

Scenario Modelling to Support Monitoring Plans for CO₂ Storage Sites

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British
Geological Survey

NATURAL ENVIRONMENT RESEARCH COUNCIL



Background



- Most jurisdictions require a CO₂ storage site's operator to plan for measurement, monitoring and verification (MMV).
- In Europe, this requirement is specified in EC Directive 2009/31/EC (the 'Storage Directive').
- The UK needs to determine priority technologies and methodologies to enable effective MMV in offshore areas, where CO₂ storage is planned.
- The UK's Energy Technologies Institute (ETI) instigated a project to review UK legislative and technical requirements for MMV, and determine future development priorities.



Aims of Scenario Modelling

- Essential MMV goals are to determine that:
 - the storage system behaves as expected
 - the defined storage complex does not leak CO₂

- Overall project goals included determining:
 - whether each available monitoring technique can identify unexpected abnormal behaviour of stored CO₂
 - under what circumstances

- Scenario modelling aimed to inform evaluations of monitoring techniques by:
 - illustrating hypothetical consequences of abnormal behaviour and CO₂ leakage
 - exploring how quantitative metrics (e.g. amounts of water and free CO₂, pressure etc) might vary in these circumstances

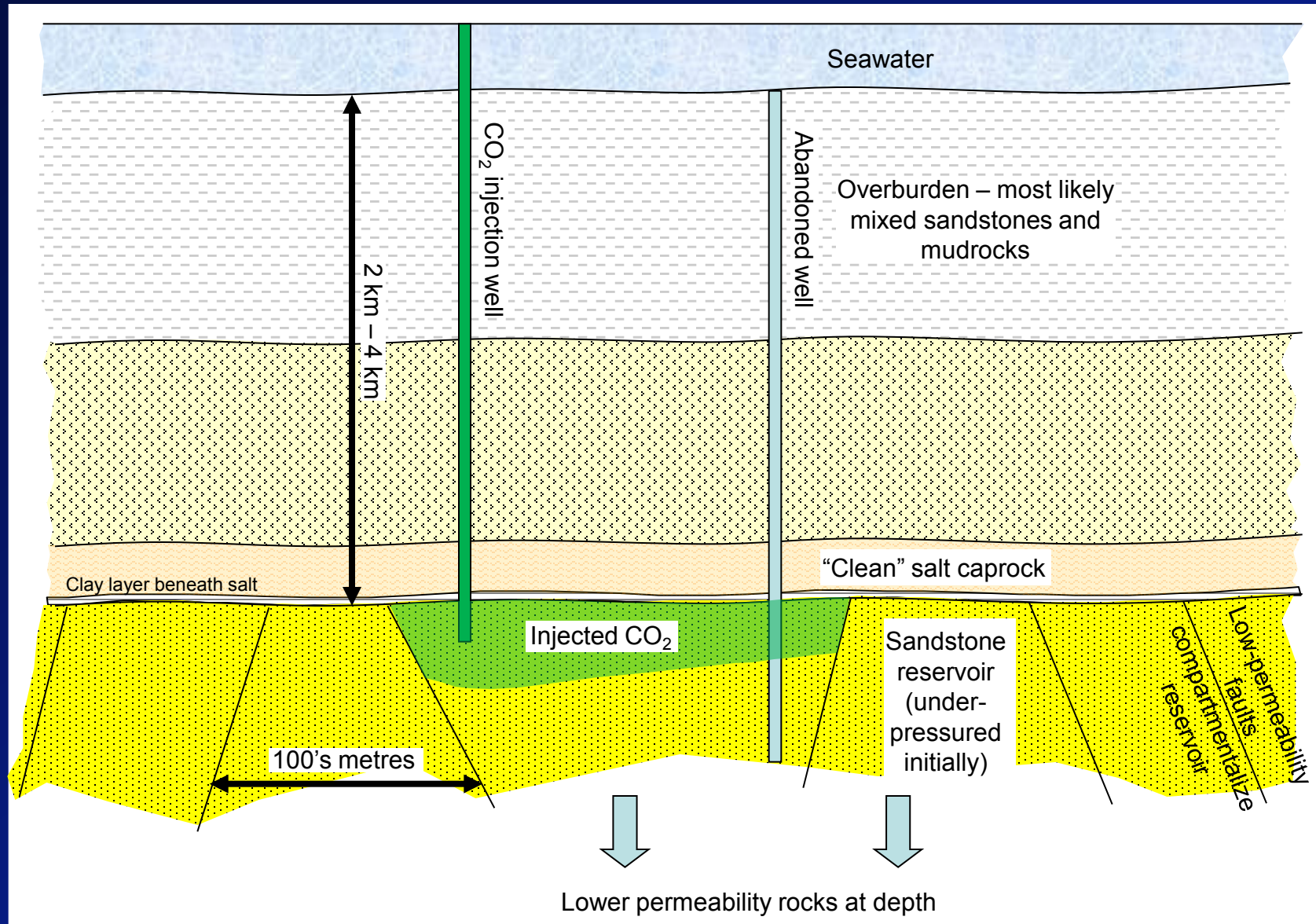
Workshop
Attended
by
Quintessa,
BGS, TNO

Explore hypothetical leakage scenarios using systems models

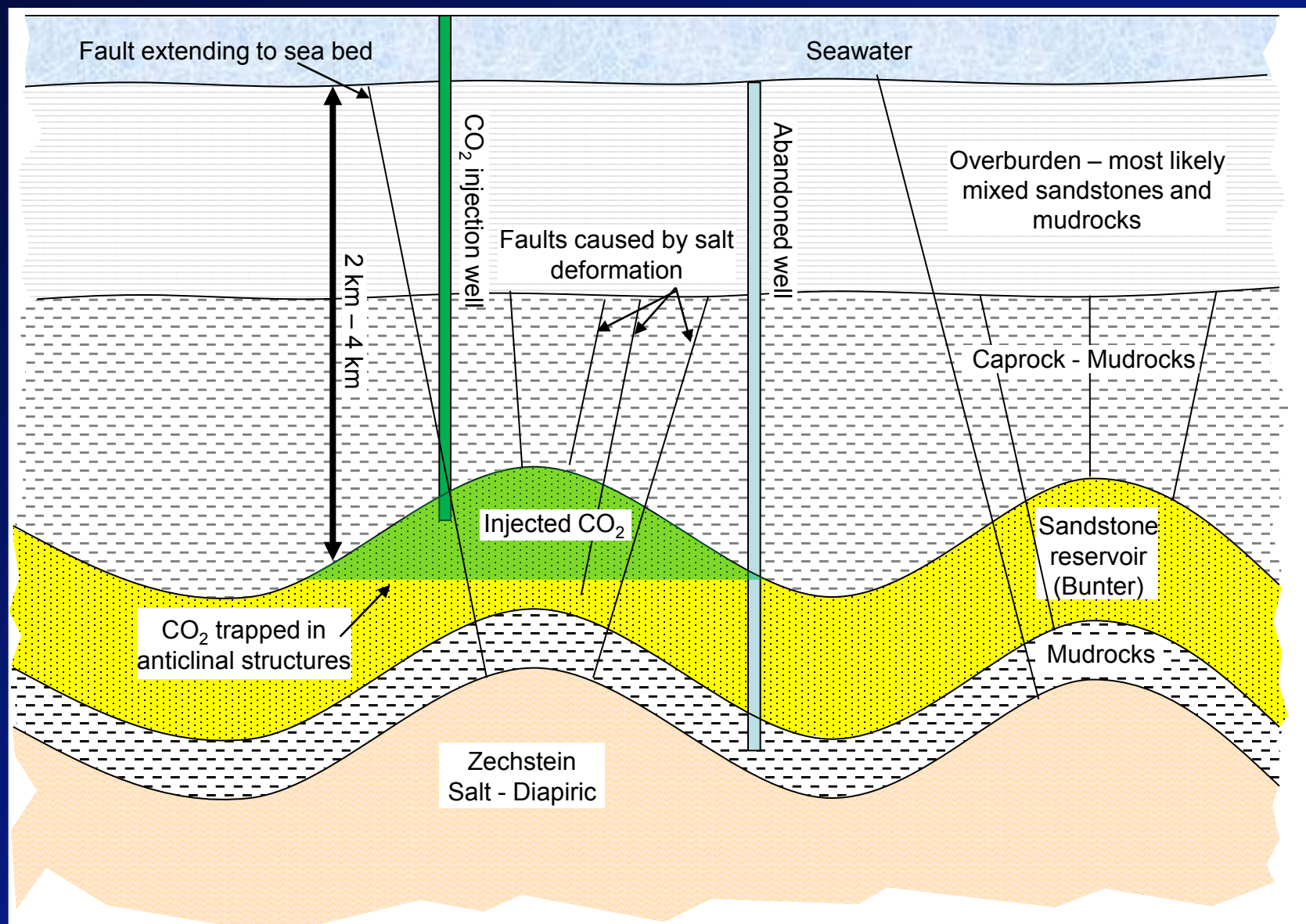
- Standard “check-list”
- Ensure nothing significant missed
- Freely accessible

<http://www.quintessa.org/co2fepdb>

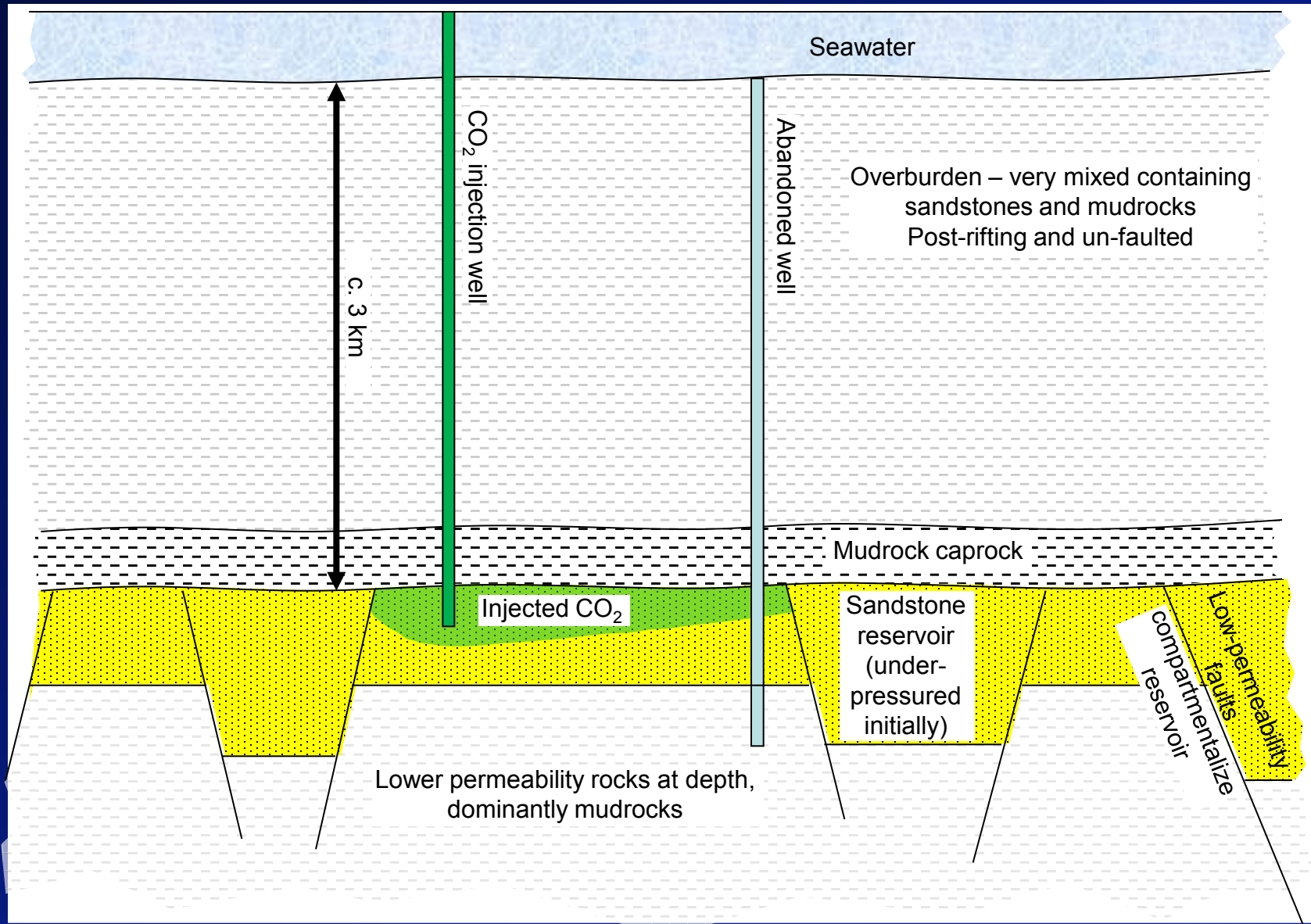
Storage Site Type 1 (S North Sea)



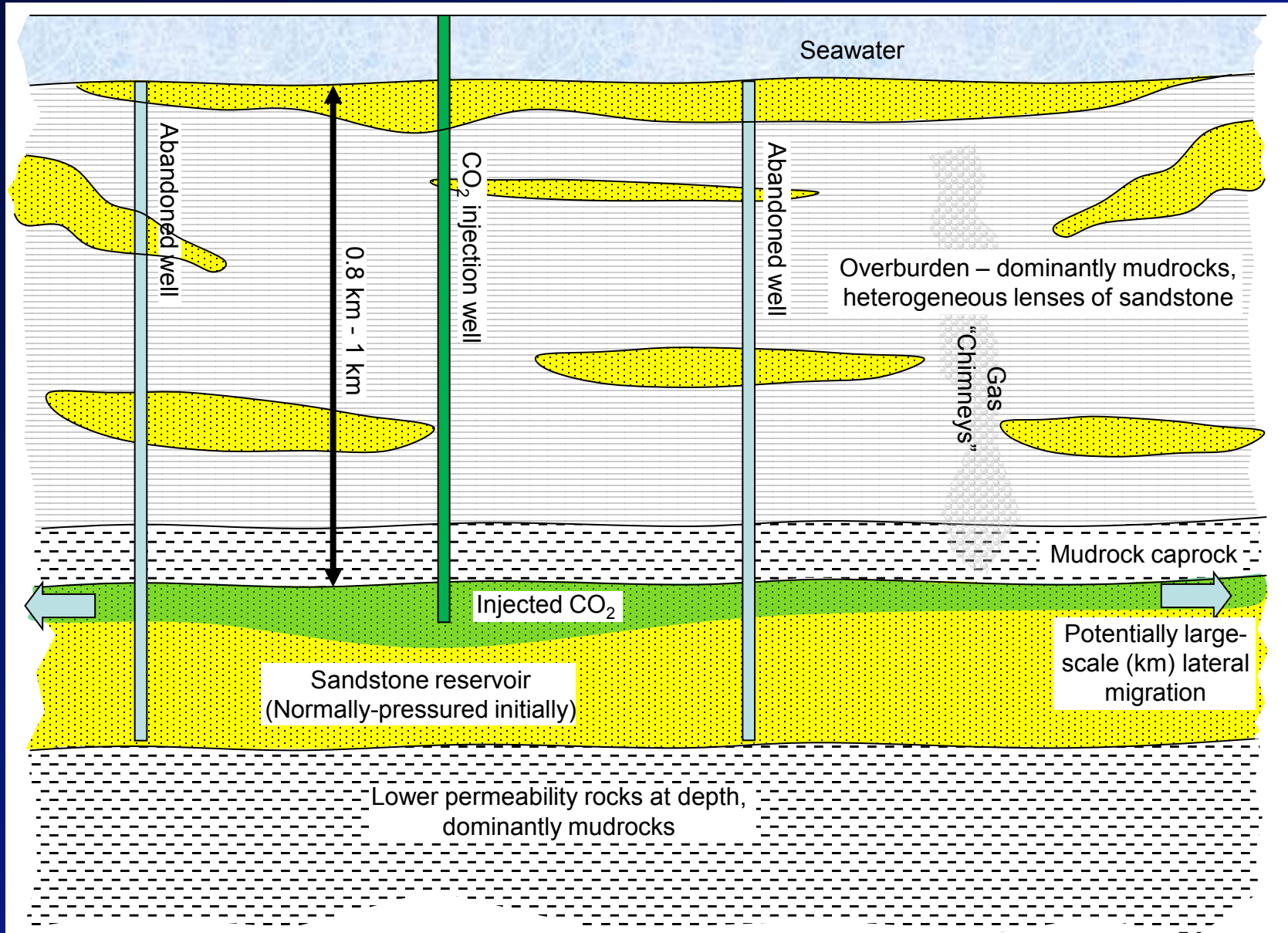
Storage Site Type 2 (S North Sea)



Storage Site Type 3 (Central, Northern N Sea)



Storage Site Type 4 (Central, Northern N Sea)



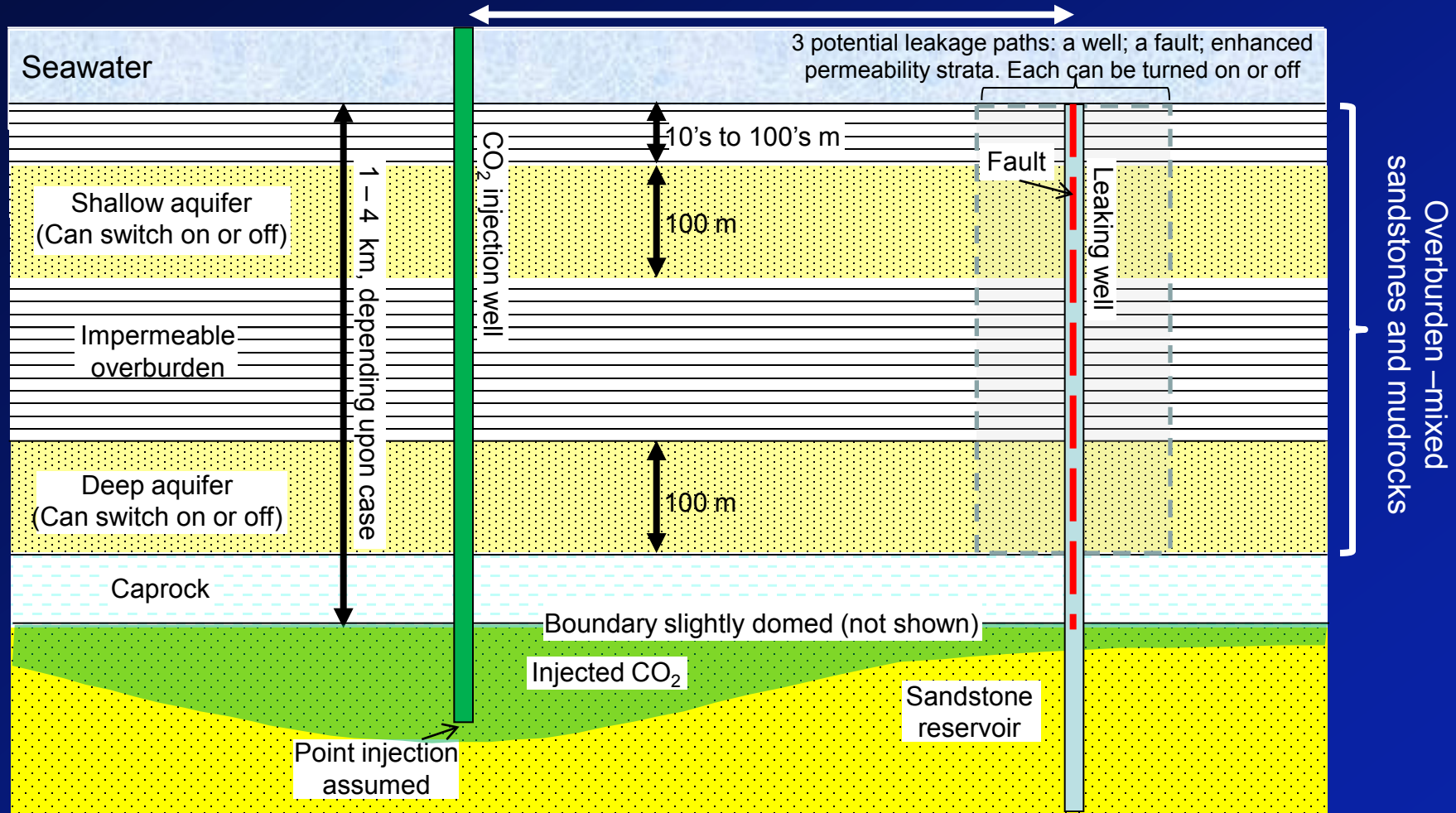
Scenarios



- In the hypothetical case that CO₂ can leak upwards, the most likely pathways are:
 - a well (1D path, “well leakage scenario”)
 - a fault (2D path, “fault leakage scenario”)
 - enhanced-permeability rock zone (3D path, “enhanced permeability overburden scenario”) representing
 - heterogeneously distributed interconnected permeable strata within dominantly impermeable overburden
 - or a gas chimney
 - the caprock, over wide area (“leaking caprock scenario”)
- Common features of scenarios:
 - reservoir
 - impermeable caprock
 - impermeable overburden containing a “deep aquifer” and a “shallow aquifer”
 - seawater at the top boundary
 - injection well

Basic Systems Model

Calculated to be consistent with plume extent after 10 years of injection



Lower permeability rocks at depth – represent by no-flow boundary
For each kind of site, each kind of leakage path placed same distance from injection well

Model Cases

➤ Case 1 –

- relatively deep brine-filled reservoir brine
- initial, pre-injection CO₂ pressure below hydrostatic
- final reservoir fluid pressure hydrostatic

➤ Case 2 –

- relatively shallow saline water-filled reservoir
- initial, pre- injection CO₂ pressure is hydrostatic pressure
- end-injection reservoir fluid pressure slightly >hydrostatic
- decreases rapidly to hydrostatic

➤ Case 3 –

- relatively shallow brine-filled reservoir
- initial pre-injection CO₂ pressure hydrostatic pressure
- final reservoir fluid pressure just below (85%) of lithostatic

3 pathways
considered for
each case:

Case 1_Well
Case 1_Fault
Case 1_Cap
etc

Site / Scenario / Case Correspondence

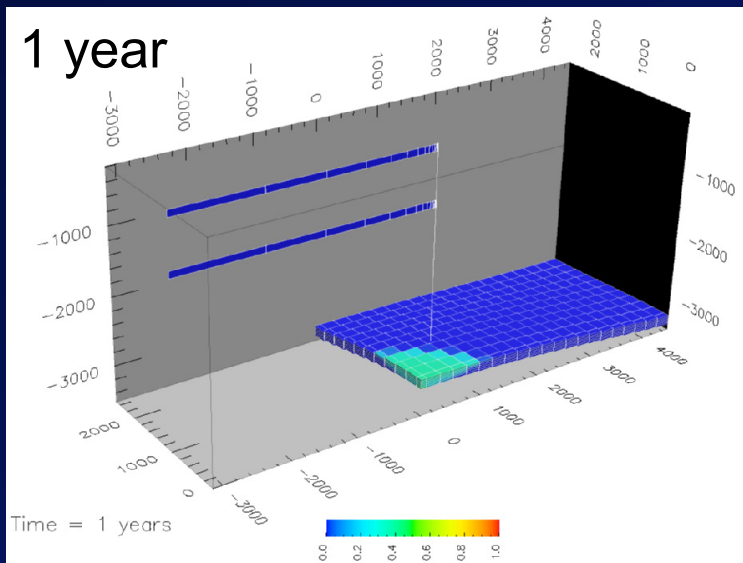
Simulations with generic systems model				Corresponding Storage Site			
Cases				Southern North Sea Type 1	Southern North Sea Type 2	Central & Northern North Sea Fault Block-type Type 3	Central & Northern North Sea Aquifer Type 4
Case	Initial reservoir pressure	Final reservoir pressure	Injection duration				
Leaking well scenario							
1_Well	Under-pressured	Hydrostatic	50 years	Correspondence	Correspondence	Correspondence	None
2_Well	Hydrostatic	Hydrostatic+	50 years	Weak correspondence	Correspondence	Correspondence	Correspondence
3_Well	Hydrostatic	Sub-lithostatic	50 years	Weak correspondence	Correspondence	Correspondence	Weak Correspondence
Leaking fault scenario							
1_Fault	Under-pressured	Hydrostatic	50 years	None	Correspondence	None	None
2_Fault	Hydrostatic	Hydrostatic+	50 years	None	Correspondence	None	None
3_Fault	Hydrostatic	Sub-lithostatic	50 years	None	Correspondence	None	None
Leaking caprock and enhanced overburden permeability scenario							
1_Cap	Under-pressured	Hydrostatic	50 years	None	Correspondence	None	None
2_Cap	Hydrostatic	Hydrostatic+	50 years	None	Correspondence	None	Correspondence
3_Cap	Hydrostatic	Sub-lithostatic	50 years	None	Correspondence	None	None

Modelling Software

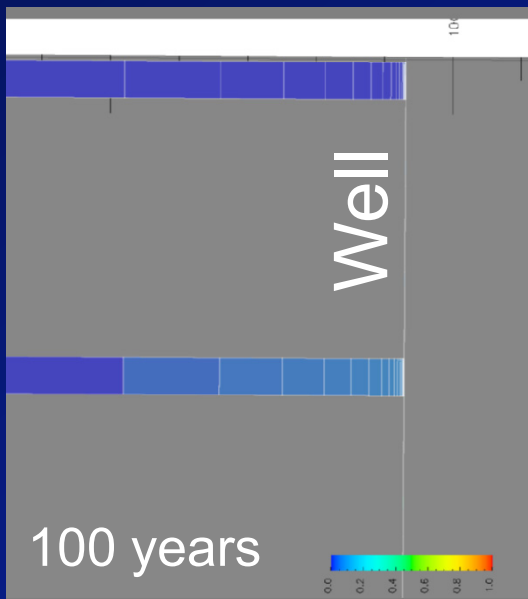
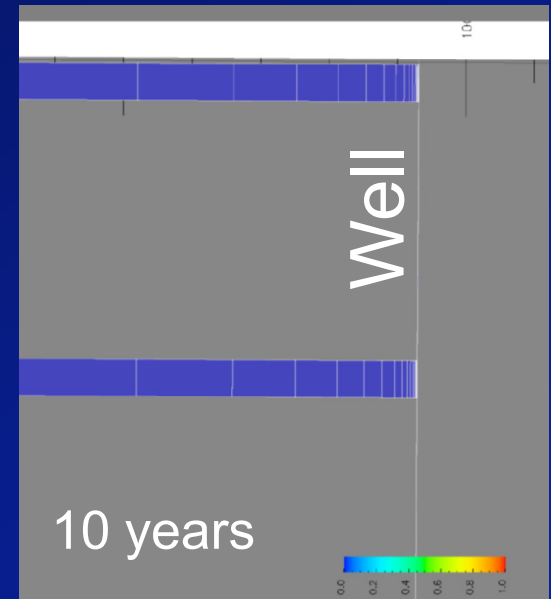
- Quintessa's QPAC software:
 - General-purpose modelling tool
 - Solves wide-ranging problems, including strongly-coupled, non-linear processes
- Allows modeller to define included processes:
 - Thermal
 - Hydrogeological (Darcy Flow, Multi-Phase Flow etc)
 - Mechanical
 - Reactive Transport
 - Solute Transport
 - a 'systems-level'
 - 'detailed' research-level



Well Leakage Scenario, Case 1_Well

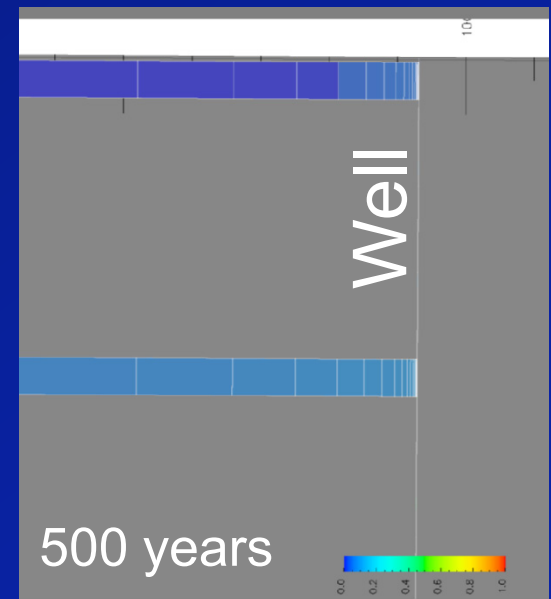


Buoyancy only
driving force



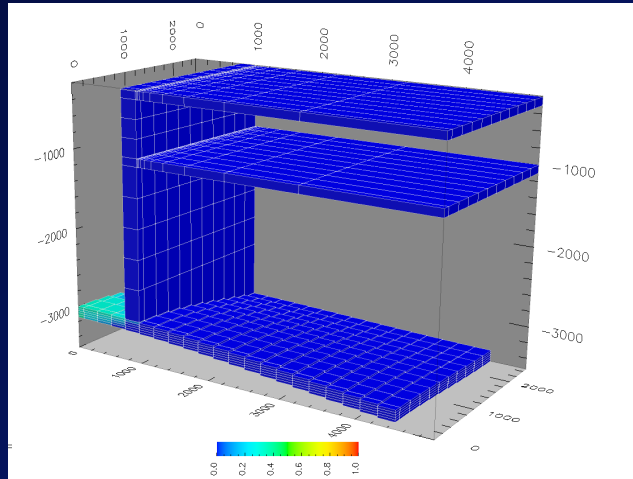
CO₂ Saturation

- Significant CO₂ enters aquifers (esp. lower aquifer)
- Explained by large CO₂ surface area per unit volume flowing

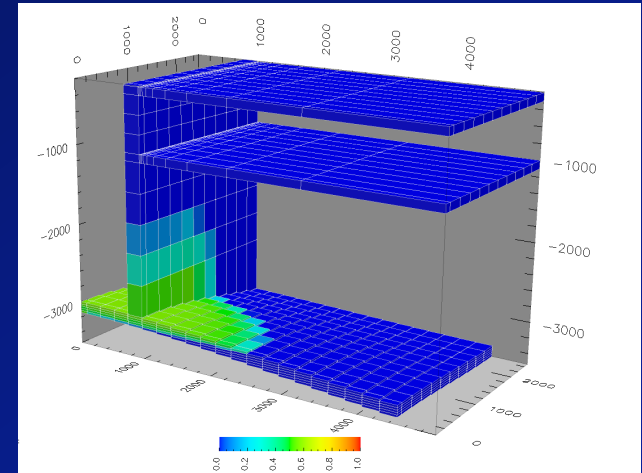


Fault Leakage Scenario, Case 1_Fault

1 year

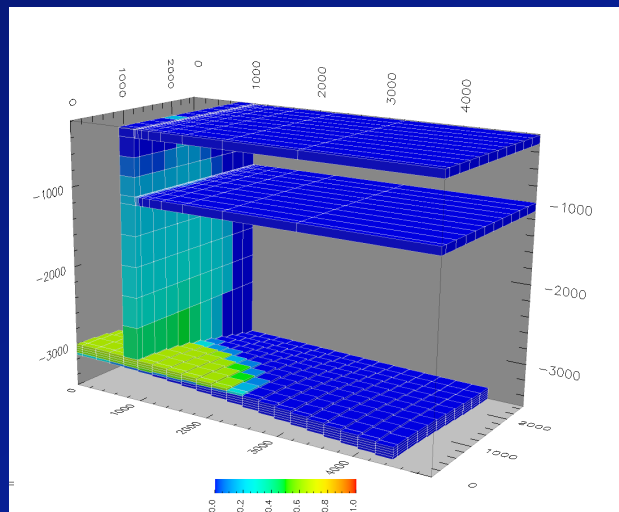


50 years



CO₂ Saturation

400 years

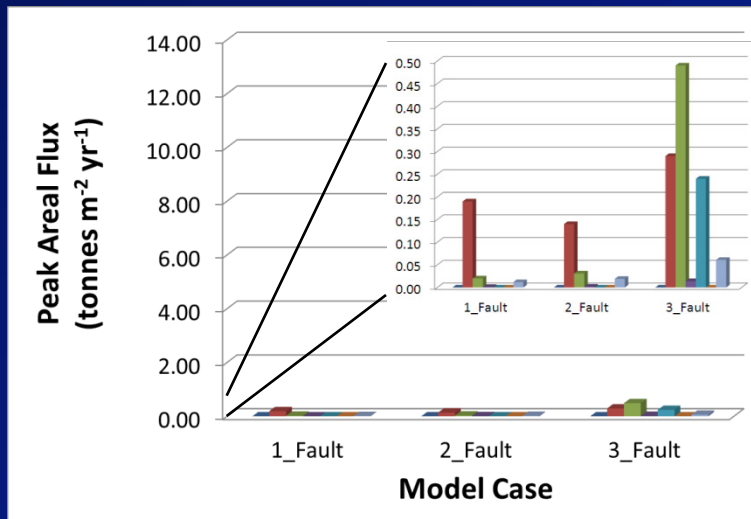
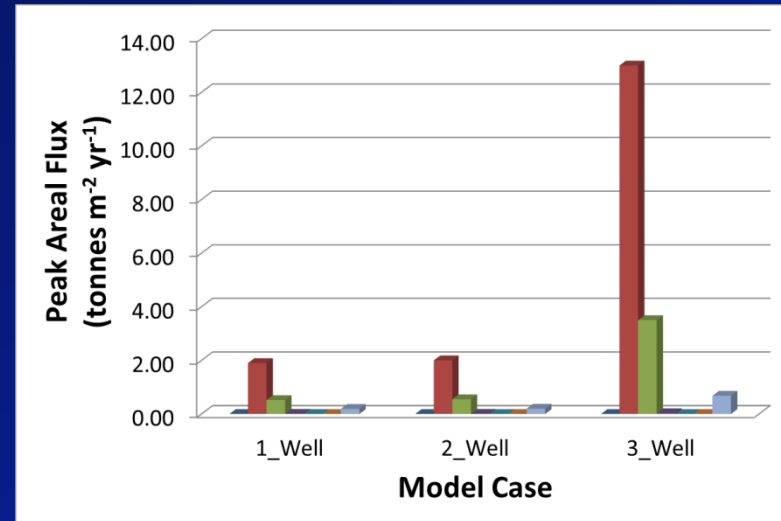


- Negligible CO₂ enters the aquifers
- Owing to relatively small CO₂ surface area per unit volume (c.f. wells)

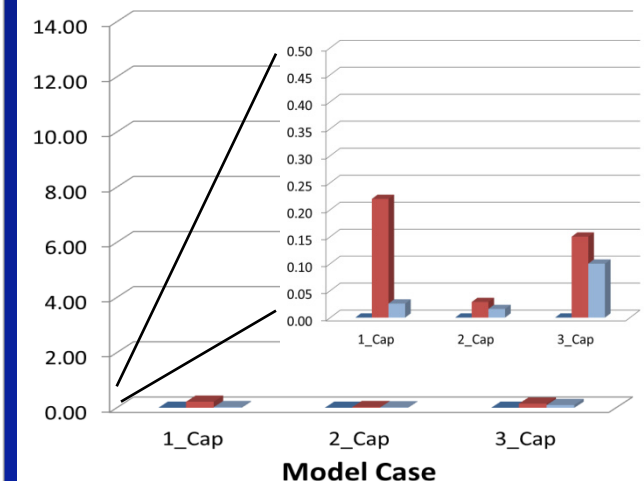
Free CO₂: Peak Areal Fluxes at Key Locations

- Peak fluxes for well cases
- Highest fluxes for near-lithostatic final pressure condition
- Fluxes reflect area of leakage path intersecting the particular model location

<<Hydrostatic – Hydrostatic Hydrostatic – >Hydrostatic Hydrostatic – 85% Lithostatic



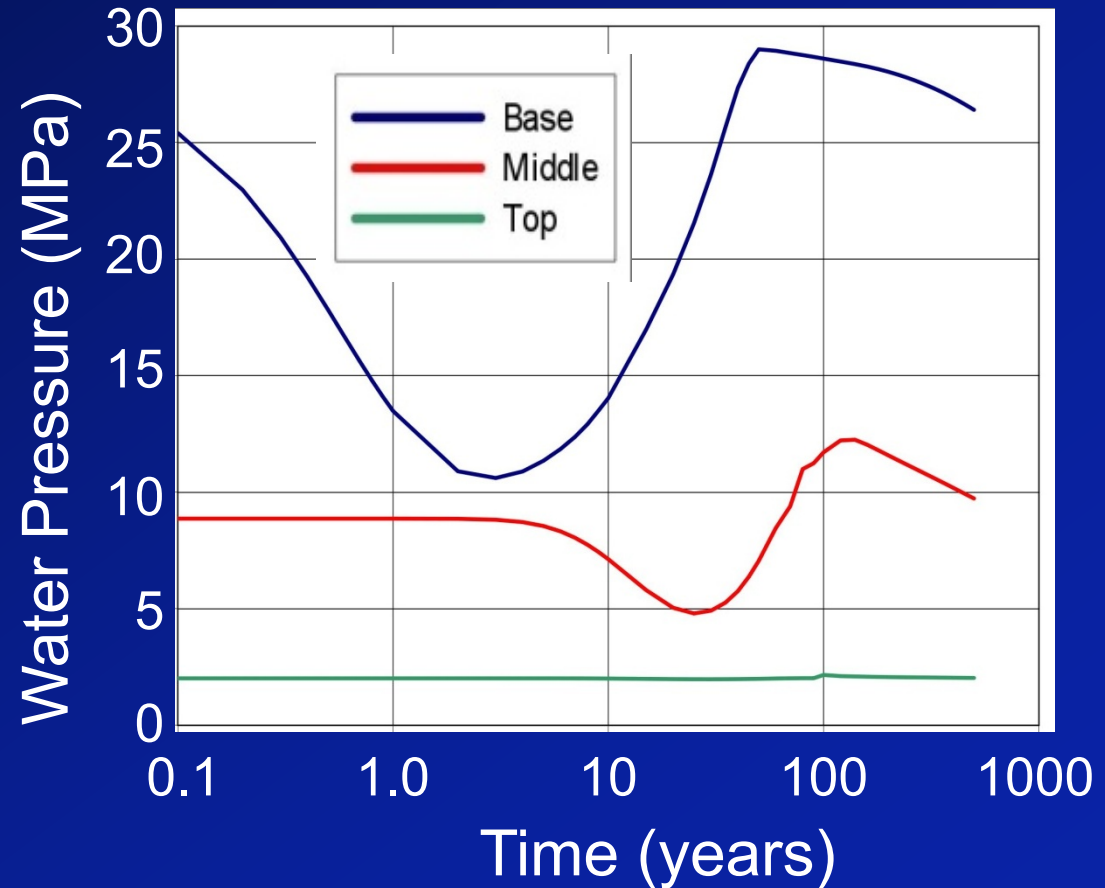
■ Reservoir Boundary (if open)
■ Reservoir to leakage pathway
■ Leakage pathway to lower aquifer
■ Leakage pathway to upper aquifer
■ Boundary fluxes from lower aquifer
■ Boundary fluxes from upper aquifer
■ Leakage pathway to sea bed



Case 1_Cap, Failed Cap Pressure Response

- Initial pressure below hydrostatic
- Greatest pressure variation among the 3 leak modes
- Impact of low initial reservoir pressure seen
- See effects of subsequent CO₂ injection, and initiation of upwards pressure-driven flow (esp. 2 - 20 years)
- Buoyancy effects tend to dominate by >20 years

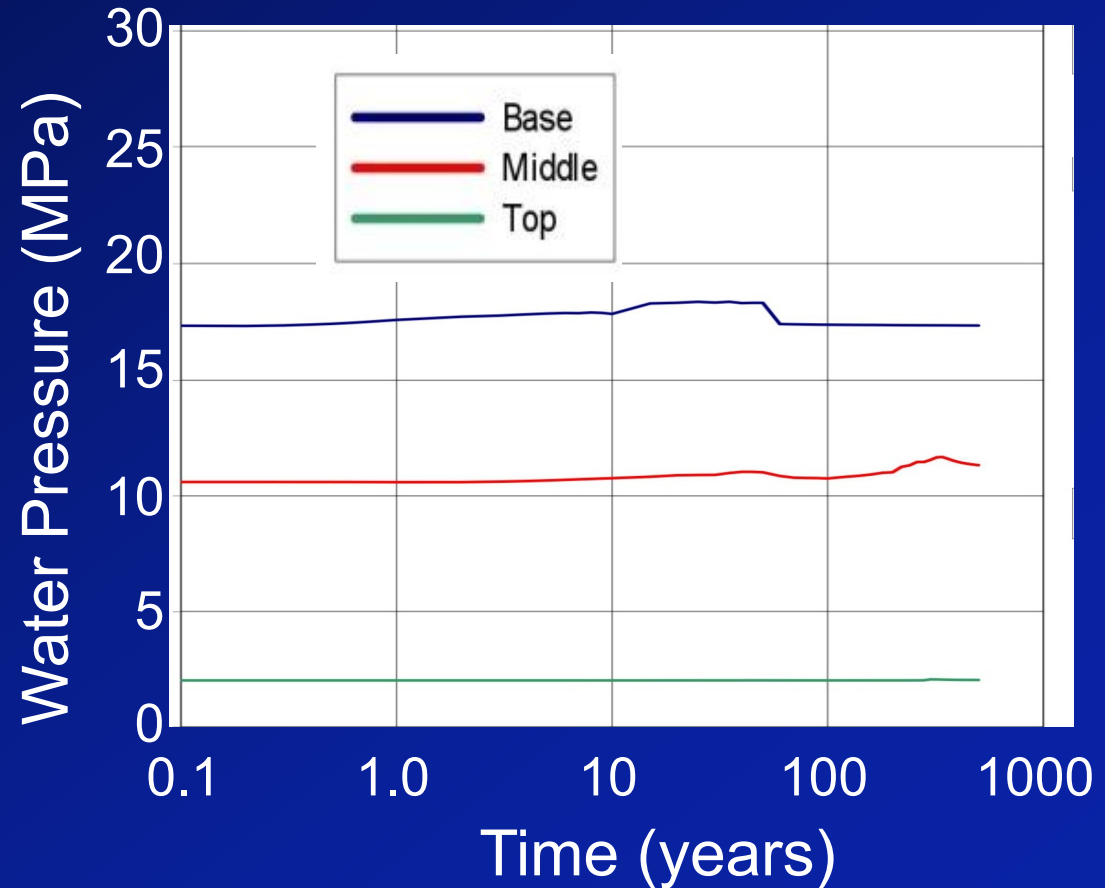
Locations along leakage path



Case 2_Cap, Failed Cap Pressure Response

- Initial pressure hydrostatic
- Much lower pressure variation than in initially underpressured case (Case 1_Cap)
- Minor pressure impacts caused by CO₂ injection
- Subsequent CO₂ migration up the pathway is largely buoyancy driven

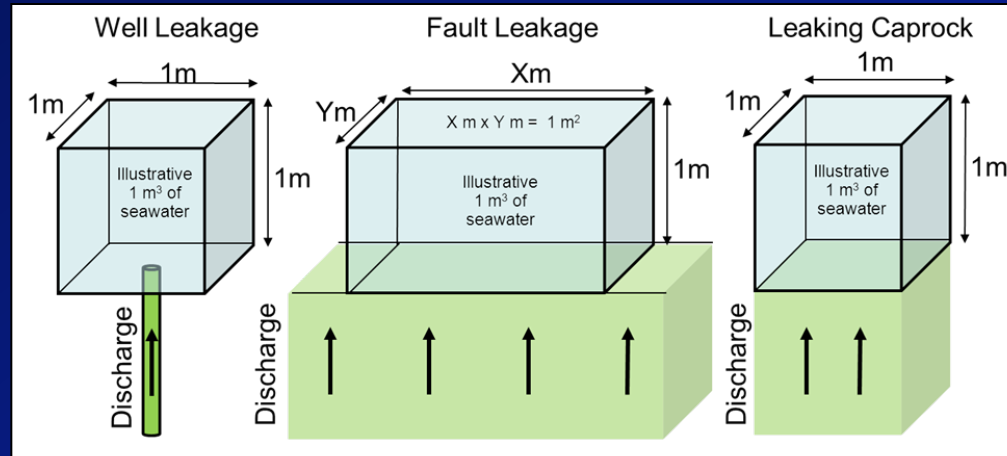
Locations along leakage path



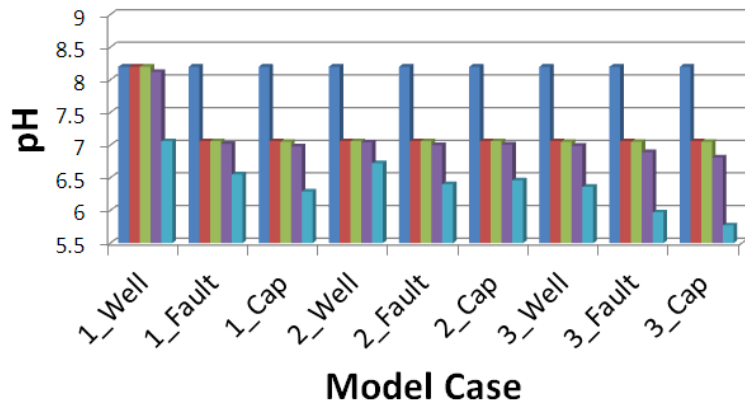
Illustrative Influence on Seawater pH

- Free CO₂ flux causes much greater influence than dissolved CO₂ flux
- Dissolved CO₂ effect only for near-lithostatic pressures in well case

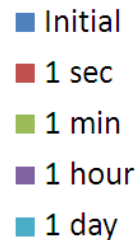
Conceptual Model For Illustrative Calculations



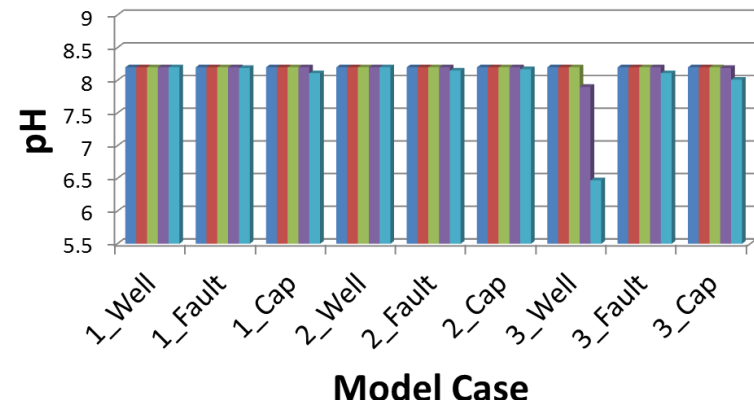
Peak Free CO₂ Flux to Seabed



Seawater Turnover Rate



Peak Dissolved CO₂ Flux to Seabed



Conclusions



- Scenario modelling aids development and communication of monitoring plans, and **is not a prediction tool**
- Systems modelling using simplified grids allows rapid exploration of alternative cases (sensitivity studies)
- Reservoir and over-burden characteristics heavily influence the most appropriate monitoring strategies, e.g:
 - Pressure monitoring of initially under-pressured reservoirs before CO₂ injection could help indicate potential leakage paths
 - Monitoring aquifers in overburden likely more useful for demonstrating wells don't leak than for demonstrating no other kinds of leakage path
 - Monitoring CO₂ remaining in a reservoir less able to identify leaks through borehole leaks than through faults or enhanced-permeability zones
 - Chemical monitoring of a caprock inappropriate because little CO₂ will enter the caprock over relevant timescales



Acknowledgments

- This work was carried out as part of a study commissioned by the Energy Technologies Institute (ETI)
- We thank the ETI for the support of its staff and members in completing this work