

# New Apparatus For Solid-Fluid Equilibrium Measurements

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# Introduction

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➔ The production of LNG requires temperatures as low as - 161 °C (-112 K), which is the normal boiling point of methane.

## Current LNG specifications

CO<sub>2</sub> < 50 ppm

Water < 0.1 ppm

C4 ≤ 2 mol%

C5+ ≤ 0.1 mol%

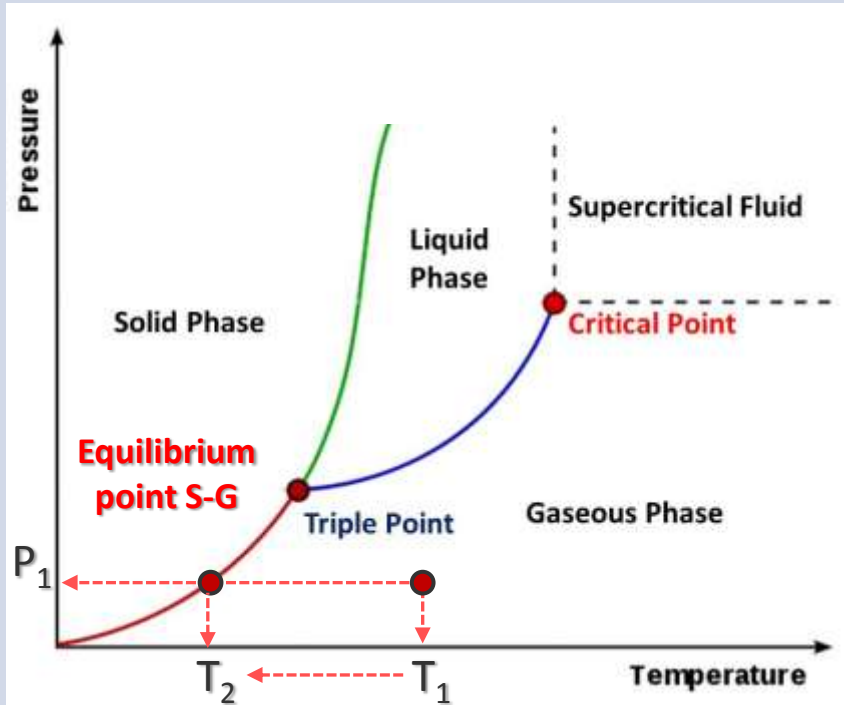
Aromatics < 2 ppm

} Very low allowable impurity levels in the gas

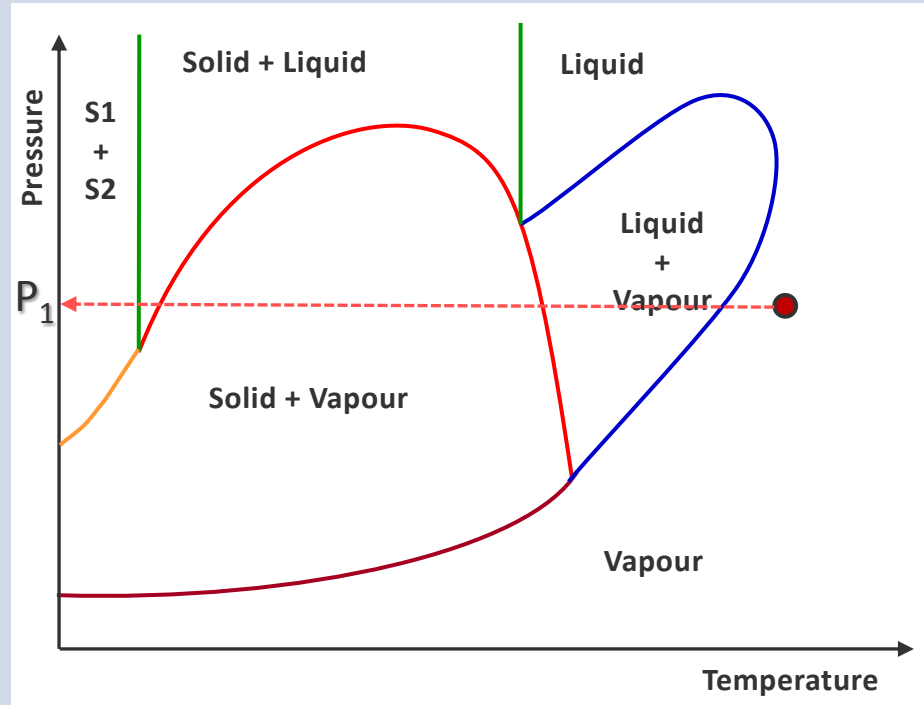
➔ It is necessary to avoid solids deposition that can plug the different parts of equipment in the liquefaction chain (heat exchangers).

➔ The objective is to investigate whether the existing specifications are reflecting the actual freeze out conditions, in order to identify if there is a potential for larger margins towards freeze out in the liquefaction process.

# Fluid phase equilibrium



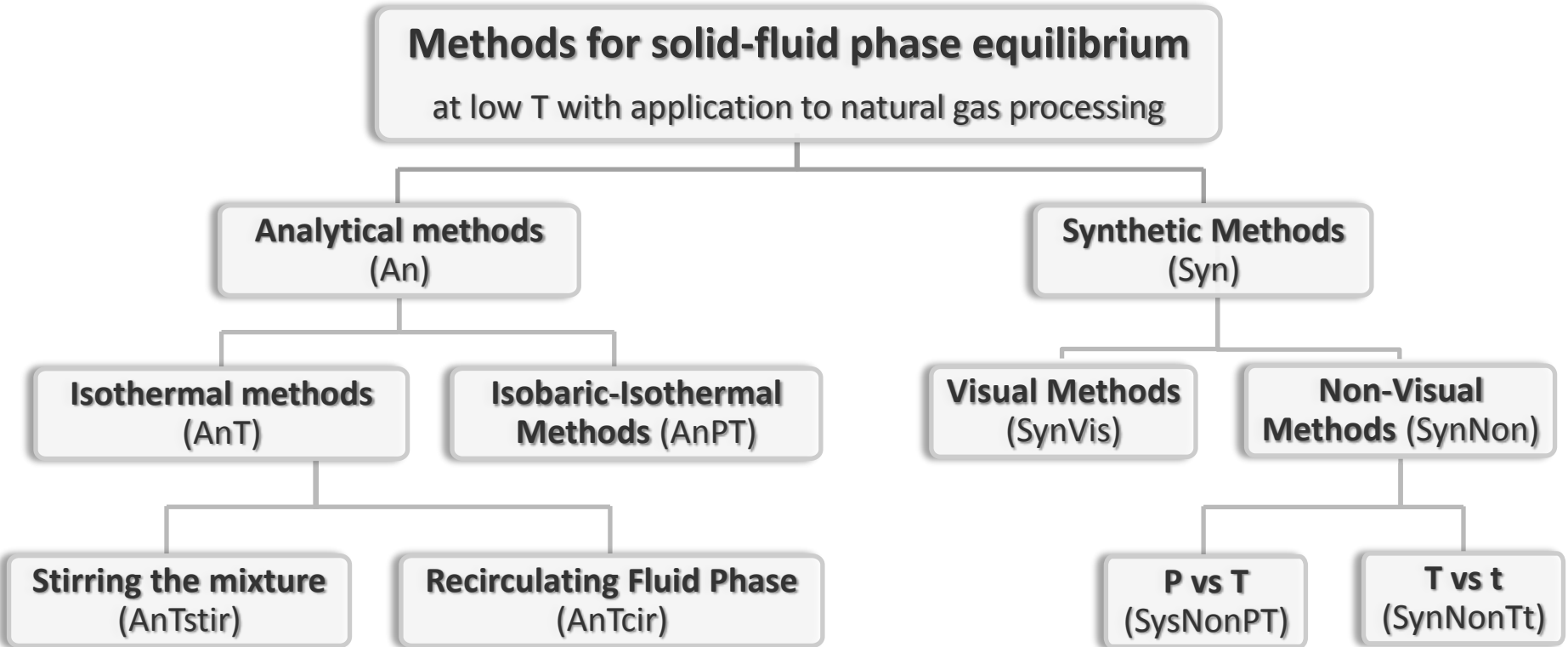
Pure component



Binary mixture

Figure adapted from Donnelly, H. G. and Katz, D. L., *Ind. Eng. Chem.* 1954, Vol. 46 (3), 511-517

# Methodology in the field of solid-fluid measurements



**Reference:** L. Zhang, *Solid-fluid phase equilibria for natural gas processing at low temperatures*, Ph.D., in: Department of Energy and Process Engineering, Norwegian University of Science and Technology, Trondheim, 2012.

# Freeze-out apparatus



## Innovation

both analytical and synthetic methods can be combined for measurements



Custom made for Statoil by Sanchez technologies, was further developed internally.

## Main elements of the rig

- Double envelope container
- Sapphire cell with stirrer and cold finger
- Two pumps for fluid circulation
- Sampling system with ROLSI® valves
- Falcon software for control and data acquisition

## Specifications

Temperature range: -170 – (+40)°C

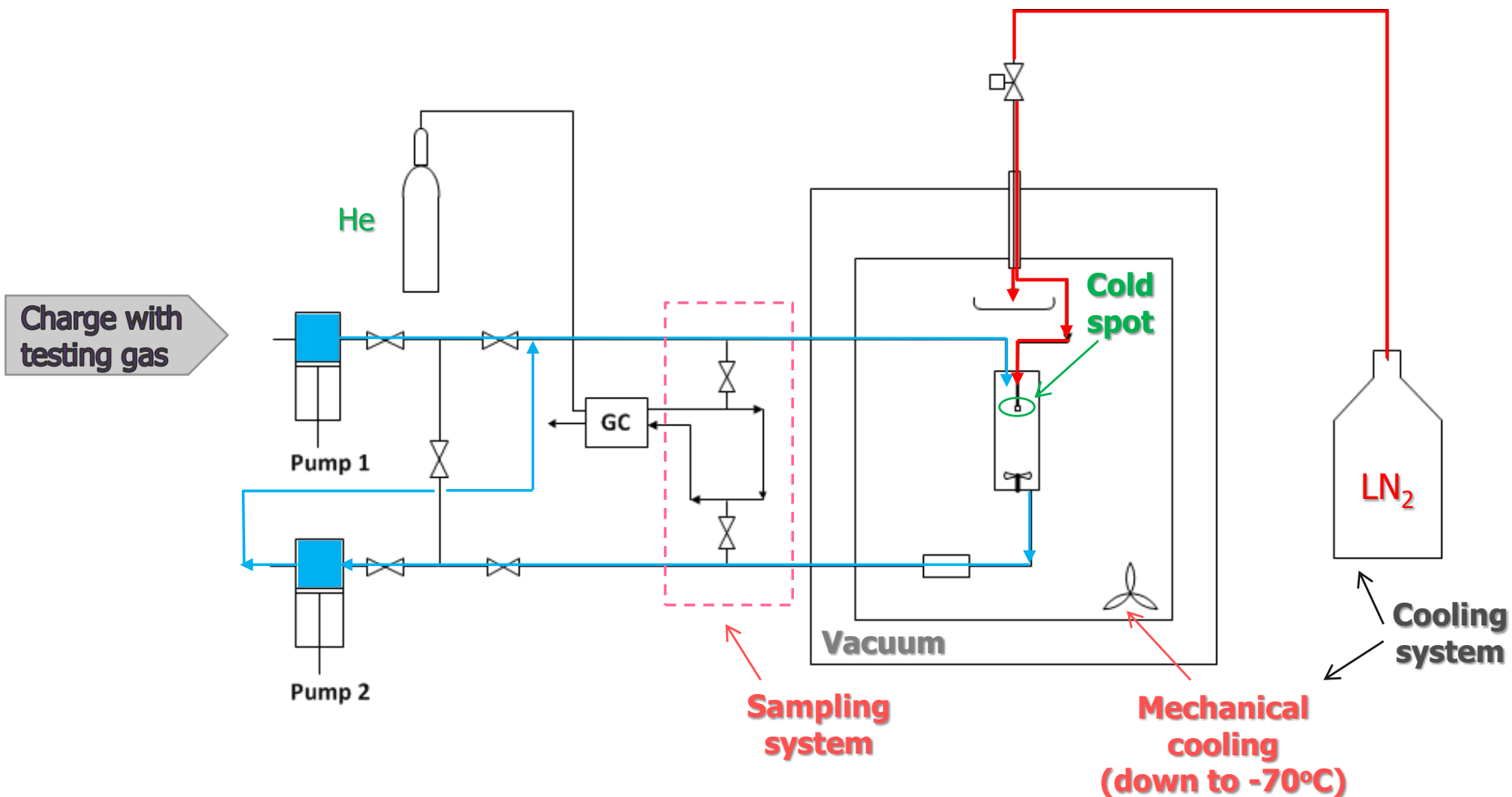
Pressure range: vacuum to 500bar

Sapphire cell volume: 80mL

Cell plus piping volume: 170mL

# Principle of Operation

1. Synthetic method ➡ e.g. keep P const and cool down until solids form
2. Analytical method ➡ Set P, cool down + recirculate + stirring until solids are form.





# Thermodynamic Model

At equilibrium:

$$\left\{ \begin{array}{l} P^\alpha = P^\beta \\ T^\alpha = T^\beta \\ f_i^\alpha = f_i^\beta \end{array} \right.$$

$\alpha, \beta$  are different phases,  
 $i$  is the component

Fluid phase

SRK EoS:  $P = \frac{RT}{v-b} - \frac{a(T)}{v(v+b)}$

$$a = 0.42748 \frac{(RT_c)^2}{P_c} \left[ 1 + m \left( 1 - \left( \frac{T}{T_c} \right)^{0.5} \right) \right]^2$$

with  
vdWaals mixing rule

$$m = 0.48 + 1.57\omega - 0.176\omega^2$$

$$b = 0.08664 \frac{RT_c}{P_c}$$

$$\ln \frac{f_i^a}{x_i P} = \frac{B_i}{B} (z-1) - \ln(z-B) - \frac{A}{B} \left( \frac{2 \sum x_j A_{ij}}{A} - \frac{B_i}{B} \right) \ln \left( 1 + \frac{B}{z} \right)$$

Solid phase

based on the assumption of the  
existence of a sub-cooled liquid  
at the same T, P as the solid:

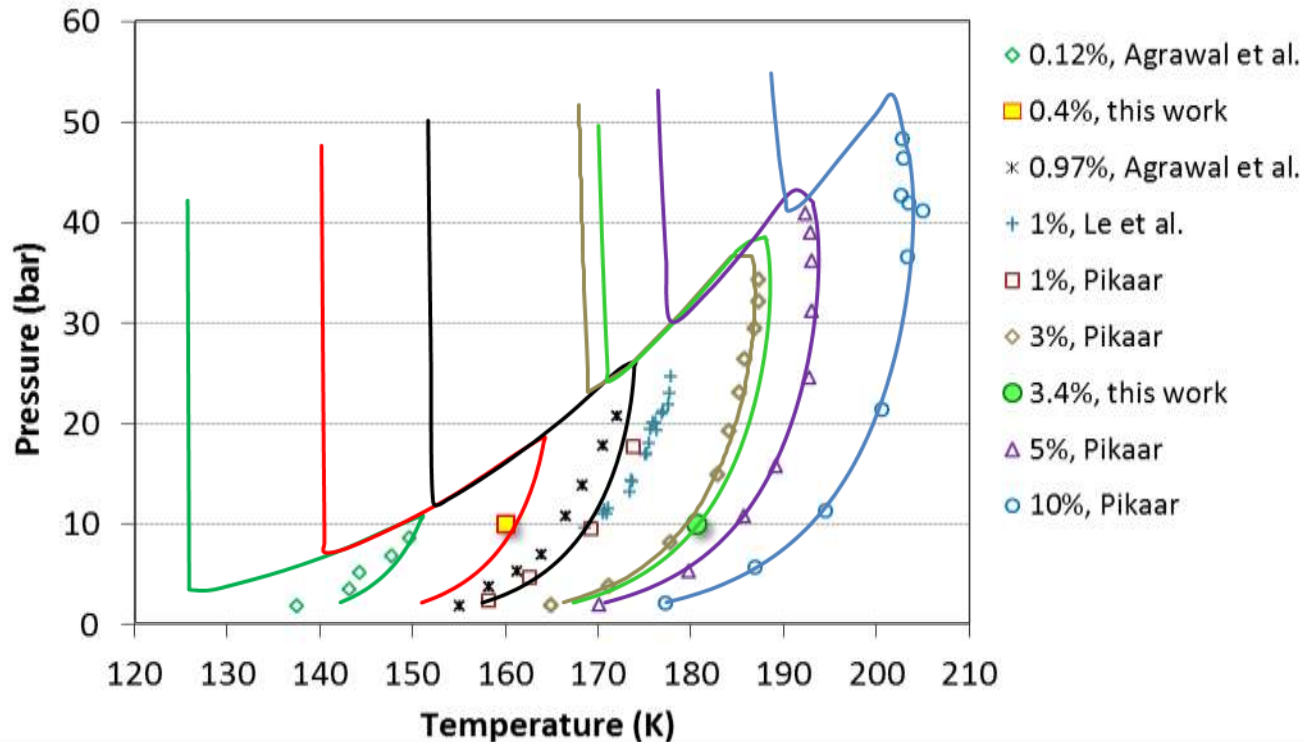
$$\ln \left( \frac{f_i^L}{f_i^S} \right) = \frac{\Delta H_{fus}}{RT_t} \left( \frac{T_t}{T} - 1 \right) - \frac{\Delta C_p}{R} \left( \frac{T_t}{T} - 1 \right) + \frac{\Delta C_p}{R} \ln \frac{T_t}{T}$$

Enthalpy of fusion      Heat capacity difference      Triple point temperature



# Results

- **Measurements were performed for CO<sub>2</sub>/CH<sub>4</sub> mixtures and compared to available literature data**



- ❑ **Two frost points, comparable to the literature experimental data.**
- ❑ **Satisfactory predictions in the solid-vapor range.**

# Conclusions

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- ✓ **The experimental apparatus can successfully be used for solid-vapor equilibrium measurements.**
- ✓ **Further work on the solid-liquid equilibrium and the SLV should be performed so as to verify the overall capabilities of the apparatus.**
- ✓ **Satisfactory predictions in the solid-vapor range with the SRK EoS.**

There's never been a better  
time for **good ideas**

**New Apparatus For Solid-Fluid  
Equilibrium Measurements**

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