

Dynamic permeability due to physical coupling of reactive CO₂-flow and deformation

Nina Simon^{1,2}

Yuri Y. Podladchikov³ and Harald Johansen¹

¹Miljøteknologi, Institutt for Energiteknikk, Kjeller, Norway

²Institutt for geovitenskap, Universitetet i Bergen, Norway

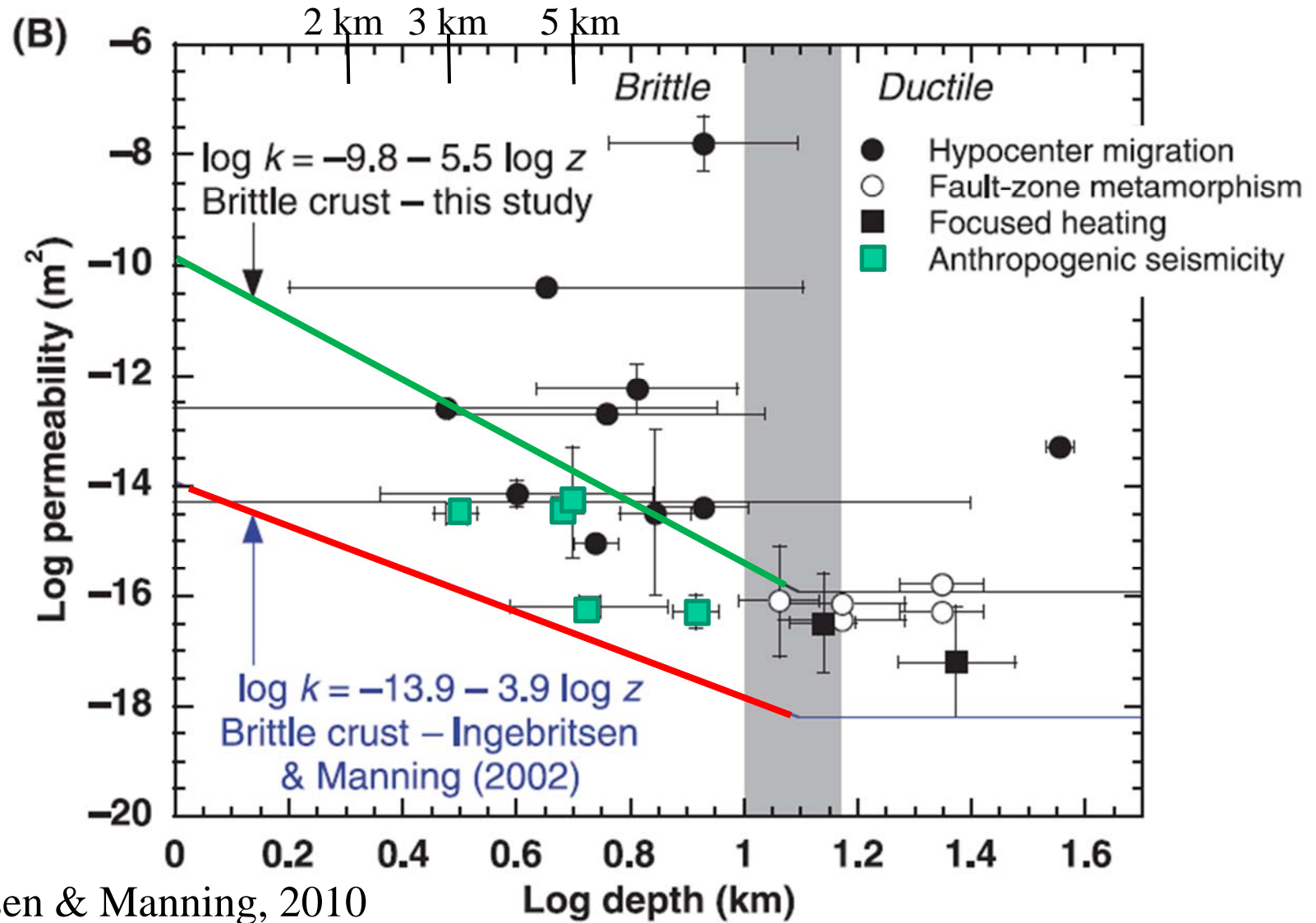
³Faculté des géosciences et de l'environnement, Université de Lausanne, Switzerland



Outline

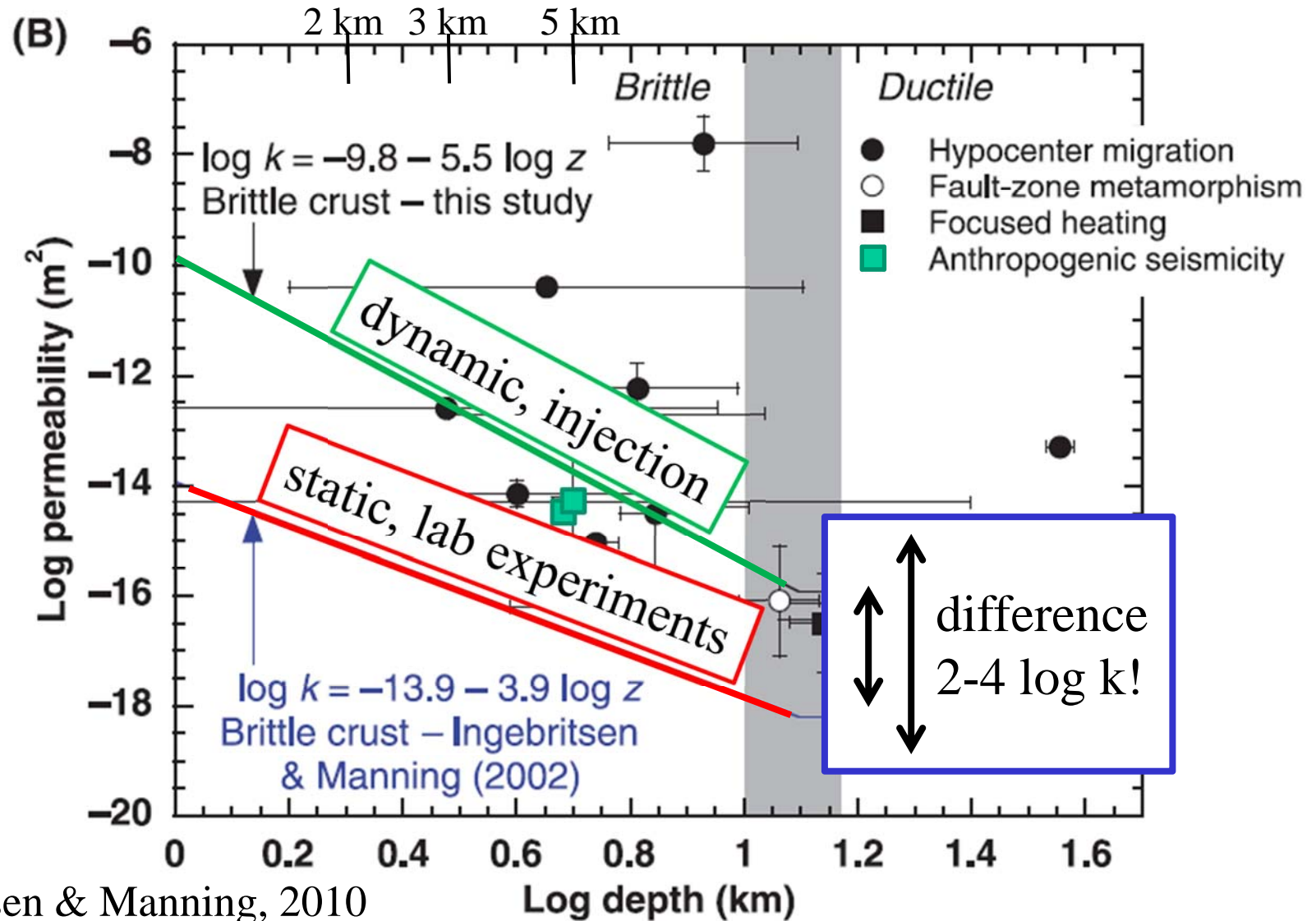
- 1) Evidence for dynamic permeability from data
- 2) What causes dynamic permeability?
 - 1) Permeability variations in space: pre-existing heterogeneity
 - 2) Permeability changes in time (and space):
 - 1) Fracturing/rock failure
 - 2) Dissolution
 - 3) Elastic response to stress changes
 - 4) Compaction: elastic, plastic, viscous
 - 5) Precipitation
- 3) How to model dynamic permeability during flow in a reservoir?
- 4) The porosity wave model: captures opening and closing of porosity as a response to variations in effective pressure (and reactions).
- 5) At which parameters do we expect porosity waves to occur in CO₂ storage operations?

Dynamic permeability: evidence from data



Ingebritsen & Manning, 2010

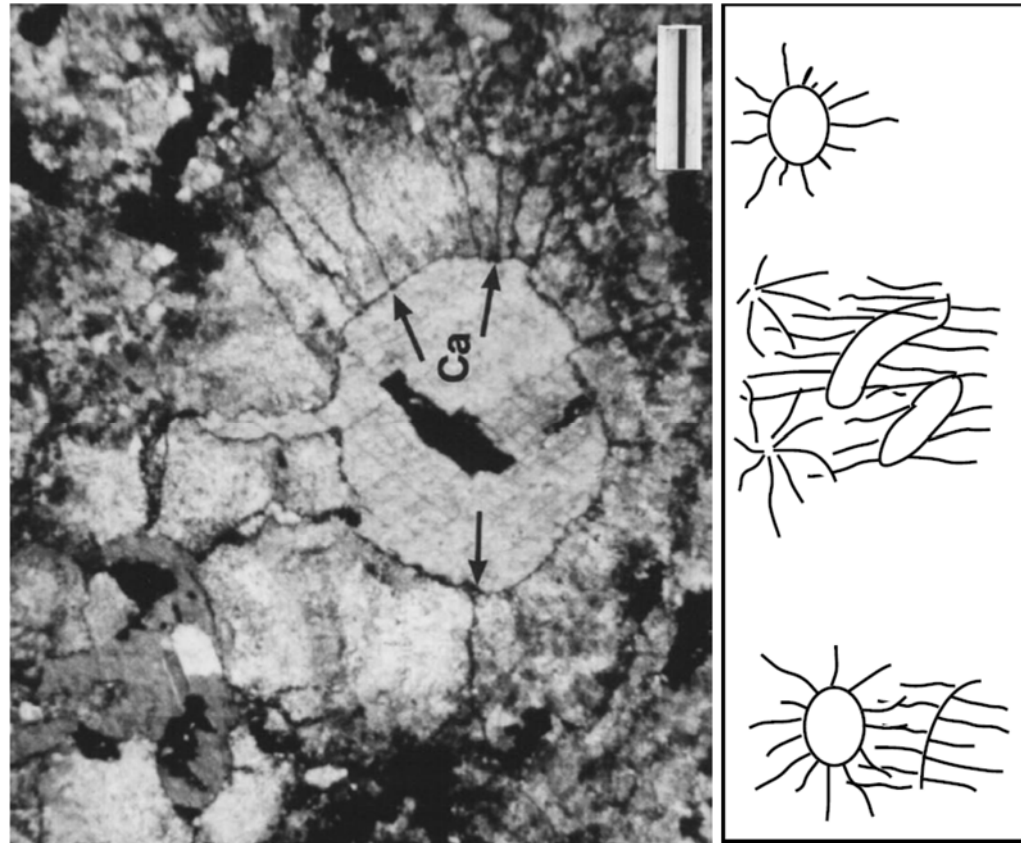
Dynamic permeability: evidence from data



Ingebritsen & Manning, 2010

Opening of pore space: permeability increase

(Micro)fracturing



Radial microfractures Upper Devonian reservoirs, deep Alberta basin (Márquez and Mountjoy, 1996).

Dissolution

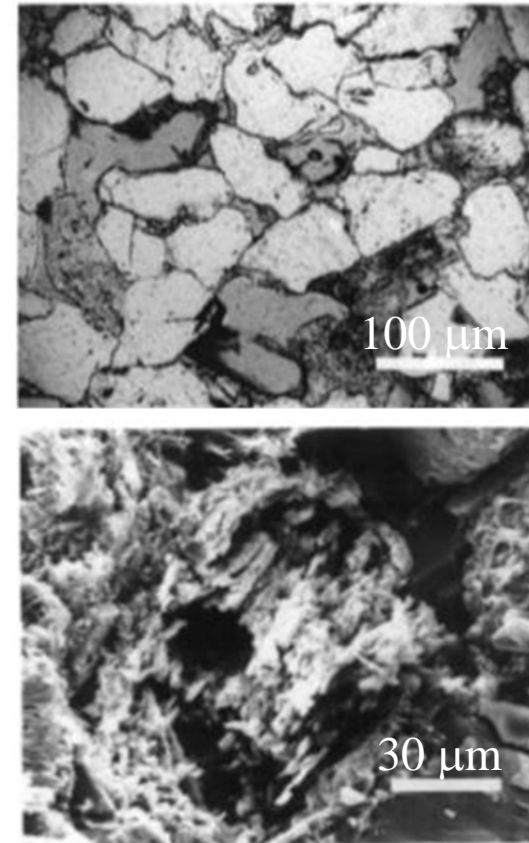


Figure 3—Scanning electron microscopy (SEM) and thin section photomicrographs from well 22/36a-1 showing extensive secondary porosity. (a) Thin section photomicrograph (plane-polarized light) showing several secondary pores after feldspar; scale bar = 100 μm, depth 4665.8 m. (b) SEM photomicrograph showing a highly corroded alkali feldspar; scale bar = 30 μm, depth 4657.2 m.

Wilkinson et al., 1997

Closure of pore space: permeability decrease

Flow-reaction-deformation experiments show closure of pores/fractures by pressure solution creep and compaction

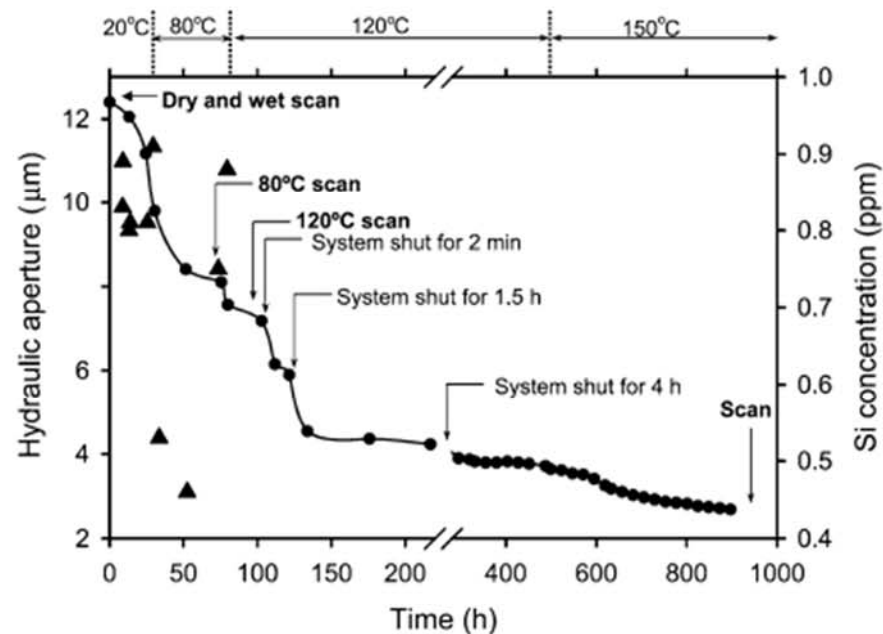


Figure 4

Change in hydraulic aperture with time for a circulation test on a fracture in novaculite. Test is conducted at incremented temperatures but constant stress (POLAK *et al.*, 2003).

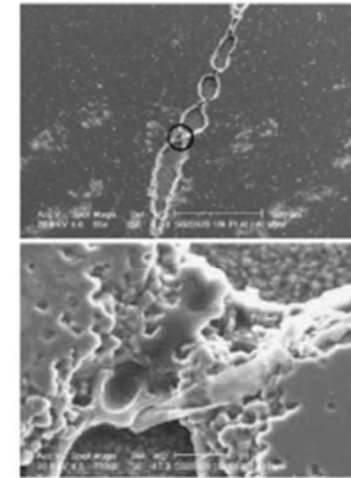


Figure 5

SEM of fracture with dissolution features of solid fracture. Yasuhara *et al.*, 2004

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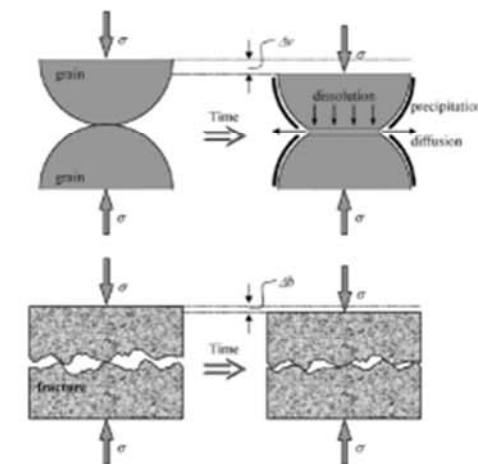


Figure 1. Schematic of pressure solution for twin contacting grains comprising an aggregate and fractured rock comprising a discontinuity. At the contacts the mineral dissolves due to high localized stresses, and dissolved mass diffuses from the interface into the pore space. Finally, precipitation occurs on the free faces of the pore walls.

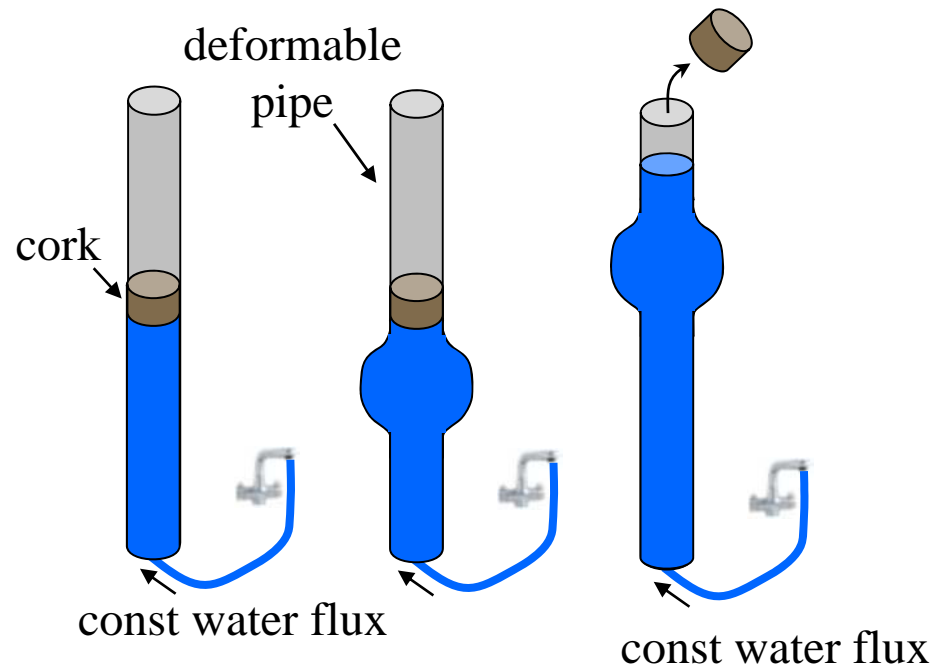
Polak et al., 2003; Yasuhara et al., 2004; Elsworth and Yasuhara, 2006

**What is the effect of coupled fluid flow,
deformation (elastic and microfracturing) and
reactions (chemical compaction)?**

- dynamic opening and closure of pores and
therefore permeability changes**
- dynamic reorganization of flow**

**How can we model all this in ONE continuum
model?**

Porosity waves: fluid flow in a deformable medium



Flow is driven by a pressure difference (in the simplest case buoyancy) and by compaction of the pores. Non-linear coupling between porosity and permeability and permeability and pressure leads to instabilities and focusing of flow.

Equations (and assumptions)

Mass balance $\frac{\partial(1-\varphi)}{\partial t} + \nabla((1-\varphi)v_s) = 0$ $\frac{\partial\varphi}{\partial t} + \nabla(\varphi v_f) = 0$ $\frac{d\rho_s}{dt} = \frac{d\rho_f}{dt} = 0$

solid fluid

Force balance $\frac{\partial \bar{\sigma}_{ij}}{\partial x_j} = \frac{\partial \sigma_{ij}^{eff}}{\partial x_j} - \frac{\partial p_f}{\partial x_i} = g \left[(1-\varphi)\rho_s + \varphi\rho_f \right] \hat{z}$ $P_{eff} = P_f - \bar{P}$

Darcy's law $\varphi(v_f - v_s) = -\frac{k(\varphi)}{\mu_f} \nabla(p_f + \rho_f g z)$

Rheology $\frac{1}{\varphi(1-\varphi)} \frac{d\varphi}{dt} = \underbrace{\frac{P_{eff}}{\eta(\varphi, P_{eff})}}_{\text{visco-plastic}} + \underbrace{\frac{1}{\beta(\varphi)} \frac{dP_{eff}}{dt}}_{\text{elastic}}$ Yarushina, 2010

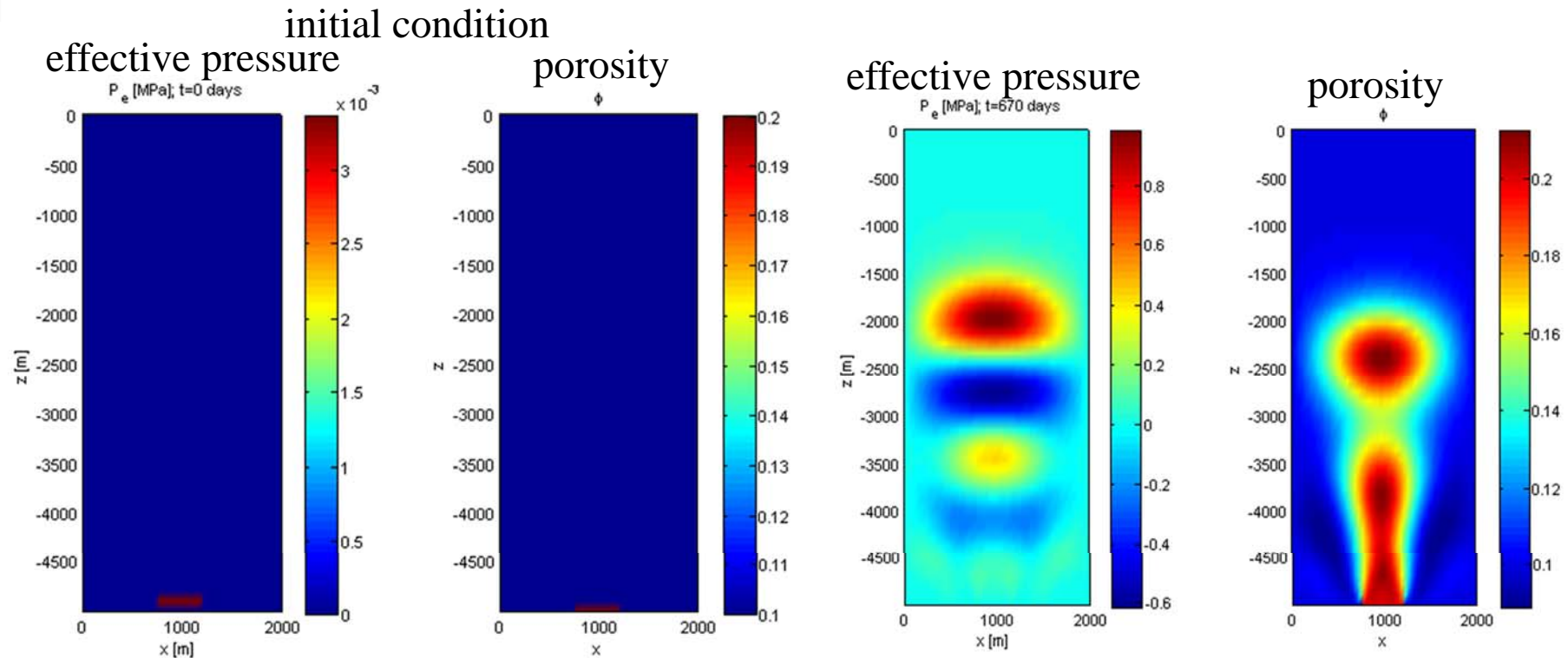
Simplified and in 1D: 2 equations, 2 unknowns

I $\frac{\partial\varphi}{\partial t} = -\frac{\partial}{\partial z} \left(\frac{k(\varphi)}{\mu_f} \cdot \left(\frac{\partial P_e}{\partial z} + \Delta\rho g \right) \right)$ II $\frac{\partial P_e}{\partial t} = \frac{1}{\beta(\varphi)} \left(\frac{\partial\varphi}{\partial t} - \frac{P_e}{\eta(\varphi)} \right)$

$$k(\varphi) = k_0 \cdot \left(\frac{\varphi}{\varphi_0} \right)^n, \quad n = 3; \quad \beta(\varphi) = \varphi^b \cdot \beta_0, \quad b = 1/2 \quad \text{and} \quad \eta(\varphi) = \eta_s / \varphi^m, \quad m = 1.$$

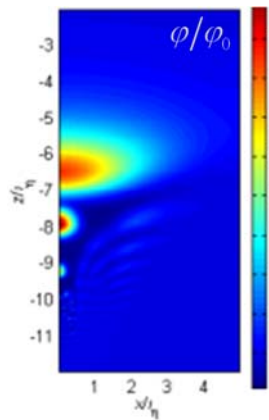
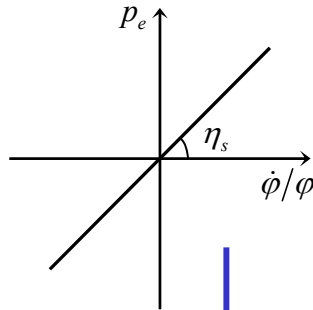
Modeling deformation and fluid flow

visco-elastic porosity waves, 2D



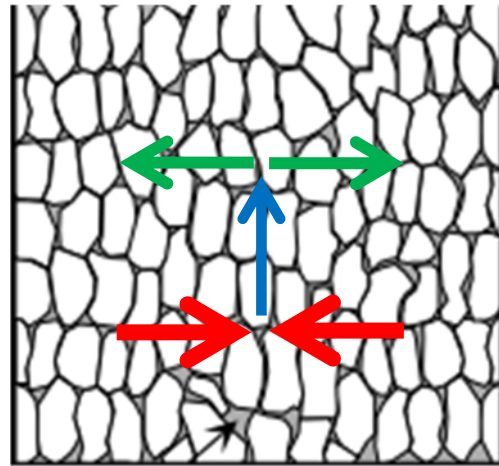
Rheology: opening of pores much easier than closure

Viscous linear

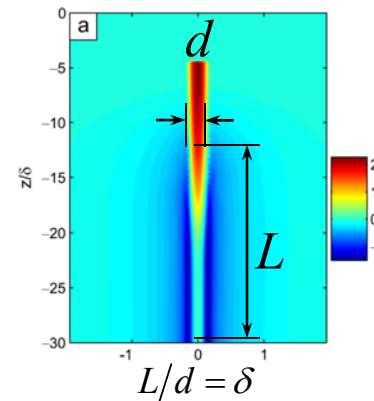
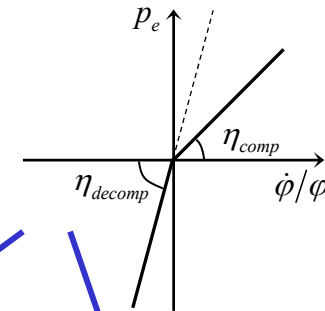


from 'blob'
to 'jet'
(or channel)

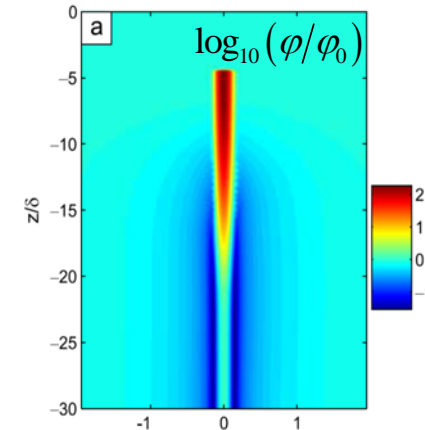
Connolly & Podladchikov, 1998



Viscous bilinear

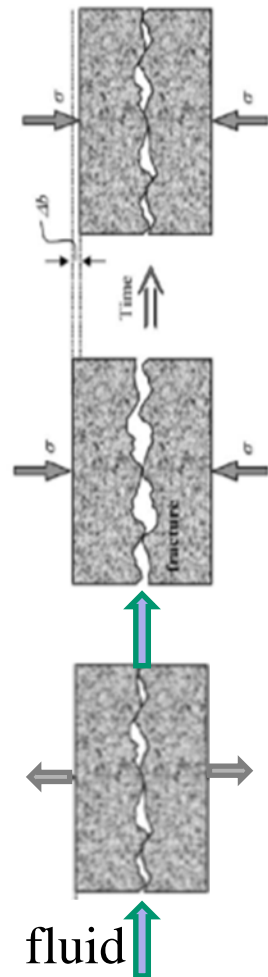


$$\delta = f(\eta_{comp}/\eta_{decomp})$$



Connolly & Podladchikov, 2007

Modeling deformation and fluid flow



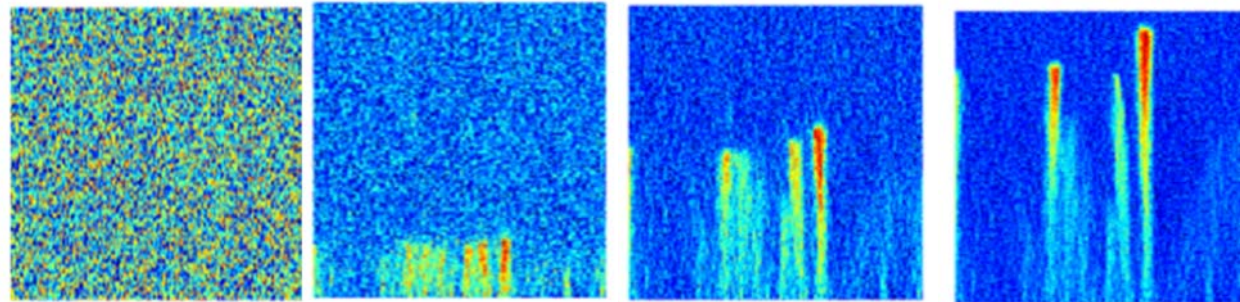
Porosity ϕ

1

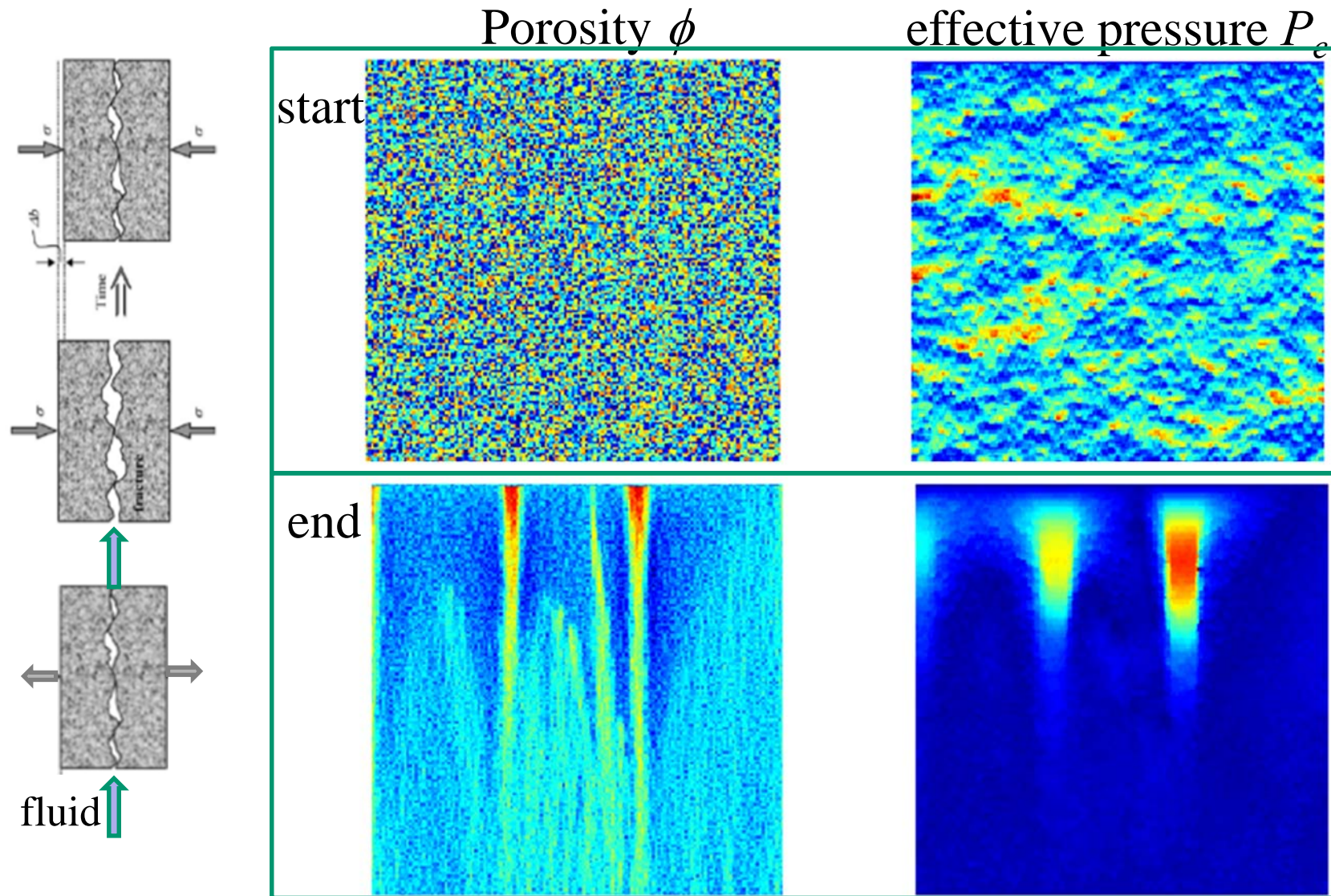
2

3

4



Modeling deformation and fluid flow



Porosity waves: relevant for CO₂ storage?

Dimensional analysis and parameter-check

Characteristic length-scale: compaction length $L^* = \sqrt{\frac{k_0 \eta_s}{\varphi_0 \mu_f}}$

Characteristic pressure $p^* = \Delta \rho g^* L^*$

Characteristic time $t^* = \frac{\eta_s}{p^*}$

with $k_0 \approx 10^{-15} m^2$, $\varphi_0 \approx 0.1$, $\mu_f \approx 10^{-4} Pa \cdot s$ we need

$$\eta_s \approx 10^{15} Pa \cdot s$$

to get $L^* = 100m$ and $t^* = 21 years$

If $\eta_{decomp} = 0.1 - 0.0001 \eta_{comp}$, and/or p^* is higher than buoyancy pressure, timescales will reduce significantly.

Reaction-induced viscosity from experiments

Le Guen et al., 2007

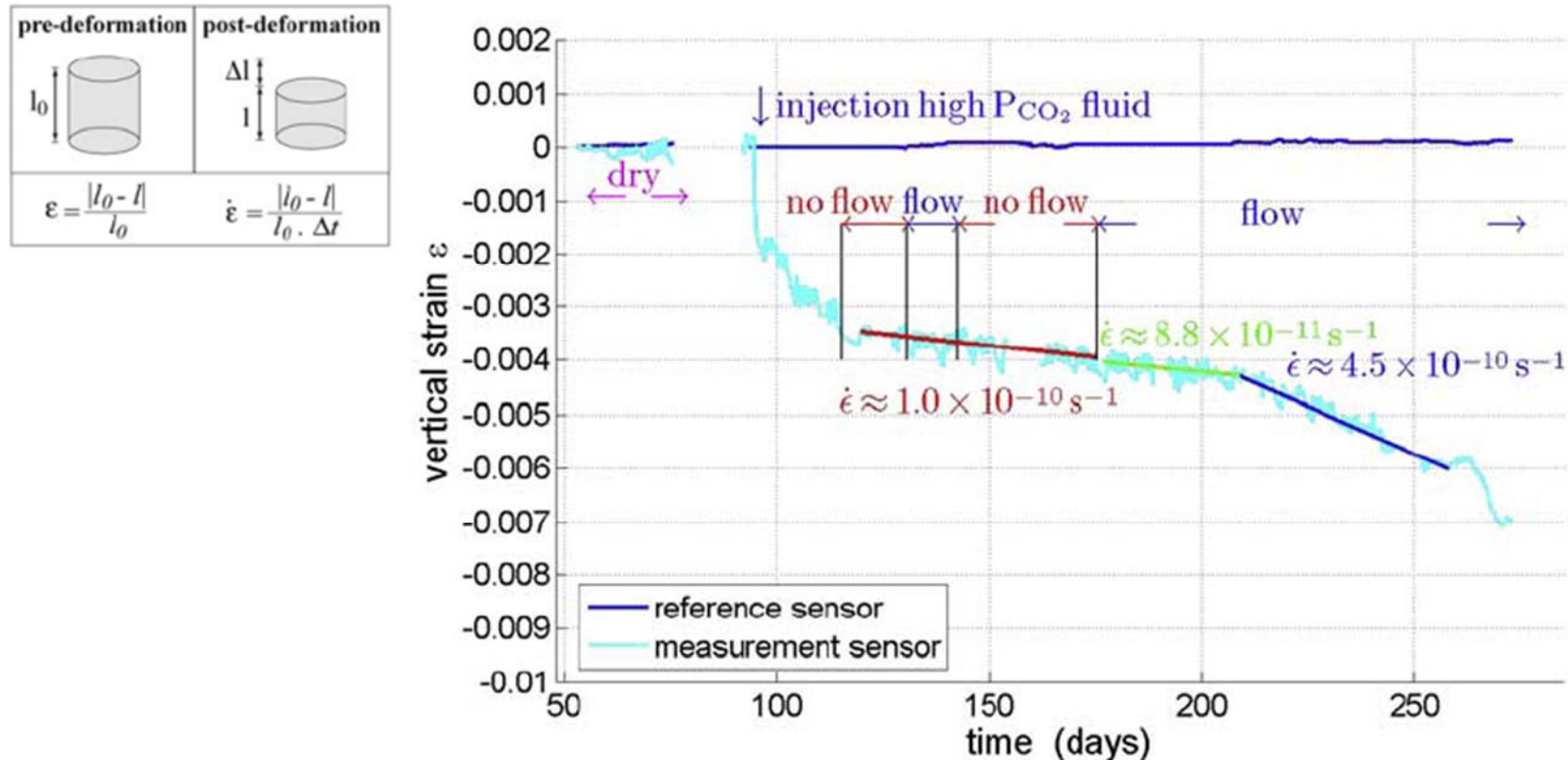


Figure 5. Vertical axial strain deformation measured for Lavoux W526 sample in the absence of fluid and during injection of high P_{CO_2} saline fluid (cyan curve). Time periods with no data represent non-stable conditions associated with parameter changes. The red time period $\dot{\epsilon}$ includes a short flow period. Note that the renewed injection of high P_{CO_2} saline solution caused a large increase in $\dot{\epsilon}$, but after time lag of ≈ 40 days. The end of the experiment was marked by a sudden, rapid increase in strain and strain rate.

Reaction-induced viscosity from experiments

Le Guen et al., 2007

Table 2. Experimental Parameters During Compaction

Rock sample	Estailades		Lavoux W526	Lavoux W520	Sandstone
Fluid P_{CO_2}	low P_{CO_2}	high P_{CO_2}	high P_{CO_2}	low P_{CO_2}	high P_{CO_2}
σ_1 (MPa)	8.9	10.0	16.3	16.3	16.0
σ_3 (MPa)	7.3	8.5	12.0	11.6	10.2
p_f (MPa)	5.9	7.8	7.9	7.9	8.3
σ_c (MPa)	3.0	2.2	8.4	8.4	7.7
P_{CO_2} (MPa)	$10^{-4.5}$	7.8	7.9	$10^{-4.5}$	8.3
T ($^{\circ}\text{C}$)	25	80	40	40	40
[NaCl] (mol l^{-1})	0	0	10^{-2}	10^{-2}	10^{-2}
Fluid flow ($\text{m}^3 \text{s}^{-1}$)	8.33×10^{-11}	8.33×10^{-11}	8.33×10^{-11}	8.33×10^{-11}	8.33×10^{-11}
Residence time (h)	20.5	20.5	12.8	14.0	10.0
Fluid velocity (m s^{-1})	6×10^{-7}	6×10^{-7}	1×10^{-6}	9×10^{-7}	1.4×10^{-6}

Table 3. Average Strain Rates With Indicated Time Ranges

	Dry (s^{-1})	Low P_{CO_2} fluid flow (s^{-1})	Low P_{CO_2} no flow (s^{-1})	High P_{CO_2} fluid flow (s^{-1})	High P_{CO_2} no flow (s^{-1})
Estailades	1.0×10^{-12} days 35–58	1.9×10^{-11} days 198–221	—	1.0×10^{-10} days 366–370	3.0×10^{-11} days 475–495
Lavoux-W526	≈ 0 day 53–74	—	—	4.5×10^{-10} day 209–258	1.0×10^{-10} day 120–175
Lavoux-W520	1.1×10^{-11} day 26–41	2.6×10^{-10} day 231–282	8.1×10^{-11} day 200–230	—	—
Sandstone	—	—	—	2.3×10^{-11} day 59–134	4.6×10^{-12} day 153–161

Reaction-induced viscosity from experiments

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P_{CO_2} (MPa)	10^{-4}			$10^{-4.5}$	8.3
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Residence time (h)	20.5			14.0	10.0
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Linear viscosity:

$$\sigma = \mu \cdot \dot{\epsilon}$$

$$\mu = \sigma / \dot{\epsilon}$$

$$\mu = 16 \cdot 10^6 \text{ Pa} / 2.3 \cdot 10^{-11} \text{ s}^{-1}$$

$$\mu \approx 10^{17} \text{ Pa} \cdot \text{s}$$

at 40°C for sandstone

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Summary

- Permeability is expected to change dynamically in a reservoir during flow, in particular if reactive CO₂-rich fluids are involved.
 - Coupling between flow, reactions and deformation leads to effectively visco-elasto-plastic rheology.
 - Fluid focusing due to non-linear coupling leading to instabilities can be modeled as porosity waves.
 - Preliminary results indicate that porosity waves/ fluid focusing and enhanced transport may occur in reservoir operations, in particular in low-permeability rocks.
- ➔ This may enhance injectivity, but also increase the risk for leakage.
- ➔ We need more theoretical and experimental investigations of coupled fluid flow, reactions and deformation, and comparison to reservoir data.

