## Cold flow investigations of a Circulating Fluidized Bed Chemical Looping Combustion system as a basis for up-scaling to an industrial application

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## **Chemical Looping principle**

Air Reactor (AR)
Oxidation of the metallic oxygen carrier.
Exothermic.

Air FReactor (AR)

AR

FR

MeO<sub>α-1</sub>

Fuel

Oxygen depleted air

Fuel Reactor (FR)
Reduction of the
metallic oxygen carrier.
Endothermic or slightly
exothermic.

#### Chemical Looping Combustion (CLC):

A divided combustion process with intrinsic CO<sub>2</sub> separation. An oxy-fuel process without the need of an oxygen plant (potential lower costs and higher net power efficiency)

 $CO_2 + H_2O$ 

## The BIGCLC project

### A subproject within the larger BIGCO2/BIGCCS project framework

#### Reactor system:

- Cold Flow Model (CFM) construction, commissioning and testing for validation of the 150kW<sub>th</sub> atmospheric rig design
- 150kW<sub>th</sub> atmospheric rig construction, commissioning and test campaigns
- 3. Pressurized conditions

#### Bischi et al.,

"Design study of a 150kW<sub>th</sub> Double Loop Circulating Fluidized Bed reactor system for Chemical Looping Combustion with focus on industrial applicability and pressurization"

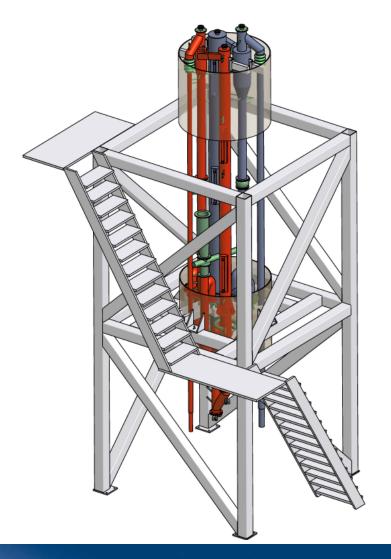
International Journal of Greenhouse Gas Control.

#### Oxygen carrier materials:

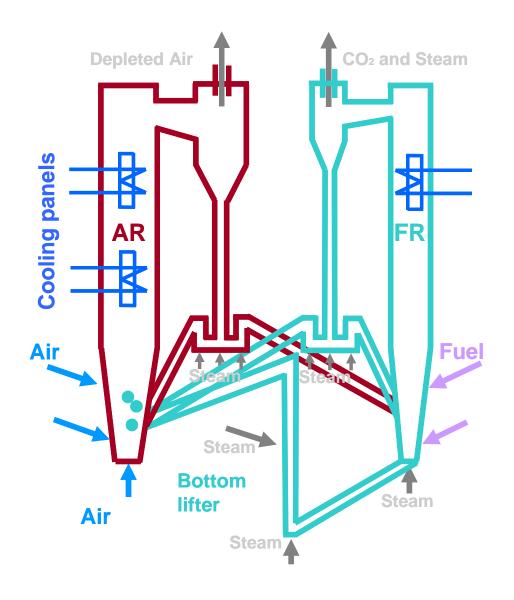
- 1. Screening and preliminary investigation
- 2. Selection and TGA testing (Mn-ore + Ca & Ti)
- 3. Fabrication by industrial methods
- 4. Testing in a small continuous FB process

#### Fossdal et al.,

"Study of inexpensive oxygen carriers for chemical looping combustion" International Journal of Greenhouse Gas Control.



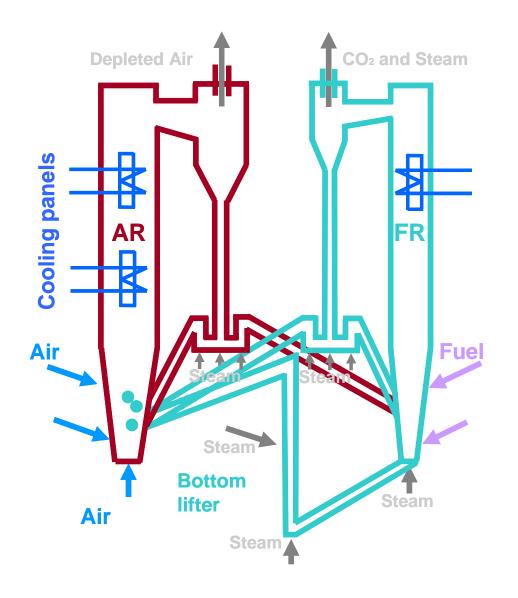
## **Double Loop Circulating Fluidized Bed (DLCFB)**



### **Design criteria**

- High gas—solids contact
- High solids exchange
- Flexibility of configuration
- Compactness
- Choose industrial solutions wherever possible
- Continuous operation

## **Double Loop Circulating Fluidized Bed (DLCFB)**



### **Design parameters**

Design parameter		AR 150kW <sub>th</sub>	FR 150kW <sub>th</sub>
$u_{o}$	[m/s]	~4	~4
D	[m]	0.25	0.15
L	[m]	5	5
$\rho_{p}$	[kg/m³]	2000	2000
$ ho_{ m f}$	[kg/m³]	0.268	0.249
d <sub>50</sub>	[µm]	100	100
μ	[Ns/m²]	4.84E-05	4.29E-05
Т	[°C]	1000	1000
P	[Pa]	100000	100000

- Geldart Group A particles
- Fast fluidization flow regime (CFB regime)

## Scaling criteria for fluidized bed hydrodynamics

### Glicksman scaling laws

- Simulating the hydrodynamics of a high temperature FB reactor with a smaller cold flow model
- Based on non-dimensional particles and fluid equations of motion
- A set of scaling parameters to be matched between actual reactor and model
- → May impose different Geldart Group of particles and different flow regime

## Scaling criteria for fluidized bed hydrodynamics

### **Knowlton scale-up**

- 1. Select operating regime
- 2. Construct a pilot plant (typical diameter 150 300 mm for group A particles)
  - Continuous operation for significant time
  - Industrial concerns can be addressed
  - Reduced wall effects
- 3. Construct a large cold-flow model (generally larger than the pilot)
- 4. Construct a demonstration plant
- 5. Construct a commercial plant
- → Flow regime and particle Geldart Group should be kept the same

## **Cold Flow Model (CFM) scaling strategy**

## Industrial Demo ~30MW

• Simplified Glicksman Criteria:

$$\frac{u_0^2}{g \cdot D}$$
,  $\frac{\rho_p}{\rho_g}$ ,  $\frac{L}{D}$ ,  $\frac{u_0}{u_{mf}}$ ,  $\frac{G_s}{\rho_p u_0}$ ,  $\varphi$ , PSD.

- Geldart A particles
- Fluidization regime: Ar & Re<sub>p</sub>

Cold Flow Model

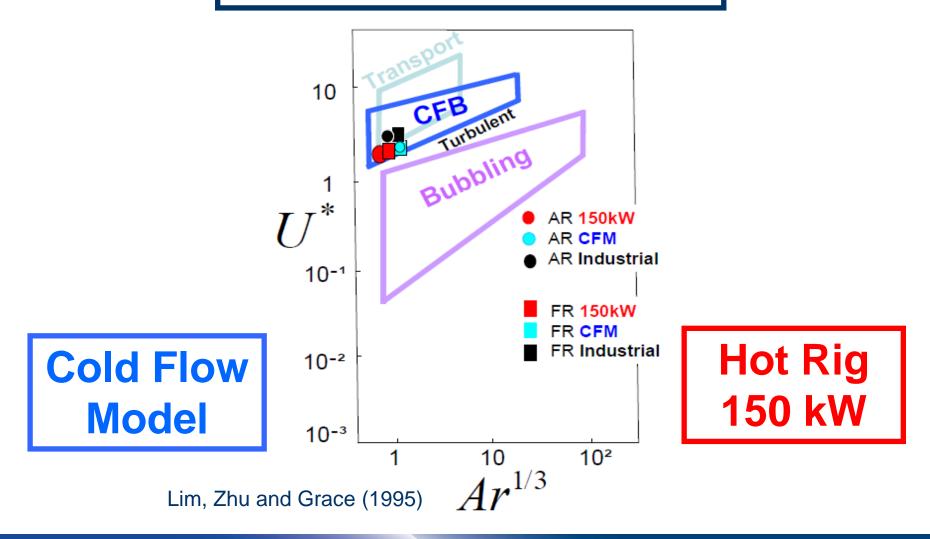
- Process parameters:
   T, P, gas composition
- Same Particles: Density, PSD, φ
- Fluidization regime: Ar & Re<sub>o</sub>

Hot Rig 150 kW

- Geometrical identity
- Geldart A particles
- Fluidization regime: Ar & Re<sub>p</sub>

## **Cold Flow Model (CFM) scaling strategy**

# Industrial Demo ~30MW



## **Experimental set-up**

#### **Cold Flow Model, full scale:**

Air Reactor (AR):

- 5m h, 0.23m id
- Nominal air flow: ~5500NI/min (2.4m/s at 20°C)

Fuel Reactor (FR):

- 5m h, 0.14m id
- Nominal air flow: ~2400NI/min (2.6m/s at 20°C)

Air Reactor Loop-seal:

Nominal air flow: ~165NI/min

Fuel Reactor Loop-seal:

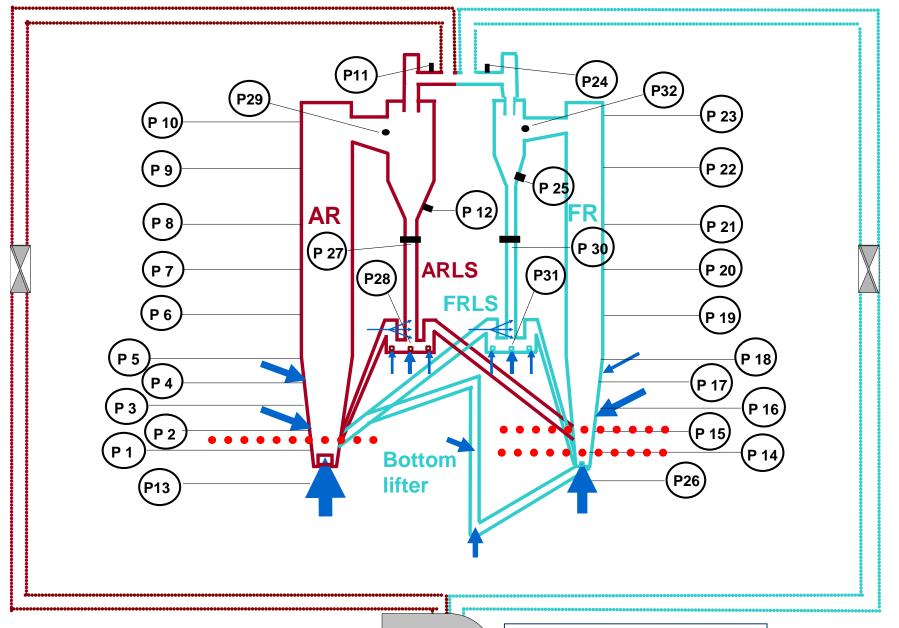
Nominal air flow: ~95NI/min

#### Fe-Si Powder:

Geldart group A

- Starting d<sub>50</sub>: 34micrometers
- Density: **7000kg/m**<sup>3</sup>
- Total Solids Inventory (TSI): ~ 120kg





Frequency controlled fan and filter box mounted on scale

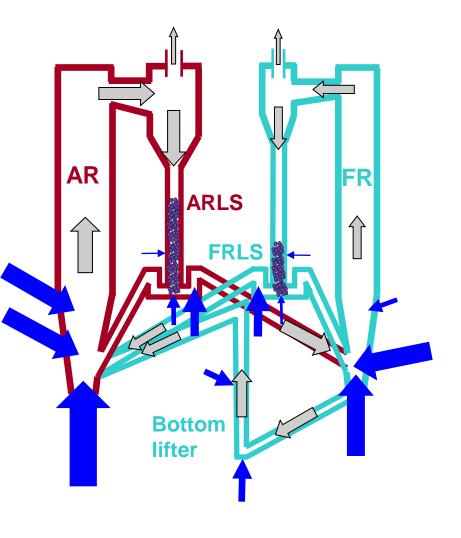
## **Experimental campaign overview**

### **Design condition performance**

- Operational performance and stability
- Validate design solutions

### "Off-design" tests

- FR increased flux/concentration
- Part-load (50%)
- Simulate reforming conditions



**AR: 5500**NI/min (**2.4**m/s)

Primary Secondary 1 Secondary 2

**55%** 22.5% 22.5%

FR: **2400**NI/min (**2.6**m/s)

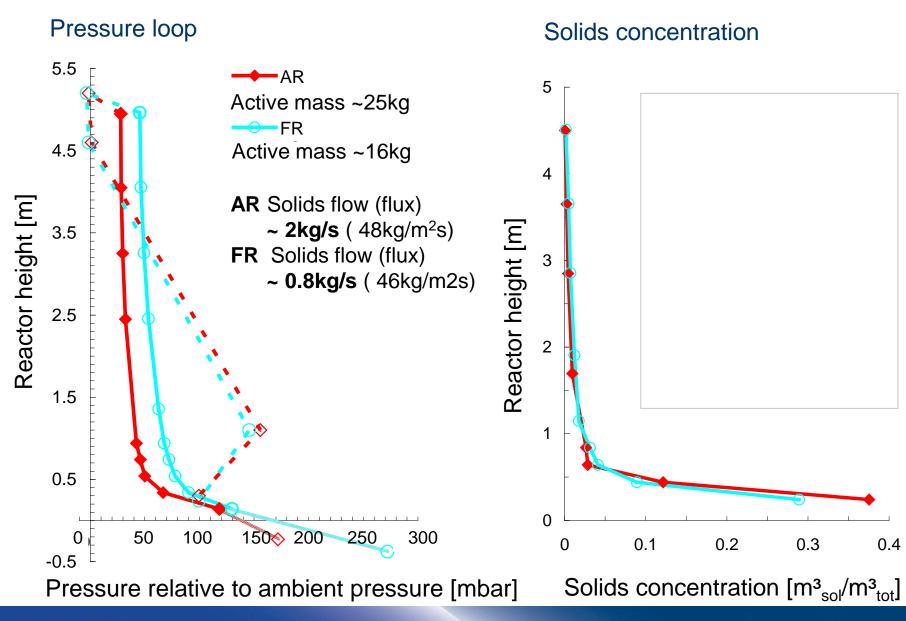
> Primary Secondary 1 Secondary 2

50% 42% 8%

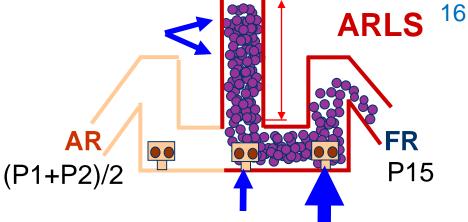
**Lift: 700**NI/min (**1.5**m/s)

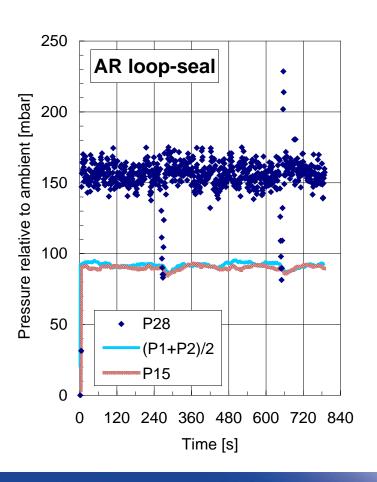
Primary Secondary ~70%

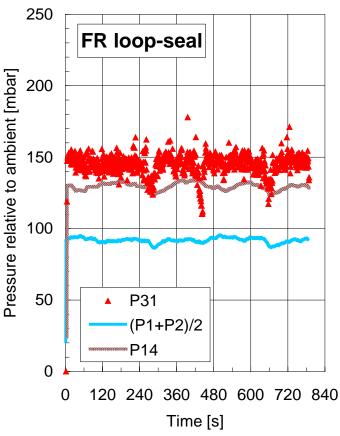
~30%



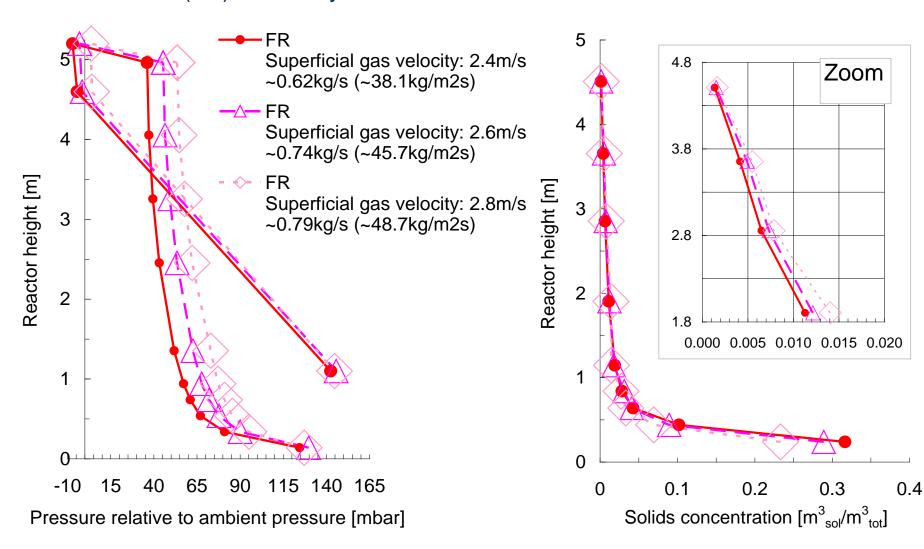
Pressure balance between loop-seals & return points







#### Fuel Reactor (FR) sensitivity



#### **Conclusions & Outlook**

- Achievement of stable operation at design conditions of the DLCFB cold flow model:
  - Solids flow above 2 kg/s → Solids flux (AR) 48 kg/m<sup>2</sup>s
- 2. Stable operation achieved at some defined off-design conditions:
  - Increased FR solids concentration/entrainment
  - Part load conditions
  - Simulated reforming conditions
- 3. Integrate lessons learnt in the final design of the 150kW<sub>th</sub> hot rig
  - Return leg height
  - Increase in FR solids concentration/entrainment
- 4. Scaling strategy incorporating elements from both Glicksman and Knowlton; the 150 kW<sub>th</sub> hot rig (i.e. the next step of the BIGCLC project) and the existing large CFM will together give valuable guidelines and process and design validation for further up-scaling

# Thank you

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