A future energy chain based on liquefied hydrogen

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Outline

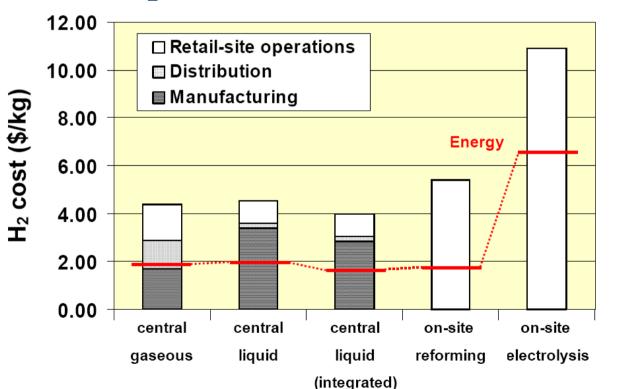
- Introduction to the role of liquefaction in an energy chain with hydrogen as energy carrier
- Comparison of existing and proposed conceptual hydrogen liquefiers
- Selection of a high-efficiency case for the following tasks:
 - Replacement of original pre-cooling of hydrogen to 75 K with a new pre-cooling cycle based on mixed refrigerant (MR) technology
 - Investigate the consequences of this modification with respect to power consumption and process efficiency
- LH₂ in relation to LNG
- Conclusions and further work





Previous Shell study on hydrogen well-to-wheel ¹

- Early-phase scenario: reforming of methane, CO₂ capture and bulk transportation of hydrogen from production site to retail site
- Liquid hydrogen (LH₂) vs. compressed gaseous hydrogen (CGH₂)



Assumed specific liquefaction power for LH₂: 10 kWh/kg_{1 H2}

Average distribution distance: 75 km

Production volume: 100 tonnes/day

Number of retail sites: 100

LH₂ transport capacity: 3500 kg/truck

CGH₂ transport capacity: 350 kg/truck

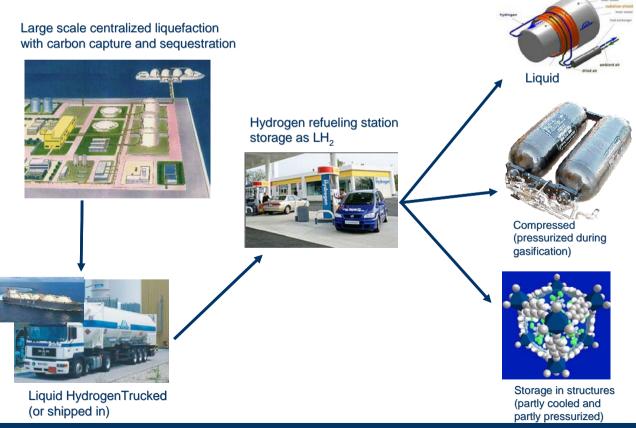
¹Kramer G.J., Huijsmans J.P.P. and Austgen D.M. *Clean and green hydrogen*. 16th World hydrogen energy conference, 2006





Advantages of LH₂

- Flexibility With close to equal overall cost, LH₂-based distribution enables delivery of hydrogen in any form with low energy consumption at retail-side filling stations
- CGH₂ does not offer this flexibility without on-site refrigeration





Transition from current LH₂ production

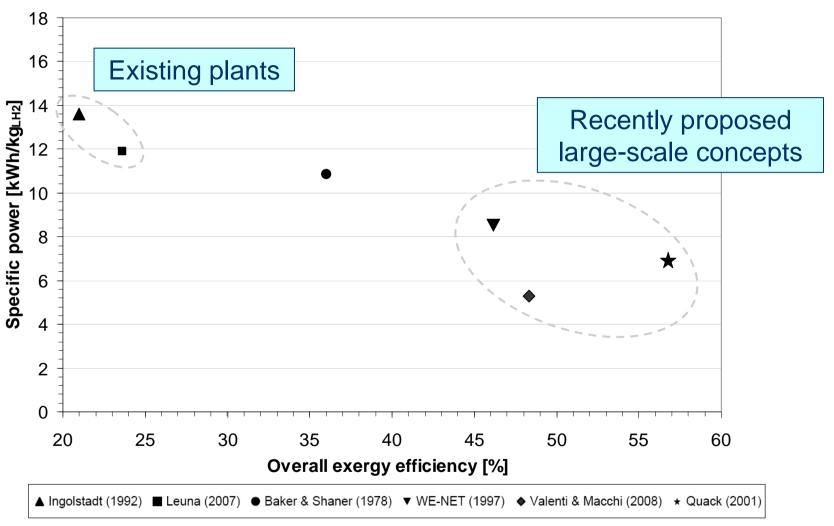
	Existing liquefiers	Envisioned future liquefiers	
Market	LH ₂ for specific industrial purposes	LH ₂ as an energy commodity	
Plant capacity	4.4 tonnes/day (Ingolstadt, 1992) ¹ 5.0 tonnes/day (Leuna, 2007) ²	Significant scale-up in capacity (50–100 tonnes/day or more)	
Specific liquefaction power consumption	13.6 kWh/kg (Ingolstadt) ¹ 11.9 kWh/kg (Leuna) ² (10 kWh/kg used in Shell study)	Considerably lower due to higher emphasis on energy efficiency, scaling-up advantages and shifted cost structure	
Operation	Flexible operation (Leuna: 40–100% load range)	Large base-load plants with high efficiency at full load	

¹Bracha M. et al. Large-scale hydrogen liquefaction in Germany. Int J Hydrogen Energy 19(1):53–59, 1994

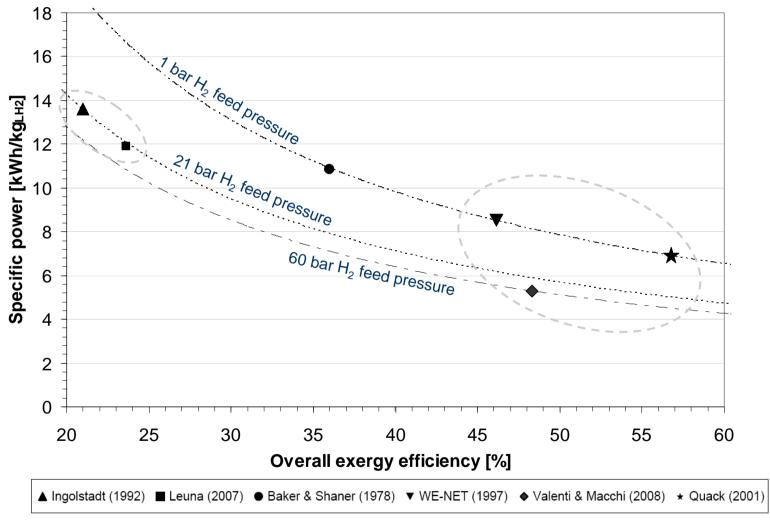
²Bracha M. and Decker L. *Grosstechnische Wasserstoffverflüssigung in Leuna*. Deutsche Kälte-Klima-Tagung, 2008





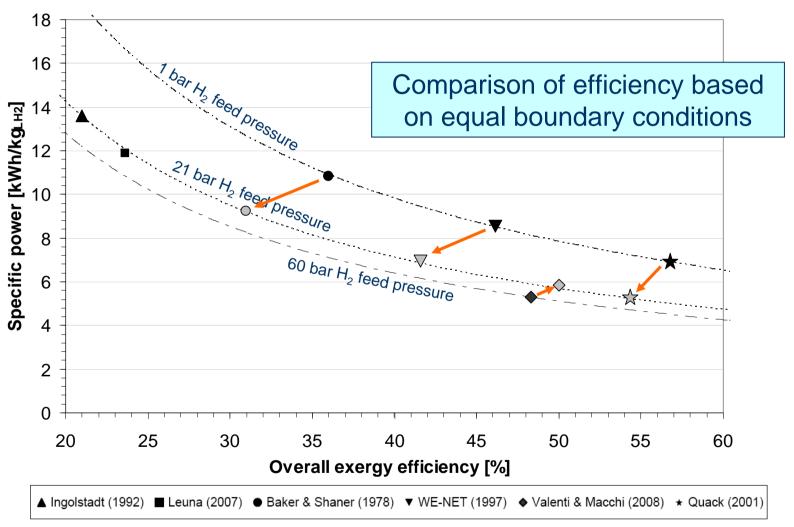




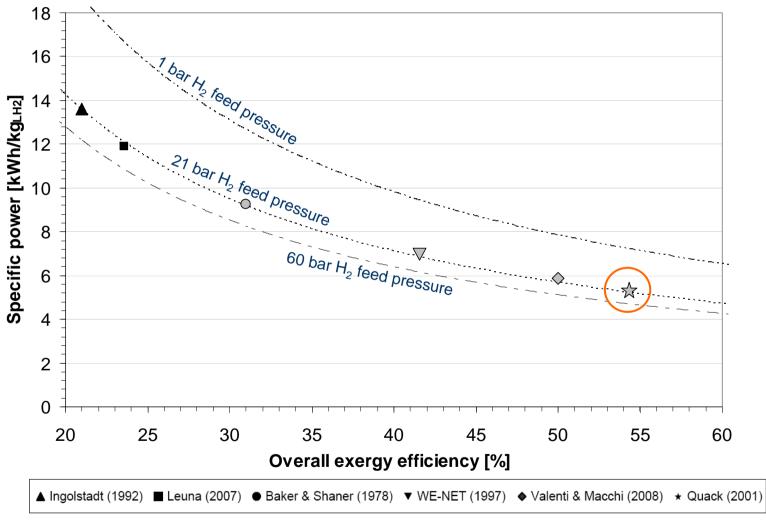














Selecting a reference case for our work

- The concept by Prof. Quack¹ (2001) is the most efficient concept published we have therefore based our work on this concept and using it as reference process
- Changed assumptions of the reference process to be more conservative than in original configuration:
 - For pre-cooling to 220 K, the original 3-stage propane cycle is replaced with 2-stage propane + single-stage ethane refrigeration cycles
 - Assumed 21 bar feed pressure instead of 1 bar
 - Inter-cooler temperature in compressor trains: 310 K
 - Implemented pressure drop in all heat exchangers and inter-coolers
 - Minimum temperature approach (MTA) in heat exchangers:
 - Above 235 K: MTA = 3 K
 - Below 235 K: MTA = 2 K
- Liquefaction capacity: 86 tonnes/day (~ 1 kg/s)
- Resulting exergy efficiency: 45.7%

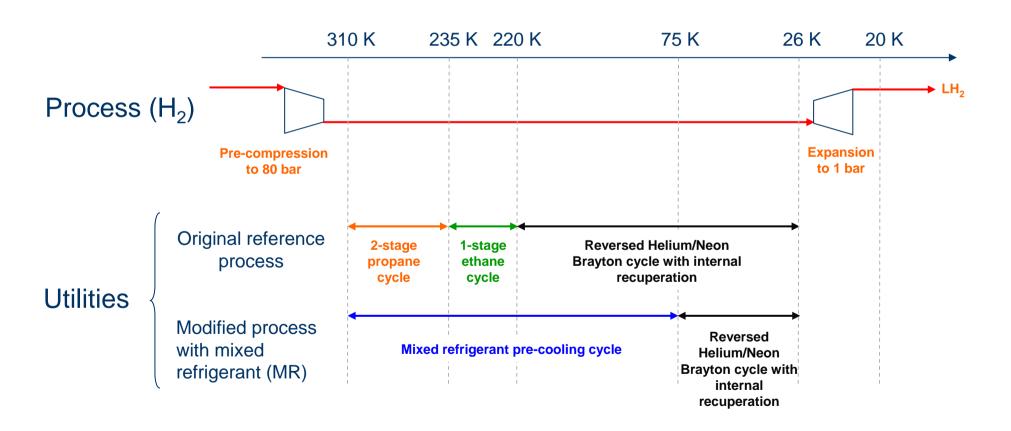
¹Quack H. *Conceptual design of a high efficiency large capacity hydrogen liquefier*. Advances in Cryogenic Engineering 47:255–263, 2001



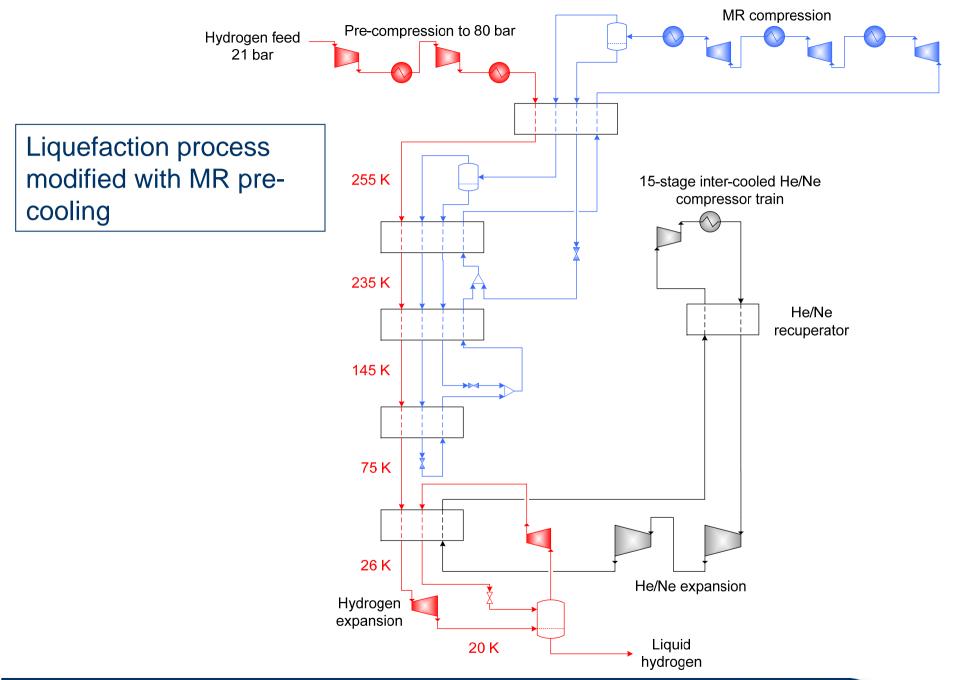


Implementing mixed refrigerant precooling in the reference case

Utilities in the different temperature intervals







Power figures and overall results

	Reference case	Modified MR case with J-T expansions	Modified MR case with liquid expanders
	Electric power [MW]	Electric power [MW]	Electric power [MW]
He/Ne compression	23,139	14,867	14,869
H2 feed compression	2,401	2,401	2,401
Propane-ethane/MR compression	0,732	7,392	6,330
H2 flash-gas compression	0,043	0,043	0,043
Total compression power	26,315	24,703	23,643
He/Ne expansion	3,443	1,271	1,271
H2 liquid expansion	0,086	0,086	0,086
MR expansion	0	0	0,085
Total expansion power	3,529	1,357	1,442
Net power consumption	22,786	23,346	22,201
Specific power consumption [kWh/kg]	6,33	6,49	6,17
Exergy efficiency	45,7 %	44,6 %	46,9 %

- Replacement of J-T valves with rotating liquid expanders (85% isentropic efficiency):
 - Reduces MR HP/LP ratio from 22.4 to 12.4
 - Reduces MR compression power by 17%



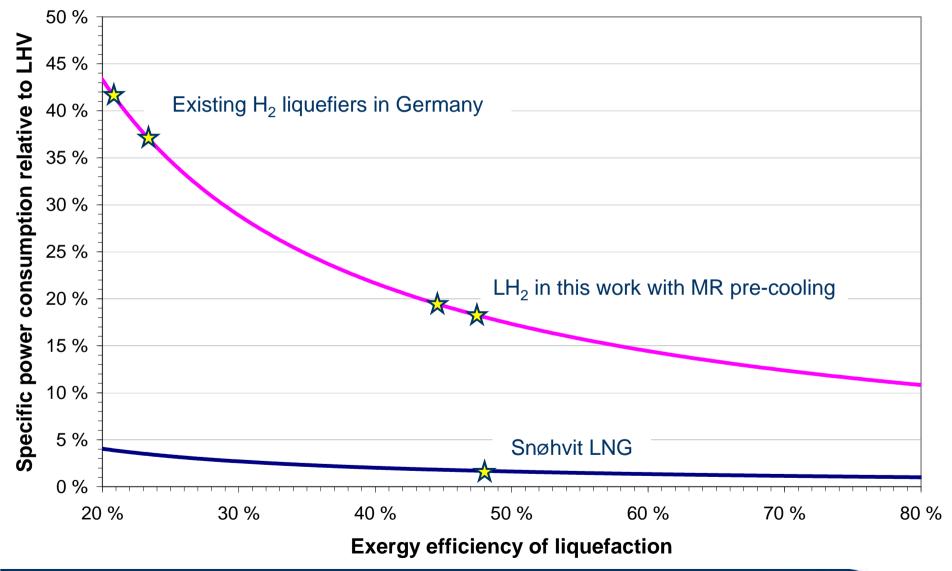
LH₂ related to LNG

- Lower heating value:
 - LNG: ~13.6 kWh/kg (~49 MJ/kg)
 - LH₂: 33.4 kWh/kg (120 MJ/kg)
- Reversible liquefaction power (specific):
 - LNG: 0.11 kWh/kg (Snøhvit gas, Hammerfest conditions)
 - LH₂: 2.89 kWh/kg (21 bar feed pressure, 300 K ambient temperature)
- The Snøhvit LNG plant:
 - Specific design power consumption: 0.23 kWh/kg¹
 - Exergy efficiency: ~48%
- The best-performance LH2 process with MR pre-cooling:
 - Specific design power consumption: 6.17 kWh/kg
 - Exergy efficiency: ~47%

¹Heiersted R.S., Lillesund S., Nordhasli S., Owren G. and Tangvik K. *The Snohvit Design Reflects A Sustainable Environmental Strategy*. Conference paper, LNG-14, Quatar, 2004.



LH₂ related to LNG



Conclusion

- The LH₂ processes employing MR pre-cooling show a specific power consumption of 6.17–6.49 kWh/kg and exergy efficiency of 44.6–46.9%
- 40–50% reduction of power consumption, down from 12 to 6–7 kWh/kg, will represent a radical improvement within large-scale hydrogen liquefaction and contribute to further enhancement of the competitiveness of LH₂ as energy carrier in an hydrogen-based energy chain
- As for LNG, MR pre-cooling may play an important role in the efforts towards efficient large-scale liquefaction processes
- High exergy efficiency is desired and may be obtainable for largescale liquefiers with energy optimisation, extensive process integration and high-efficiency compressors and expanders



Further work: continuation project proposal

Theoretical studies (SP 3)

MR pre-cooling MR freeze-out Ortho-para conversion

Experimental development (SP 4)

MR pre-cooling MR freeze-out Ortho-para conversion



Large-scale liquefaction plants (SP 1)

Modelling and simulation

Components and system elements verification

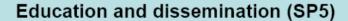
Evaluation of interaction between liquefaction and other utilities and uses



From well to end-user (SP 2)

Case development

Modelling and simulation of complete chains for the given cases



Management (SP6)





Acknowledgements

Financial support





Scientific support

