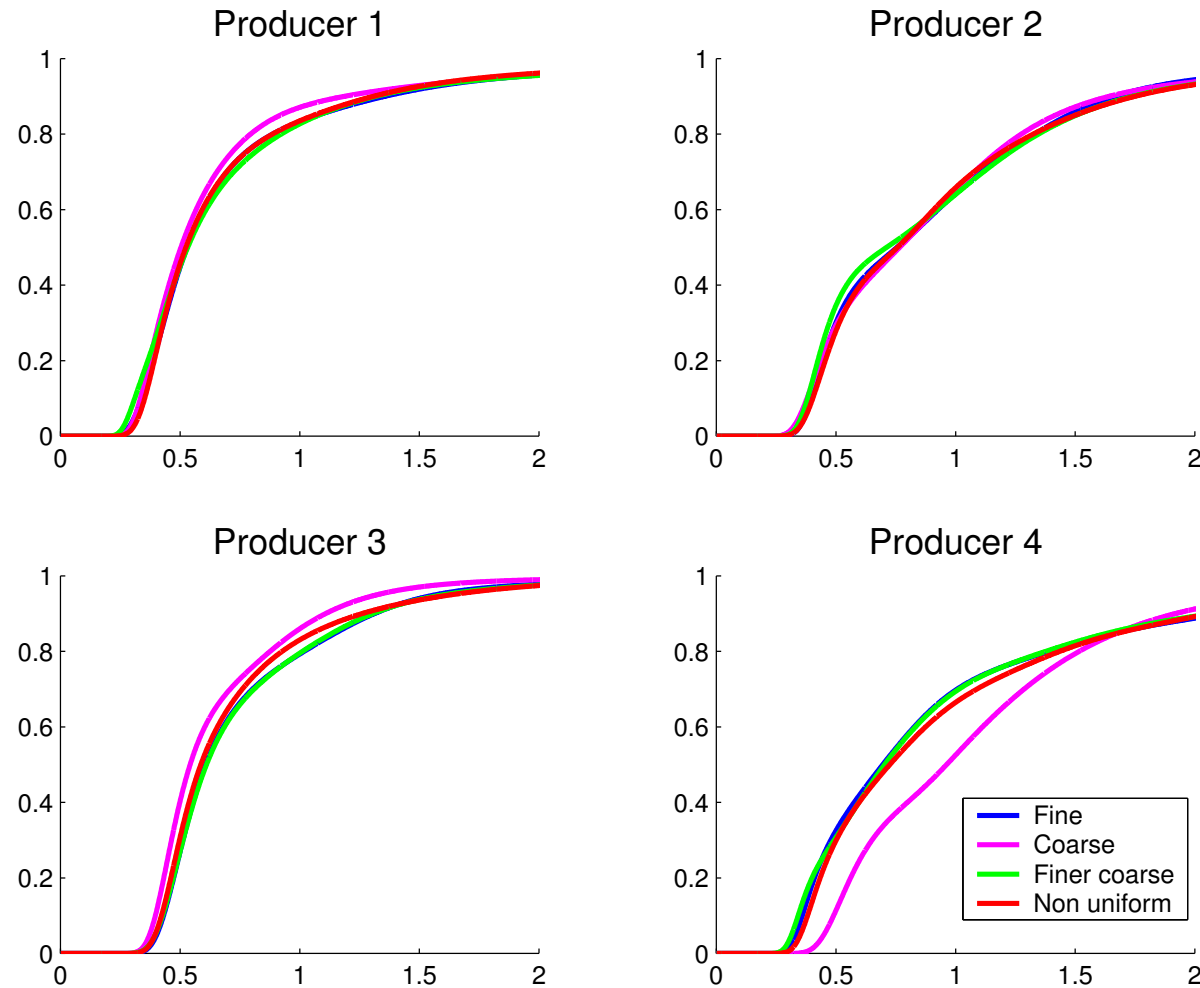
Saturation profiles at  $t = 1.5$ .





# Numerical experiments 2, cont.

Water cut curves ( $\lambda = 1$ ,  $f(S) = S$ ):



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## Numerical experiments 2, cont.

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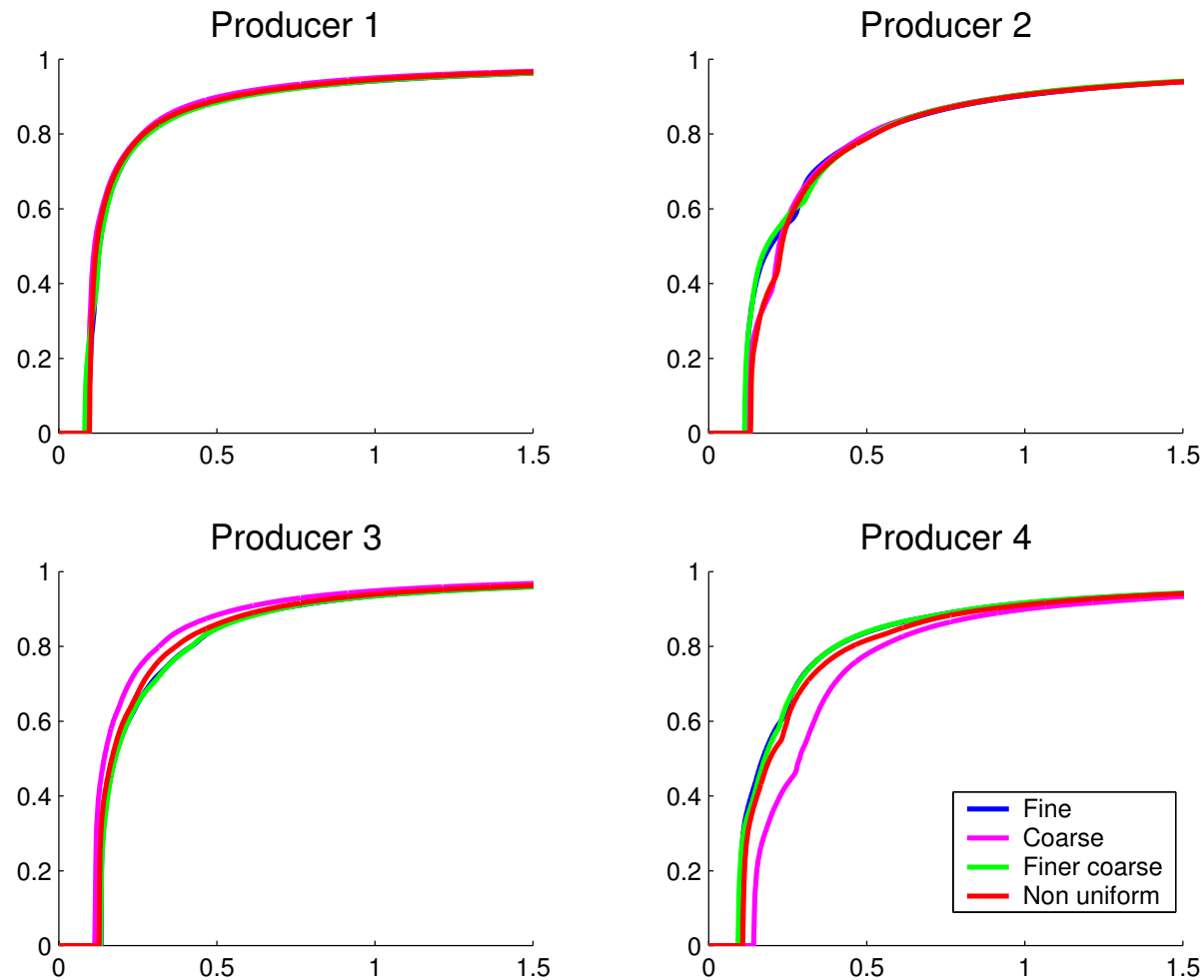
Water cut curves for

$$\lambda_w = \frac{(S^*)^2}{\mu_w}, \lambda_o = \frac{(1 - S^*)^2}{\mu_o},$$

where  $S^* = (S - S_{wc}) / (1 - S_{wc} - S_{or})$ ,  $S_{wc} = S_{or} = 0.2$  and  $\mu_o / \mu_w = 10$ .

# Numerical experiments 2, cont.

## Water cut curves for (non linear mobility)



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## Final remarks

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