



# Anchorage of tower foundations in rock

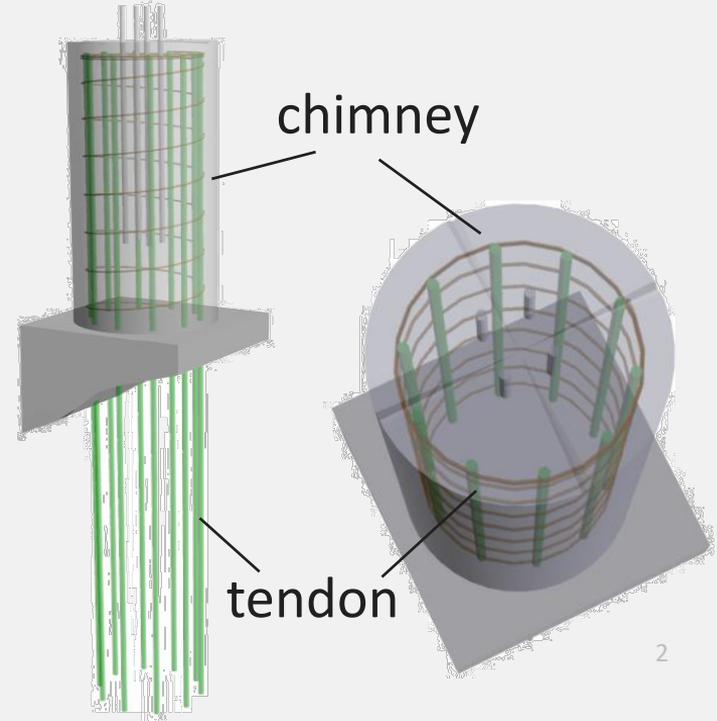
## Classification of rock ground and design rules

Jessica Ka Yi Chiu, [jessica.ka.yi.chiu@ngi.no](mailto:jessica.ka.yi.chiu@ngi.no)

ROCARC-webinar 2020-11-18

# Agenda

1. Background
2. Classification of rock ground
3. Design rules



**NGI Statnett**

**Anchorage of power line tower foundation on rock;  
Classification of rock and design rules**

Tore Valstad<sup>[1]</sup>, Einar John Lande<sup>[1,2]</sup> and Elin Katrine Morgan<sup>[1]</sup>

<sup>[1]</sup> Norwegian Geotechnical Institute (NGI), NO-0806 Oslo, Norway

<sup>[2]</sup> Department of Civil and Transport Engineering –  
Norwegian University of Science and Technology, NO-7491 Trondheim, Norway

John-Petter Sivertsen<sup>[3]</sup>

<sup>[3]</sup> Statnett SF, NO-0484 Oslo, Norway



**GEOVANCOUVER  
2016**

# Foundation of tower chimneys on rock

**Statnett**

**Teknisk standard**

Fundamentering av mastestabber på berg; Klassifisering av berggrunnen

Dokument ID:  
Konfidensialitet:  
Denne kopien ble lastet ned 06.02.2018 av John-Petter Sivertsen.  
Originaldokumentet kan ha blitt publisert i ny revisjon eller trukket tilbake etter at denne kopien ble lastet ned.  
Gjeldende revisjon av dette dokumentet kan lastes ned her:  
<http://samhandling.statnett.no/styrendedok/Dok.aspx?id=SDOK-82-3>

Arbeidsgruppe:  
Ansvarlig:  
Dokumenteier:  
Verifisert:  
Godkjent:  
Planlagt revidert innen:

**Statnett**

**Teknisk standard**

Fundamentering av mastestabber på berg;  
Dimensjoneringsregler

Dokument ID: SDOK-82-3, revisjon: 5.0

Konfidensialitet: K1 For Statnetts interne bruk eller etter avtale med Statnett

Arbeidsgruppe: Seksjon for Mekanisk prosjektering (UTLM)  
Ansvarlig: Leif Halvor Moen  
Dokumenteier: Greta Bjørbeth

Verifisert: 14.11.2016 av Leif Halvor Moen  
Godkjent: 14.11.2016 av Greta Bjørbeth  
Planlagt revidert innen: 14.11.2019

Nøkkelord: Master og fundamenter

- After a power line foundation failure in Sauda – Liastøl, NGI was employed by Statnett to develop a better procedure for rock ground investigation and designing of anchorage of power line tower foundation on rock.
- This resulted in two contract documents: «Classification of rock ground», which presents a procedure for classification of rock ground.
- «Design rules», which presents a procedure for determining bearing capacity of rock ground and required embedment depth of tendons in the tower chimneys based on rock class.

# Load scenarios and loads on tower foundations

- ↴ Stretching of line
- ↴ Wind (50-year return period)
- ↴ Icing (150-year return period)
  
- ↴ Vertical compressional and tensile loads
- ↴ Horizontal forces
- ↴ (Moments)



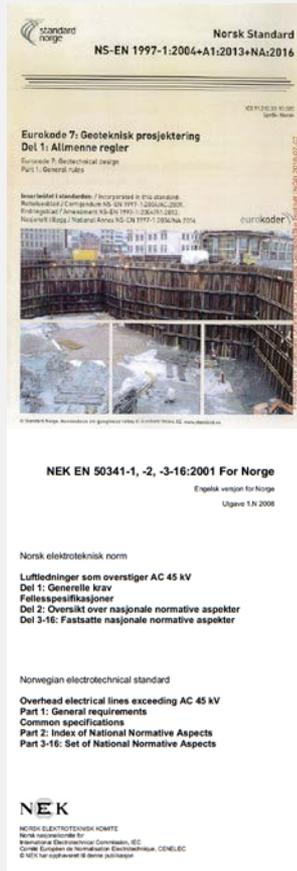
«Record» in icing on power line (22 kV), ca. 1.5 m ice that constituted ca. 300 kg/m line  
Picture from Lønahorgi, 1961 (Olav Wist)

# What is the purpose of these specification?

- To establish a safe practise for design of the tower foundations on rock ground, with focus on:
  - A. Bearing capacity on rock ground
  - B. Pull-out resistance of the rock ground



# General information about the specifications



- General rules for design of overhead electric lines are given in NEK-EN 50341-1, and -3-16:2001 «Overhead electric lines exceeding AC 45 kV», however, this does not cover tower foundations in rock.
- Therefore the rules are based on Eurocode 7, NS-EN 1997-1:2004+A1:2013+NA:2016
- The main focus is on anchorage of the chimney foundations against pull-out forces, which is usually controlling the design.
- To be applied by consultants and contractors responsible for design and construction of power lines for Statnett.
- Based on a classification of the rock ground at the site.



# Classification of rock ground

# Table 1 Classification of rock ground

<i>Rock class</i>	<i>Designation</i>	<i>Description</i>
0	Massive rock	Intact rock or massive rock with a few widely spaced joints. The joint surfaces are unweathered and rough
1	Slightly jointed rock	Rock mass intersected by one or two sets of joints. The joints are well interlocked and unweathered. Joint surfaces are rough to planar.
2	Blocky rock	Rock mass intersected by two or three, sets of joint forming cubical blocks. Joints are well interlocked and unweathered. Joint surfaces are rough to planar.
3	Very blocky rock	Rock mass intersected by four or more joint sets. Joints are slightly interlocked or slightly weathered. Joints are planar or slightly filled with gauge material.
4	Disturbed or disintegrated rock	Rock mass with several joint sets. Joints are poorly interlocked, persistent or schistose. Joints may be planar or filled with gauge material.
<i>Remark</i>	The term “joint” is used herein as a common description of discontinuities in rock such as crack, fissure, shear, fault, bedding, etc.	



# Table 1 Classification of rock ground

<i>Rock class</i>	<i>Designation</i>	<i>Description</i>
0	Massive rock	<b><u>Class 0 &amp; Class 1</u></b> Sufficient tensile strength to withstand uplifting forces.
1	Slightly jointed rock	
2	Blocky rock	<b><u>Class 2 &amp; Class 3</u></b> So low tensile strength that the uplifting forces can only be countered by <b>shear resistance of joints</b> and the <b>weight of the rock lump</b> between the embedded tendons.
3	Very blocky rock	
4	Disturbed or disintegrated rock	<b><u>Class 4</u></b> A concrete foundation in a blasted or excavated pit is <b>cheaper</b> than to reinforce the rock mass with tendons.



# Classification criteria

Property	ROCK CLASS				
	0	1	2	3	4
	Massive	Slightly jointed	Blocky	Very blocky	Disturbed or disintegrated
<b>Weathering</b>	Grade 0 - 1 Fresh or slightly	Grade 0 - 1 Fresh or slightly	Grade 0 - 1 Fresh or slightly	Grade 0 - 1 Fresh or slightly	Grade 2, 3, 4 Moderate or higher
<b>Unconfined compressive strength</b>	Grade 0 - 2 $q_u > 100$ MPa	Grade 0 - 3 $q_u > 50$ MPa	Grade 0 - 4 $q_u > 25$ MPa	Grade 0 - 4 $q_u > 25$ MPa	Grade 0 - 6 $q_u < 25$ MPa
<b>Number of joint sets</b>	$\leq 1$ + random	$\leq 2$	$\leq 3$	$\leq 3$ + random	$\geq 4$
<b>Joint spacing</b>	Very wide $\geq 2000$ mm	Wide or greater $\geq 600$ mm	Medium or greater $\geq 200$ mm	Close or greater $\geq 60$ mm	Very close or less $< 60$ mm
<b>Joint roughness</b>	Rough, stepped or undulating	Rough, stepped or undulating	Rough, stepped, undulating or planar	Rough, smooth, stepped, undulating or, planar	Any roughness
<b>Joint aperture</b>	Tight or less $\leq 0.25$ mm	Partly open or less $\leq 0.5$ mm	Open or less $\leq 2.5$ mm	Moderately wide or less $\leq 10$ mm	Very wide or greater $\geq 10$ mm
<b>Joint filling</b>	None	None	Granular material	Granular material	Clayey material

# Example from Inner Oslofjord – reporting

## ➤ Results of classification (for each tower leg)

Property	ROCK CLASS				
	0	1	2	3	4
	Massive	Slight jointed	Blocky	Very blocky	Disturbed or disintegrated
Weathering	Grade 0 - 1 Fresh or slightly	Grade 0 - 1 Fresh or slightly	Grade 0 - 1 Fresh or slightly	Grade 0 - 1 Fresh or slightly	Grade 2, 3, 4 Moderate or higher
Unconfined compressive strength	Grade 0 - 2 $q_u > 100$ MPa	Grade 0 - 3 $q_u > 50$ MPa	Grade 0 - 4 $q_u > 25$ MPa	Grade 0 - 4 $q_u > 25$ MPa	Grade 0 - 6 $q_u < 25$ MPa
Number of joint sets	$\leq 1$ + random	$\leq 2$	$\leq 3$	$\leq 3$ + random	$\geq 4$
Joint spacing	Very wide $\geq 2000$ mm	Wide or greater $\geq 600$ mm	Medium or greater $\geq 200$ mm	Close or greater $\geq 60$ mm	Very close or less $< 60$ mm
Joint roughness	Rough, stepped or undulating	Rough, stepped or undulating	Rough, stepped, undulating or planar	Rough, smooth, stepped, undulating or, planar	Any roughness
Joint aperture	Tight or less $\leq 0.25$ mm	Partly open or less $\leq 0.5$ mm	Open or less $\leq 2.5$ mm	Moderate wide or less $\leq 10$ mm	Very wide or greater $\geq 10$ mm
Joint filling	None	None	Granular material	Granular material	clayey material



# Design investigations (2)

- ↗ For Class 2 & Class 3:
- ↗ Fractured and weathered surface rock may be removed, then undertake **new classification**.
- ↗ Hydraulic hammer are well suited in removal of surface rock.
- ↗ Blasting of surface rock will seldom be appropriate. The base charge often tears up the rock and create new joints.



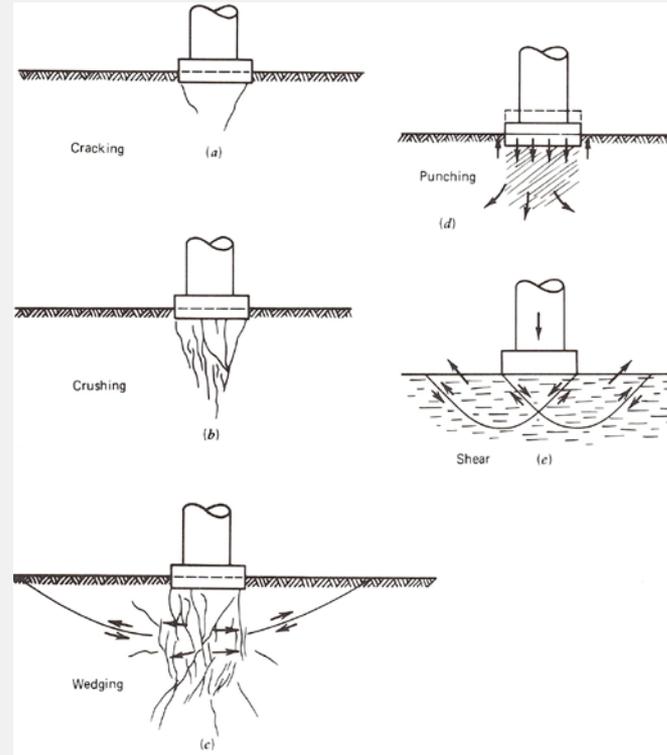


# Design rules

# Chimney foundation design - general requirements

➤ Design of chimney foundations comprise two main tasks:

1. Check that bearing capacity of the rock ground are adequate against **design compressional loads** from the chimney.



Possible modes of failure at ultimate bearing capacity of foundation rock (Goodman 1989)

# Chimney foundation design - general requirements

- Design of chimney foundations comprise two main tasks:
  1. Check that the anchorage in rock has adequate resistance (capacity) against **design tensile forces from chimney**.

# Strength parameters of rock mass

Tabell 1 Karakteristiske og dimensjonerende fasthetsparametere for berggrunnen  
Table 1 Characteristic and design strength parameters of rock mass

Fasthetsparameter Strength Parameter	Bergklasse / Rock Class			
	0	1	2	3
Enaksial trykkfasthet i intakt berg, $q_{u,k}$ Unconfined compressive strength of intact rock, $q_{u,k}$ MPa	100	50	25	25
Strekkfasthet av bergmassen, $T_{0,k}$ Tensile strength of the rock mass, $T_{0,k}$ MPa	4.0	0.81	0.17	0.06
Bæreevne av berggrunnen, $q_{ad}$ Bearing capacity of rock mass, $q_{ad}$ MPa	71.4	16.4	5.0	3.1
Dimensjonerende strekkfasthet av bergmassen, $T_{0d}$ Design tensile strength of rock mass, $T_{0d}$	2.0	0.40	0.085	0.03
Dimensjonerende heftfasthet i berggrunnen og i forankring berg / mørtel, $f_{brd}$ Design bond strength in rock mass and in anchorage rock/mortar, $f_{brd}$ MPa	1.97	1.4	1.0	0.7
Dimensjonerende heftfasthet mørtel/stag; B35, $f_{bcd}^{[1]}$ Design bond strength mortar/tendon; B35, $f_{bcd}$ MPa	1.97	1.97	1.97	1.97

<sup>[1]</sup> Bestemt iht. NS-EN 1992-1 for terningfasthet,  $f_{ck} = 45$  MPa /  
According to NS-EN 1992-1 for cube strength,  $f_{ck} = 45$  MPa

## How to determine bearing capacity of the rock ground?

- Characteristic values for bearing capacity of rock class (0-3)
- Bearing capacity based on the UCCS of intact rock, joint spacing, joint aperture.
- Characteristic strength values of rock ground estimated based on classification criteria, using the Hoek & Brown failure criterion.
- Boundary limits between the rock classes and engineering judgements

# Bearing capacity of foundation rock

Presumptions:

- I. Only effective area of the chimney can transfer compressive force to bedrock (= inner diameter of hoop reinforcement)
- II. Design compression capacity of tendons,  $f_{yd} = 400$  Mpa.
- III. Design compressive strength of concrete,  $f_{cd} = 19,8$  Mpa
- IV. Concrete cover = 50 mm.
- V. Diameter hoop reinforcement 10 mm.



# Bearing capacity of foundation rock

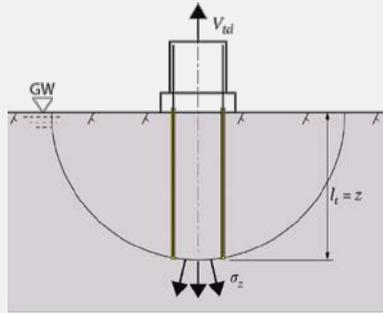
- For rock class 0 and 1, the bearing capacity is limited by the reinforced chimney, i.e steel and concrete.
- For rock class 2 and 3 the bearing capacity is limited by capacity of rock mass and steel tendons.

Tabell 2 Dimensjonerende bæreevne av berggrunnen; stabbe type I, II og III  
 Table 2 Design bearing capacity of bedrock; chimney type I, II and III

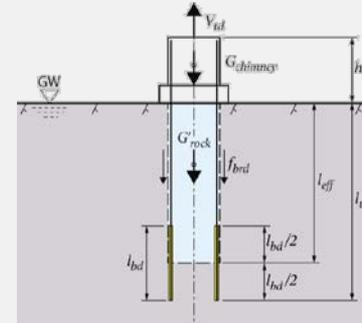
Type	Diameter	Stabbe / Chimney				Dim. bæreevne / Design bearing capacity			
		Lengdearmoring / reinforcement		Kapasitet/ capacity, $R_{td}^{(1)}$	Eff. areal betong/ Net area concrete	Bergklasse / rock class			
		Ø stag / bar	Antall stag / number of tendons			0	1	2	3
mm	mm	-	kN	mm <sup>2</sup>	kN	kN	kN	kN	
I	600	25	6	1178	180 956	4 761	4 761	1 794	1 377
			8	1571		5 154	5 154	2 186	1 770
			10	1964		5 547	5 547	2 579	2 163
			12	2357		5 940	5 940	2 972	2 556
			14	2750		6 333	6 333	3 365	2 949
I	600	32	6	1930	180 956	5 513	5 513	2 545	2 129
			8	2573		6 156	6 156	3 188	2 772
			10	3216		6 799	6 799	3 831	3 415
			12	3859		7 442	7 442	4 474	4 058
			14	4502		8 085	8 085	5 118	4 701
II	750	25	6	1178	311 725	7 351	7 351	2 238	1 521
			8	1571		7 743	7 743	2 631	1 914
			10	1964		8 136	8 136	3 024	2 307
			12	2357		8 529	8 529	3 417	2 700
			14	2750		8 922	8 922	3 809	3 092
			16	3142		9 315	9 315	4 202	3 485
			18	3535		9 707	9 707	4 595	3 878
II	750	32	6	1930	311 725	8 102	8 102	2 989	2 272
			8	2573		8 745	8 745	3 633	2 916
			10	3216		9 388	9 388	4 276	3 559
			12	3859		10 031	10 031	4 919	4 202
			14	4502		10 675	10 675	5 562	4 845
			16	5146		11 318	11 318	6 205	5 488
			18	5789		11 961	11 961	6 849	6 132
III	1000	25	6	1178	608 212	13 221	13 221	3 246	1 847
			8	1571		13 614	13 614	3 639	2 240
			10	1964		14 007	14 007	4 032	2 633
			12	2357		14 399	14 399	4 425	3 026
			14	2750		14 792	14 792	4 818	3 419
			16	3142		15 185	15 185	5 210	3 811
			18	3535		15 578	15 578	5 603	4 204
			20	3928		15 971	15 971	5 996	4 597
			22	4321		16 363	16 363	6 389	4 990
			24	4714		16 756	16 756	6 782	5 383
			26	5106		17 149	17 149	7 174	5 775
			28	5499		17 542	17 542	7 567	6 168
			III	1000		32	6	1930	608 212
8	2573	14 615			14 615		4 641	3 242	
10	3216	15 259			15 259		5 284	3 885	
12	3859	15 902			15 902		5 927	4 528	
14	4502	16 545			16 545		6 570	5 171	
16	5146	17 188			17 188		7 214	5 815	
18	5789	17 831			17 831		7 857	6 458	
20	6432	18 475			18 475		8 500	7 101	
22	7075	19 118			19 118		9 143	7 744	
24	7718	19 761			19 761		9 786	8 387	
26	8362	20 404			20 404		10 430	9 030	
28	9005	21 047			21 047		11 073	9 674	

<sup>(1)</sup>  $R_{td}$  = Dimensjonerende motstand i stålvertsnitt stag med dim. flytekapasitet  $f_{td} = 400 \text{ N/mm}^2$  / Design resistance of tendon cross section for design yield strength  $f_{td} = 400 \text{ N/mm}^2$ .

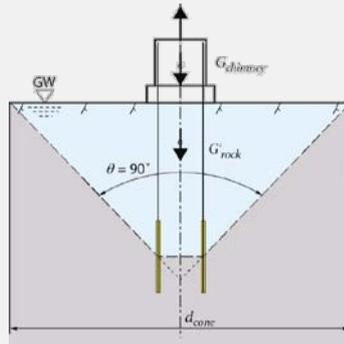
# Computational models for pull-out resistance in rock



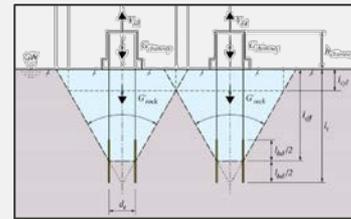
1. Tensile strength model (rock class 0-1)



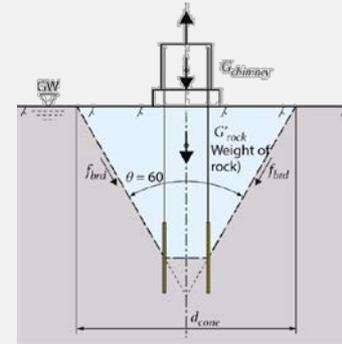
2. Pull-out cylinder shaft (rock class 1-2)



3. Weight of cone (rock class 2-3)



*For long embedded tendons*



4. Combined weight of cone and bond strength (rock class 2-3)

# Required embedment depth of tendons

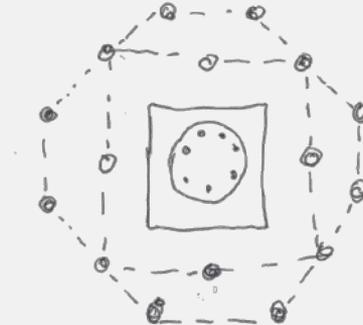
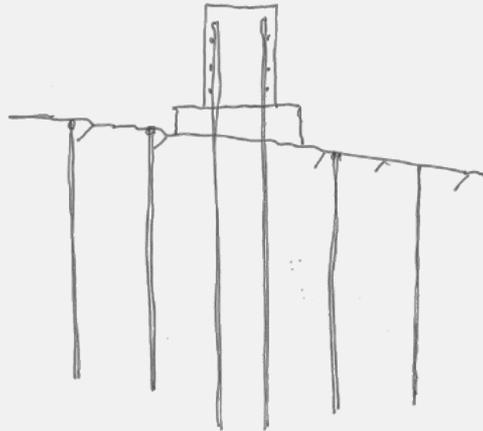
CHIMNEY							FORANKRINGSDYBDE   BERG / EMBEDMENT DEPTH OF TENDONS IN BEDROCK																												
Type	Outer diameter mm	Reinforcement				R <sub>td</sub> kN	Bond resistance												Tensile Strength Criterion				Shaft Friction Criterion				Gravity & Bond Criterion			Gravity criterion	Summary				
		Cover mm	Ø-bar mm	Ø-hoop mm	Number of bars		R <sub>rod</sub>	R <sub>rod</sub>				Rock Class				Rock Class				Rock class			Rock Class												
								0	1	2	3	0	1	2	3	0	1	2	3	1	2	3	0	1	2	3									
I	600	50	25	10	6	1 178	1 270	910	1 280	1 790	2 550	530	1 190	2 570	4 330	460	650	920	920	1 350	1 450	1 600	4 500	1 270	1 350	1 790	2 550								
					8	1 571	1 270	910	1 280	1 790	2 550	610	1 370	2 970	5 000	610	870	1 230	1 230	1 450	1 600	1 750	4 850	1 600	1 450	1 790	2 550								
					10	1 964	1 270	910	1 280	1 790	2 550	680	1 530	3 320	5 590	770	1 090	1 540	1 540	1 550	1 700	1 900	5 200	1 270	1 550	1 790	2 550								
					12	2 357	1 270	910	1 280	1 790	2 550	750	1 680	3 640	6 120	920	1 300	1 840	1 840	1 650	1 800	2 000	5 500	1 270	1 680	1 840	2 550								
					14	2 750	1 270	910	1 280	1 790	2 550	810	1 810	3 930	6 620	1 080	1 520	2 150	2 150	1 750	1 900	2 100	5 750	1 270	1 810	2 150	2 550								
					16	3 142	1 270	910	1 280	1 790	2 550	870	1 940	4 200	7 070	940	1 320	1 870	1 870	1 650	2 000	2 200	5 950	1 270	1 940	2 000	2 550								
	I	600	50	32	10	6	1 930	1 620	1 300	1 830	2 560	3 660	680	1 520	3 290	5 540	570	1 070	1 510	1 700	1 900	2 100	5 350	1 620	1 830	2 560	3 660								
						8	2 573	1 620	1 300	1 830	2 560	3 660	780	1 750	3 800	6 400	1 010	1 420	2 010	2 010	1 850	2 250	5 850	1 620	1 850	2 560	3 660								
						10	3 216	1 620	1 300	1 830	2 560	3 660	880	1 960	4 250	7 150	1 260	1 780	2 520	2 520	1 950	2 150	2 400	6 250	1 620	1 960	2 560	3 660							
						12	3 859	1 620	1 300	1 830	2 560	3 660	960	2 150	4 660	7 840	1 150	2 140	3 020	3 020	2 050	2 300	2 550	6 600	1 620	2 150	3 020	3 660							
						14	4 502	1 620	1 300	1 830	2 560	3 660	1 040	2 320	5 030	8 470	1 760	2 490	3 520	3 520	2 150	2 400	2 700	6 900	1 620	2 490	3 520	3 660							
						16	5 145	1 620	1 300	1 830	2 560	3 660	1 120	2 500	5 400	9 200	2 370	3 160	4 200	4 200	2 150	2 400	2 700	7 500	1 620	2 500	3 520	3 660							
II	750	50	25	10	6	1 178	1 270	910	1 280	1 790	2 550	530	1 190	2 570	4 330	350	500	700	1 350	1 450	1 600	4 400	1 270	1 350	1 790	2 550									
					8	1 571	1 270	910	1 280	1 790	2 550	610	1 370	2 970	5 000	470	660	940	940	1 450	1 600	1 750	4 800	1 270	1 450	1 790	2 550								
					10	1 964	1 270	910	1 280	1 790	2 550	680	1 530	3 320	5 590	590	830	1 170	1 170	1 550	1 700	1 900	5 100	1 270	1 550	1 790	2 550								
					12	2 357	1 270	910	1 280	1 790	2 550	750	1 680	3 640	6 120	700	990	1 410	1 410	1 650	1 800	2 000	5 450	1 270	1 680	1 800	2 550								
					14	2 750	1 270	910	1 280	1 790	2 550	810	1 810	3 930	6 620	820	1 160	1 640	1 640	1 750	1 900	2 100	5 700	1 270	1 810	1 900	2 550								
					16	3 142	1 270	910	1 280	1 790	2 550	870	1 940	4 200	7 070	940	1 320	1 870	1 870	1 650	2 000	2 200	5 950	1 270	1 940	2 000	2 550								
	II	750	50	32	10	6	1 930	1 620	1 300	1 830	2 560	3 660	680	1 520	3 290	5 540	580	810	1 150	1 150	1 700	1 900	2 100	5 300	1 620	1 830	2 560	3 660							
						8	2 573	1 620	1 300	1 830	2 560	3 660	780	1 750	3 800	6 400	770	1 090	1 530	1 530	1 850	2 000	2 250	5 750	1 620	1 850	2 560	3 660							
						10	3 216	1 620	1 300	1 830	2 560	3 660	880	1 960	4 250	7 150	960	1 360	1 920	1 920	1 950	2 150	2 400	6 150	1 620	1 960	2 560	3 660							
						12	3 859	1 620	1 300	1 830	2 560	3 660	960	2 150	4 660	7 840	1 150	1 630	2 300	2 300	2 050	2 300	2 550	6 500	1 620	2 150	2 560	3 660							
						14	4 502	1 620	1 300	1 830	2 560	3 660	1 040	2 320	5 030	8 470	1 340	1 900	2 680	2 680	2 150	2 400	2 700	6 800	1 620	2 320	2 680	3 660							
						16	5 146	1 620	1 300	1 830	2 560	3 660	1 110	2 480	5 380	9 050	1 530	2 170	3 070	3 070	2 250	2 500	2 850	7 100	1 620	2 480	3 070	3 660							
III	1000	50	25	10	6	1 178	1 270	910	1 280	1 790	2 550	530	1 190	2 570	4 330	250	360	500	500	1 350	1 450	1 600	4 250	1 270	1 350	1 790	2 550								
					8	1 571	1 270	910	1 280	1 790	2 550	610	1 370	2 970	5 000	340	470	670	670	1 450	1 600	1 750	4 650	1 270	1 450	1 790	2 550								
					10	1 964	1 270	910	1 280	1 790	2 550	680	1 530	3 320	5 590	420	590	840	840	1 550	1 700	1 900	5 000	1 270	1 550	1 790	2 550								
					12	2 357	1 270	910	1 280	1 790	2 550	750	1 680	3 640	6 120	500	710	1 010	1 010	1 650	1 800	2 000	5 300	1 270	1 680	1 800	2 550								
					14	2 750	1 270	910	1 280	1 790	2 550	810	1 810	3 930	6 620	590	830	1 170	1 170	1 750	1 900	2 100	5 550	1 270	1 810	1 900	2 550								
					16	3 142	1 270	910	1 280	1 790	2 550	870	1 940	4 200	7 070	590	830	1 170	1 170	1 650	2 000	2 200	5 950	1 270	1 940	2 000	2 550								
	III	1000	50	32	10	6	1 930	1 620	1 300	1 830	2 560	3 660	680	1 520	3 290	5 540	410	560	820	820	1 700	1 900	2 100	5 150	1 620	1 830	2 560	3 660							
						8	2 573	1 620	1 300	1 830	2 560	3 660	780	1 750	3 800	6 400	550	780	1 100	1 100	1 850	2 000	2 250	5 650	1 620	1 850	2 560	3 660							
						10	3 216	1 620	1 300	1 830	2 560	3 660	880	1 960	4 250	7 150	690	970	1 370	1 370	1 950	2 150	2 400	6 050	1 620	1 960	2 560	3 660							
						12	3 859	1 620	1 300	1 830	2 560	3 660	960	2 150	4 660	7 840	820	1 160	1 650	1 650	2 050	2 300	2 550	6 400	1 620	2 150	2 560	3 660							
						14	4 502	1 620	1 300	1 830	2 560	3 660	1 040	2 320	5 030	8 470	960	1 360	1 920	1 920	2 150	2 400	2 700	6 700	1 620	2 320	2 680	3 660							
						16	5 146	1 620	1 300	1 830	2 560	3 660	1 110	2 480	5 380	9 050	1 100	1 550	2 200	2 200	2 250	2 500	2 850	7 000	1 620	2 480	2 680	3 660							

R<sub>td</sub> - Design resistance of tendon cross section for design yield strength f<sub>td</sub> = 400 N/mm<sup>2</sup>  
 R<sub>rod</sub> - Design bond resistance between tendon and mortar  
 R<sub>rod</sub> - Design bond resistance between mortar and rock mass  
 γ<sub>r</sub> - Effective weight of rock mass is assumed to be 17 kN/m<sup>3</sup>  
 Color codes: 1250 Min. bond length, 50 x Ø-bar; 460 Bond resistance tendon-mortar; 910 Bond resistance mortar-rock; 530 Tensile strength criterion; 1600 Gravity + bond strength criterion; 4500 Gravity criterion



# Ground improvement

- ↗ For Class 2 & Class 3:
- ↗ As an alternative to long tendons, the rock may be reinforced around the chimney to engage lateral rock mass instead of at depth.



# Monitoring of permanent post-tensioned rock anchors

## Surveillance d'ancrages permanents en post-tension dans la roche

E.J. Lande

*Norwegian Geotechnical Institute, Oslo, Norway*

*Norwegian University of Science and Technology (NTNU), Trondheim, Norway*

T. Valstad, E. Stein and J.M. Josefsen

*Norwegian Geotechnical Institute, Oslo, Norway*

I. Brovold

*Statnett SF, Oslo, Norway*



- ↗ Measurement once a year by Statnett
- ↗ Condition control and assess the need for future tensioning
- ↗ R&D: to gain more knowledge on the long-term behavior and hopefully improve the current design methodology for anchors in **strong rock types**.
- ↗ At least 10 years' monitoring (post-tensioning 13 September, 2017)

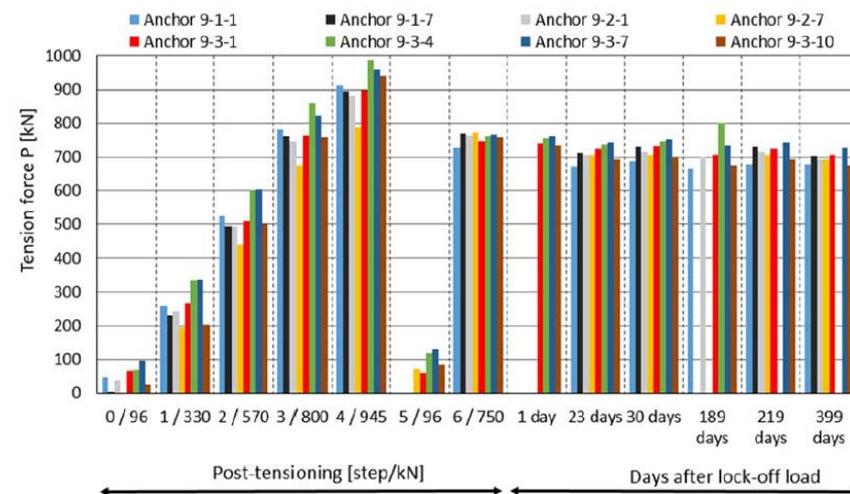


Figure 7. Tension force  $P$  in rock anchors measured with load cells on anchor head. Results from post-tensioning steps 0 to 6 (left side), and the first 399 days after lock-off load (right side).

Design pylon, Lysefjorden ([read more](#))



Thank you!



#påsikkergrunn