

# Dissolution and carbonation of activated serpentine for combined capture and storage

Mischa Werner<sup>1</sup>, Lilian Gasser<sup>1</sup>, Daniela Zingaretti<sup>2</sup>,  
Hari Subrahmaniam<sup>1</sup>, Marco Mazzotti<sup>1</sup>

TCCS-6

Accelerated Carbonation for Environmental and Materials Engineering

Trondheim, Norway, 14 – 16 June 2011

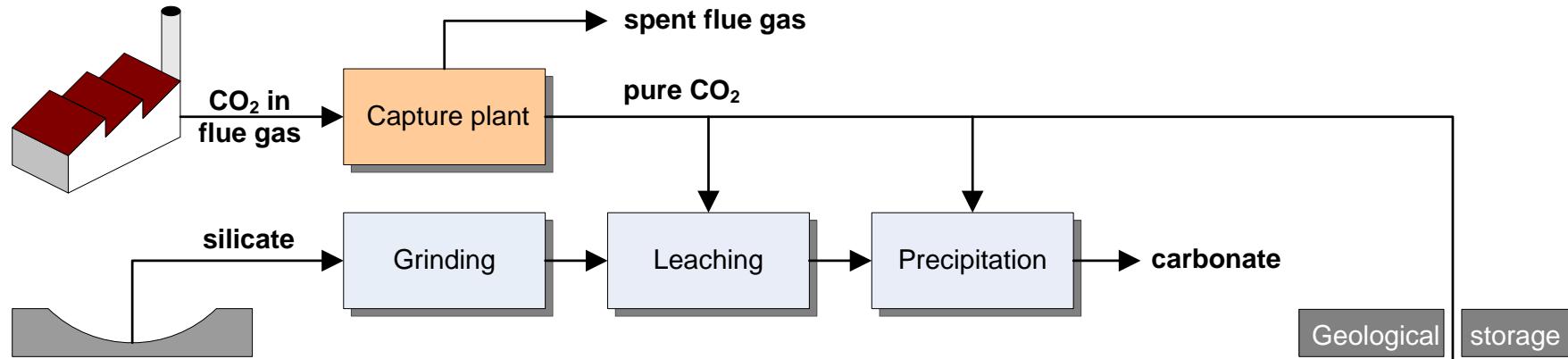
<sup>1)</sup> Institute of Process Engineering, ETHZ

<sup>2)</sup> University of Rome, Thor Vergata

# Outline

- Flue gas mineralization – the concept
- Experimental setup and material
- Capture via mineralization:
  - EQ3/6 equilibrium simulations
  - Dissolution experiments
  - Dissolution model
- Storage via mineralization:
  - EQ3/6 equilibrium simulations

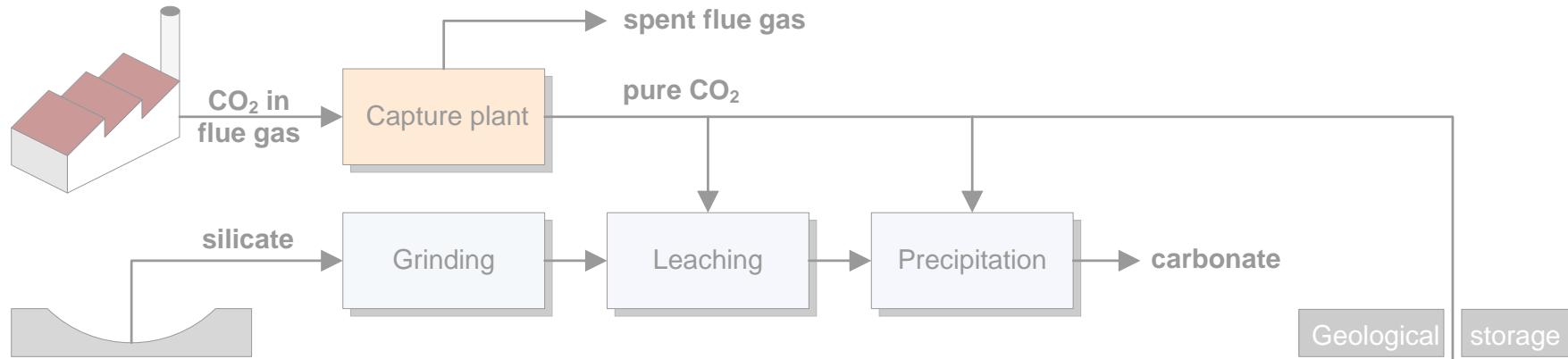
# Flue gas mineralization within a CCS system



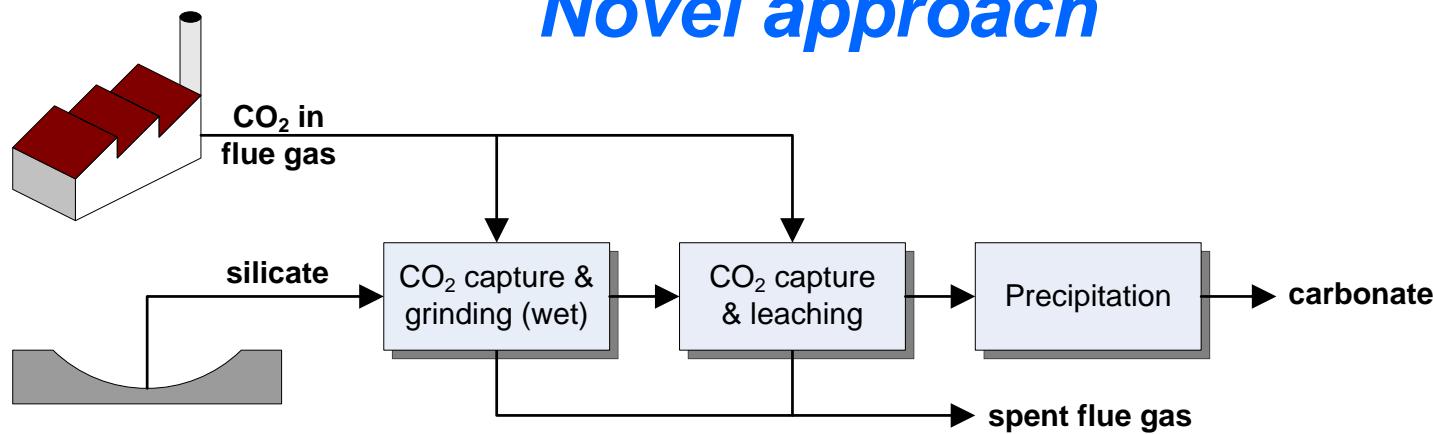
***Traditional approach***

after Verduyn et al. 2009, TCCS5, Trondheim

# Flue gas mineralization within a CCS system

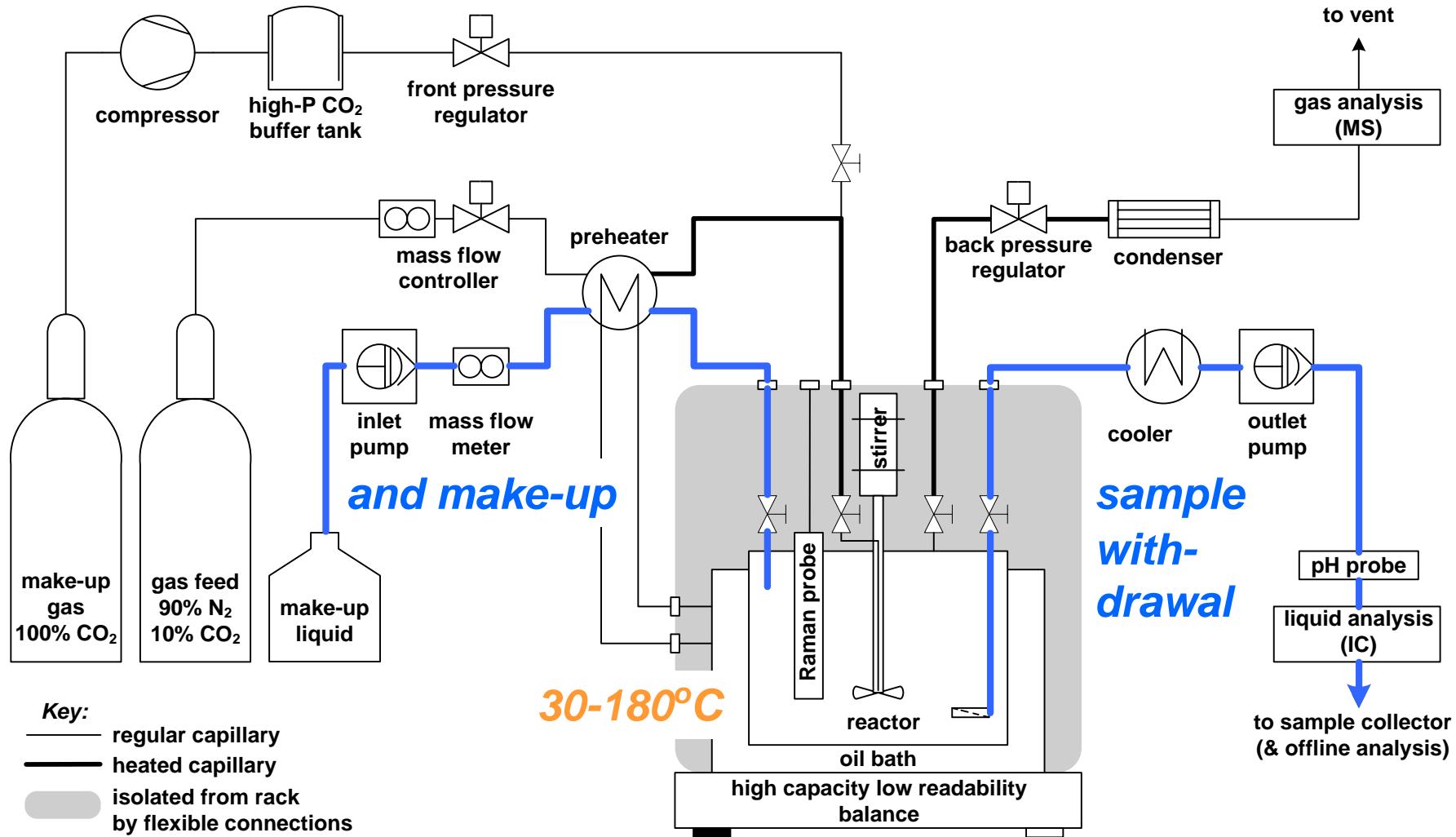


*Novel approach*

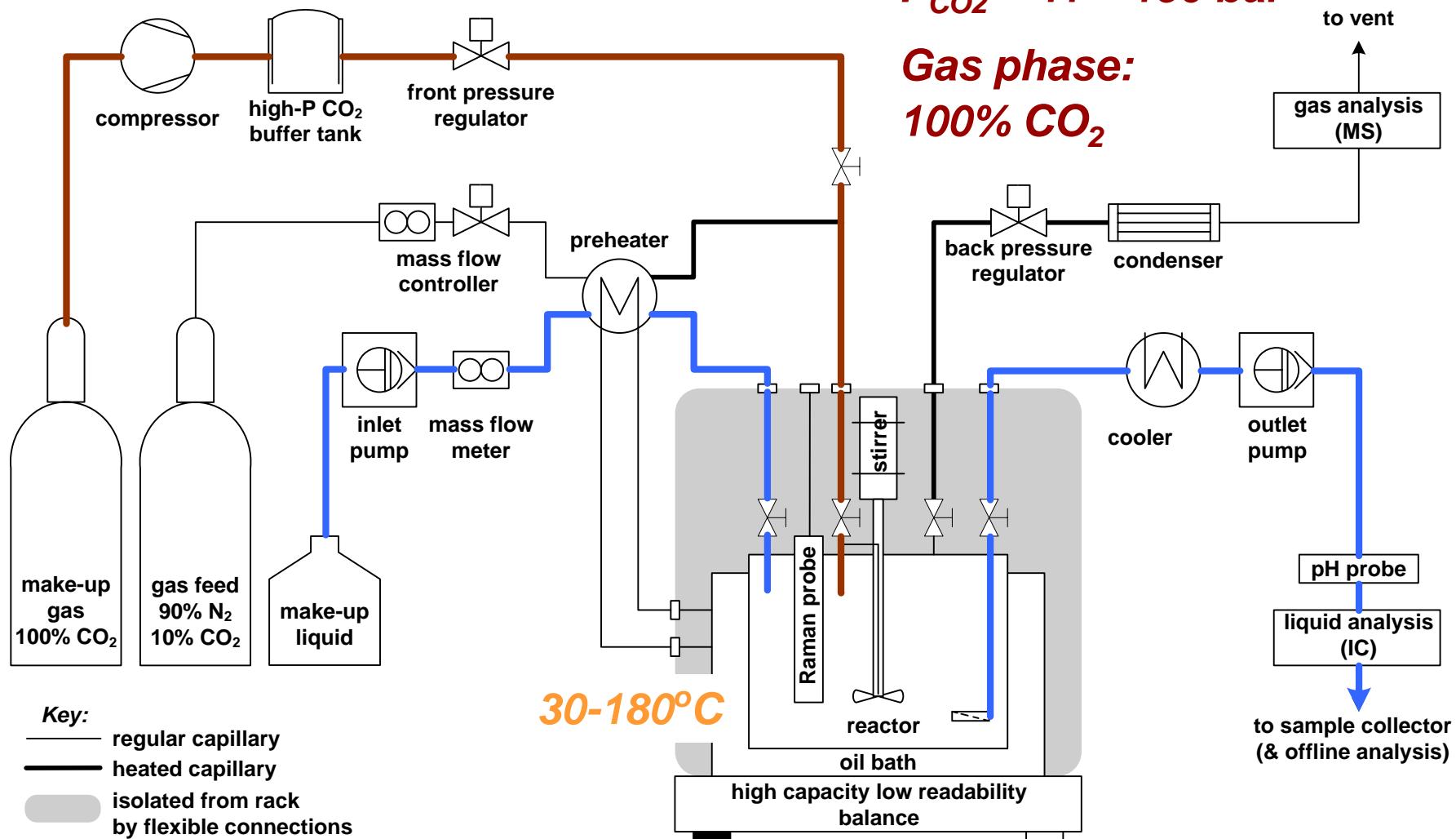


after Verduyn et al. 2009, TCCS5, Trondheim

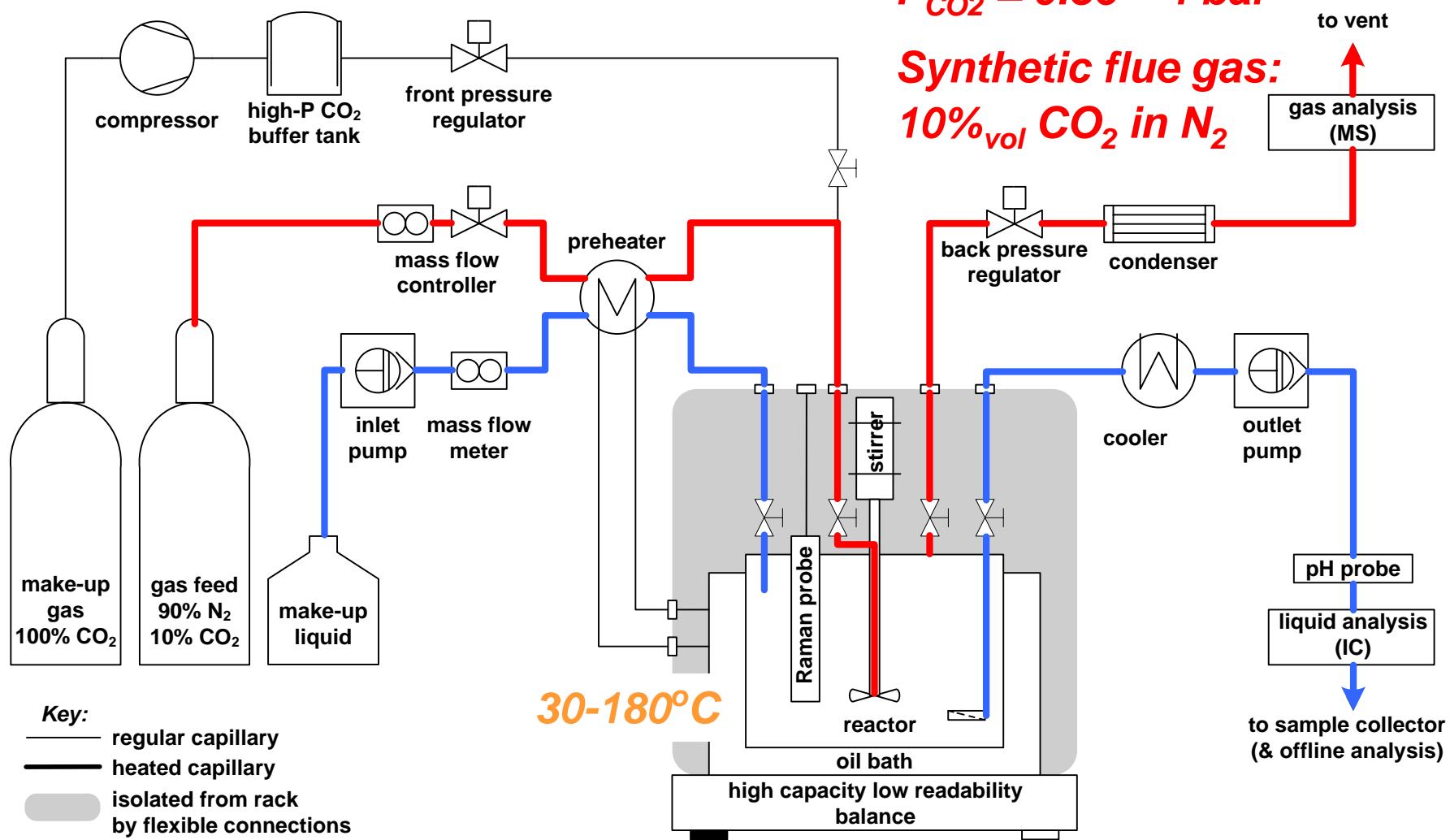
# Mineralization plant



# Mineralization plant



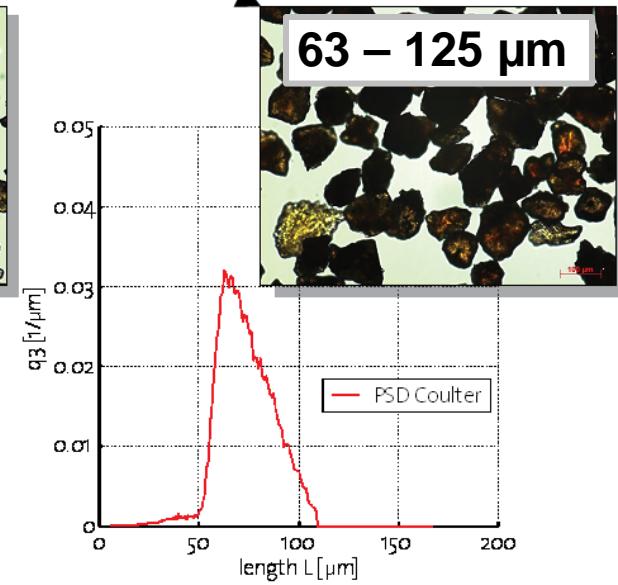
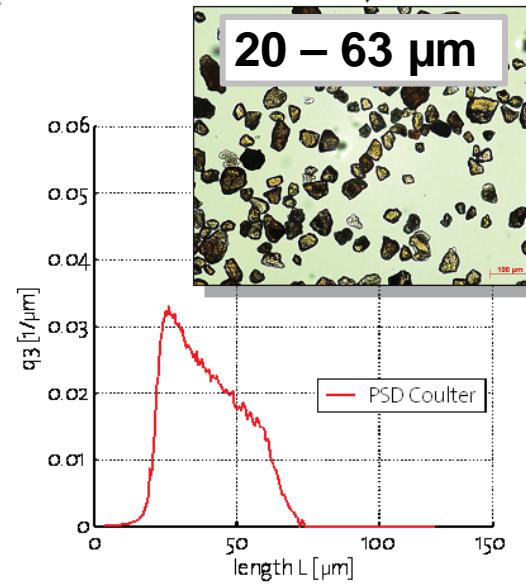
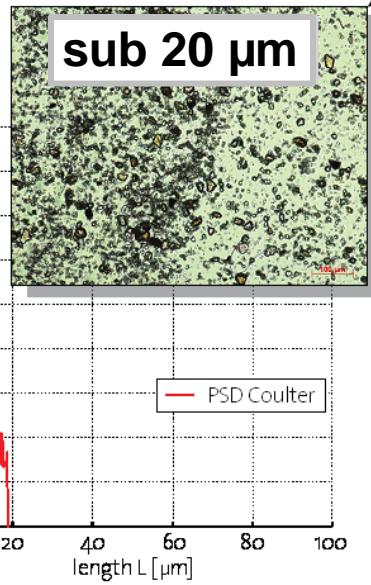
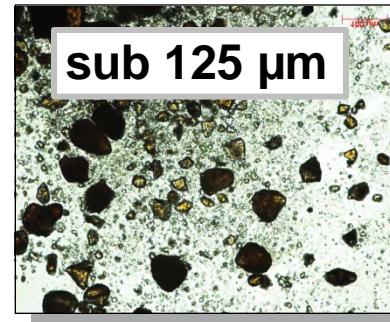
# Mineralization plant



# Activated serpentine

- $\text{Mg}_{2.42}\text{Fe}_{0.58}\text{Si}_2\text{O}_5(\text{OH})_4$
- dry ground to  $<125 \mu\text{m}$
- thermal activation at  $600^\circ \text{ C}$
- 1.5 mol  $\text{H}_2\text{O}$  per mole serpentine removed

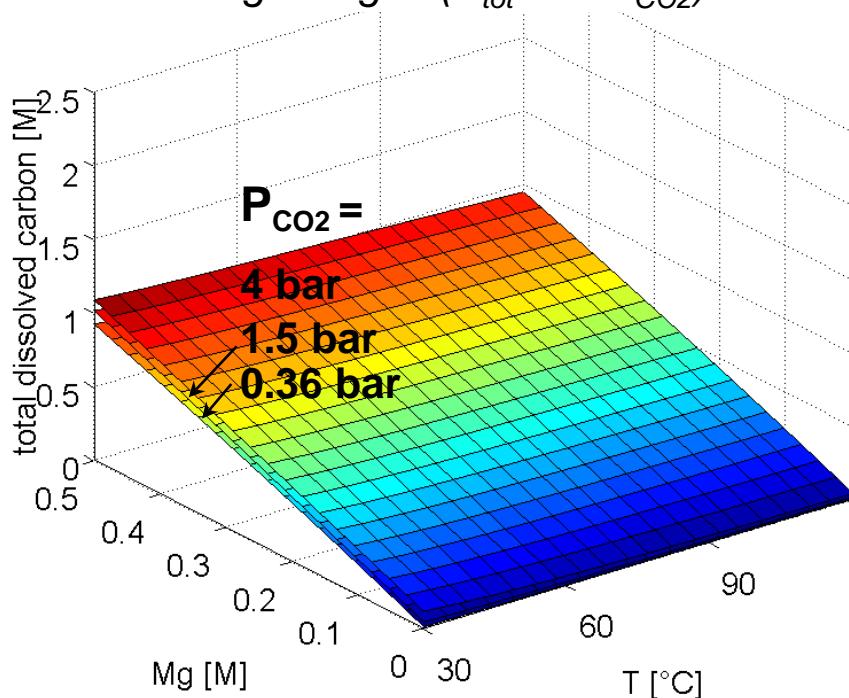
- fractionation by dry sieving
- fines removal w/ EtOH
- micropores (2-3 nm) measured (BET method)



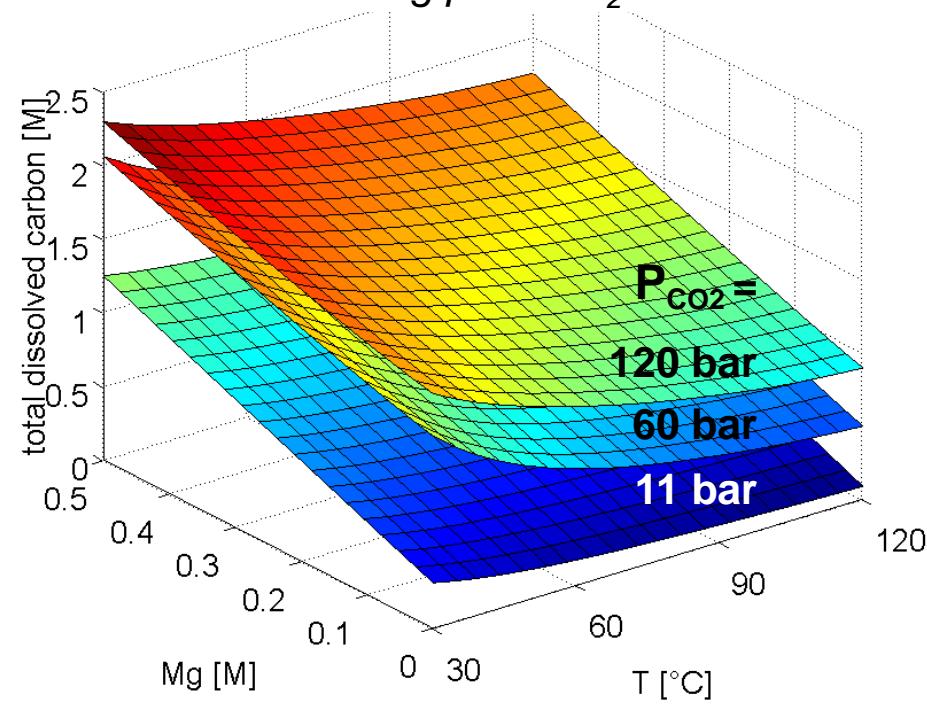
# Capture part: EQ3/6 equilibrium simulations

$\text{CO}_2$  solubility as function of  $T$  and  $[\text{Mg}^{2+}]$ , at different  $P_{\text{CO}_2}$  levels

using flue gas ( $P_{\text{tot}} = 10P_{\text{CO}_2}$ ):



using pure  $\text{CO}_2$ :



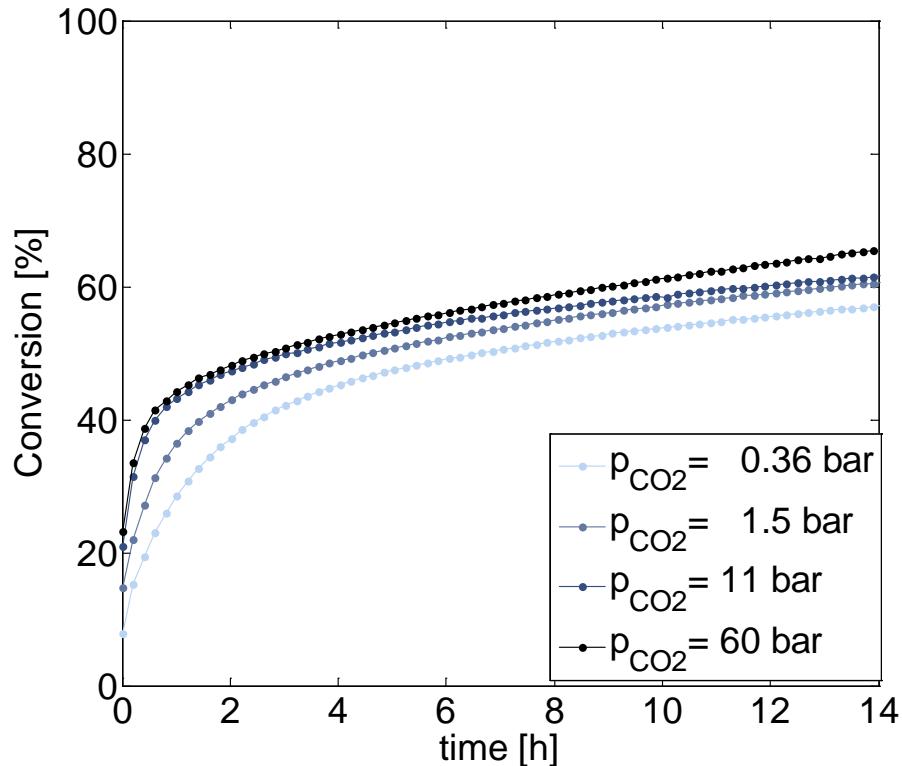
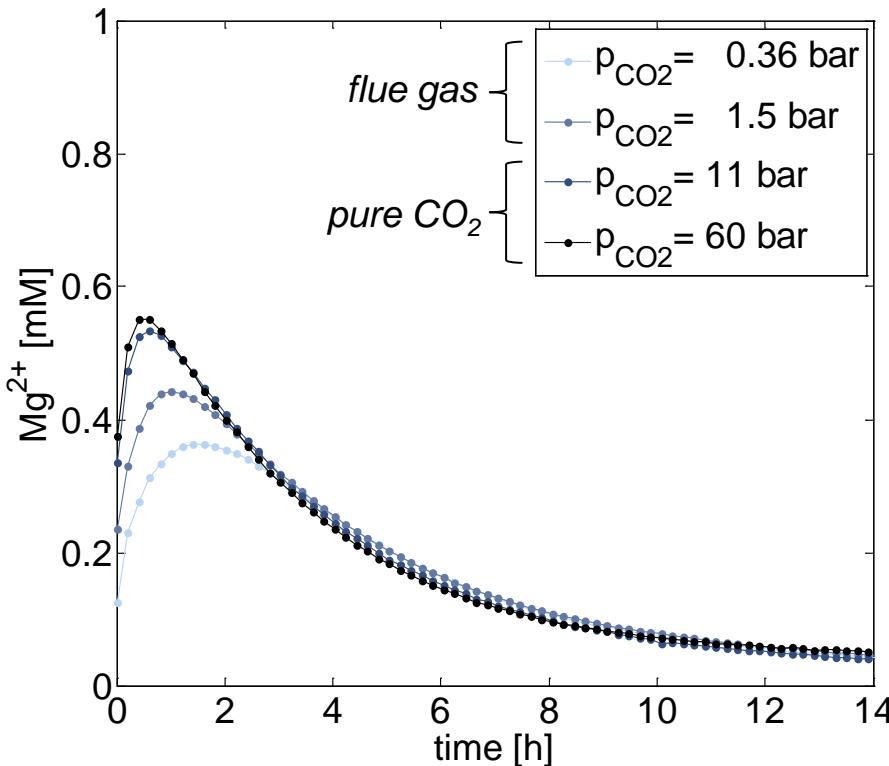
- If flue gas used:  $\text{CO}_2$  solubility predominately sensitive to  $[\text{Mg}^{2+}]$ 

→ even at low  $P_{\text{CO}_2}$  high  $\text{CO}_2$  loads possible
- If pure  $\text{CO}_2$  used: low  $T$  favorable, highest  $P_{\text{CO}_2}$  not worth the while

# Act. serpentine dissolution experiments



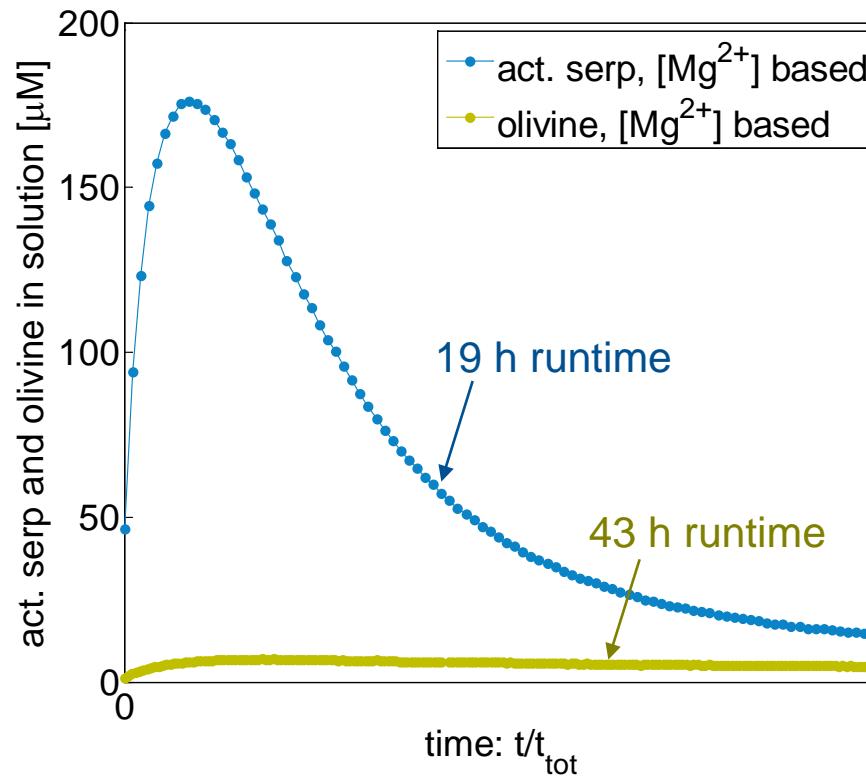
**Magnesium** concentration and conversion at 30°C:



- Dissolution using flue gas similarly effective as with pure  $\text{CO}_2$
- Complex dissolution mechanism: Drastic slowdown after fast initial phase

# Olivine vs activated serpentine dissolution

$T = 30^\circ\text{C}$ ,  $P_{\text{CO}_2} = 0.36 \text{ bar}$ , flue gas mode, 20-63  $\mu\text{m}$  fraction

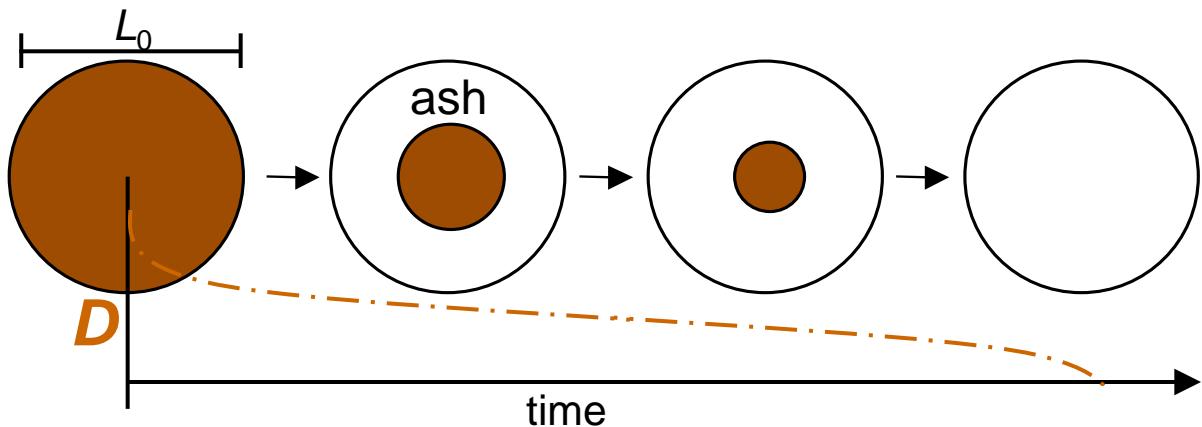


→ Olivine so far “best candidate” Mg-silicate (most reactive)\*

\*e.g. O'Connor et al., 2005, Albany Research Center

# Dissolution model for natural serpentine

**Natural serpentine**  
 dissolves acc. to  
**Shrinking core**  
 model\*



- Population balance:
- Dissolution rate:
- Solute mass balance:

$$\frac{\partial n}{\partial t} - \frac{\partial Dn}{\partial L} = 0$$

$$D = f(L, L_0)$$

$$V \frac{dc}{dt} = \frac{dm}{dt} - Qc$$

n = particle population, PSD

D = dL/dt, dissolution rate

not constant, diffusion controls

c = solute concentration

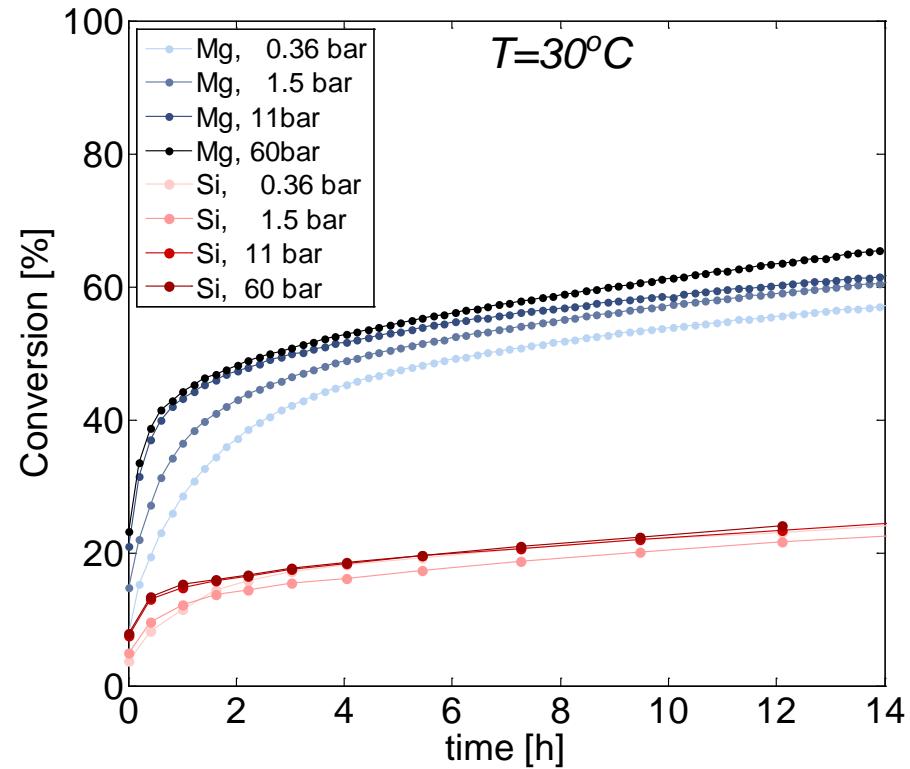
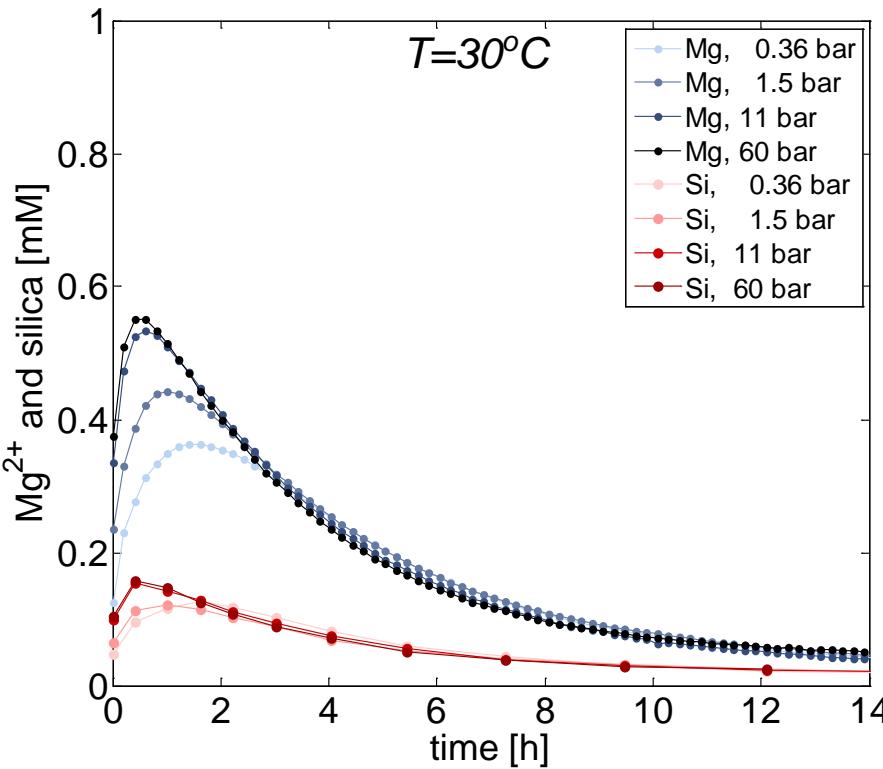
m = mass of particle population

\*e.g. Teir et al., 2007, Int J Miner Process 83;

Van Essendelft et al., 2009/2010, Ind Eng Chem Res 48/49

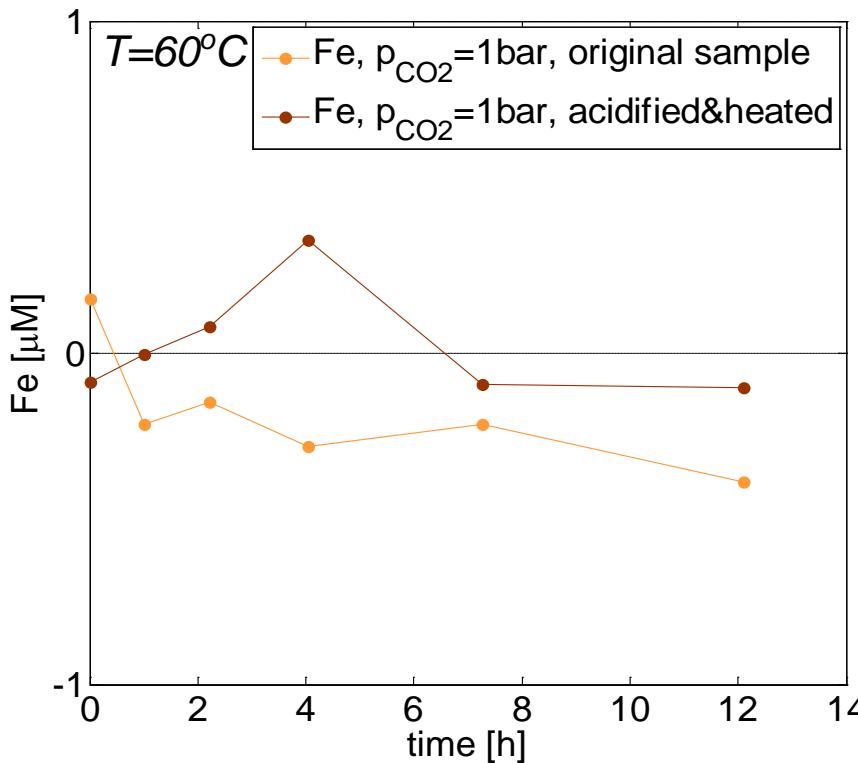
# Dissolution model for activated serpentine

- Presence of micropores and altered crystal structure cause complex, incongruent dissolution behavior
- $\text{Mg}_{2.42}\text{Fe}_{0.58}\text{Si}_2\text{O}_5(\text{OH})_4 \rightarrow \text{Silica}$  detected in reactor solution:



# Dissolution model for activated serpentine

- Presence of micropores and altered crystal structure cause complex, incongruent dissolution behavior
- $Mg_{2.42}Fe_{0.58}Si_2O_5(OH)_4 \rightarrow$  Iron absent in reactor solution:



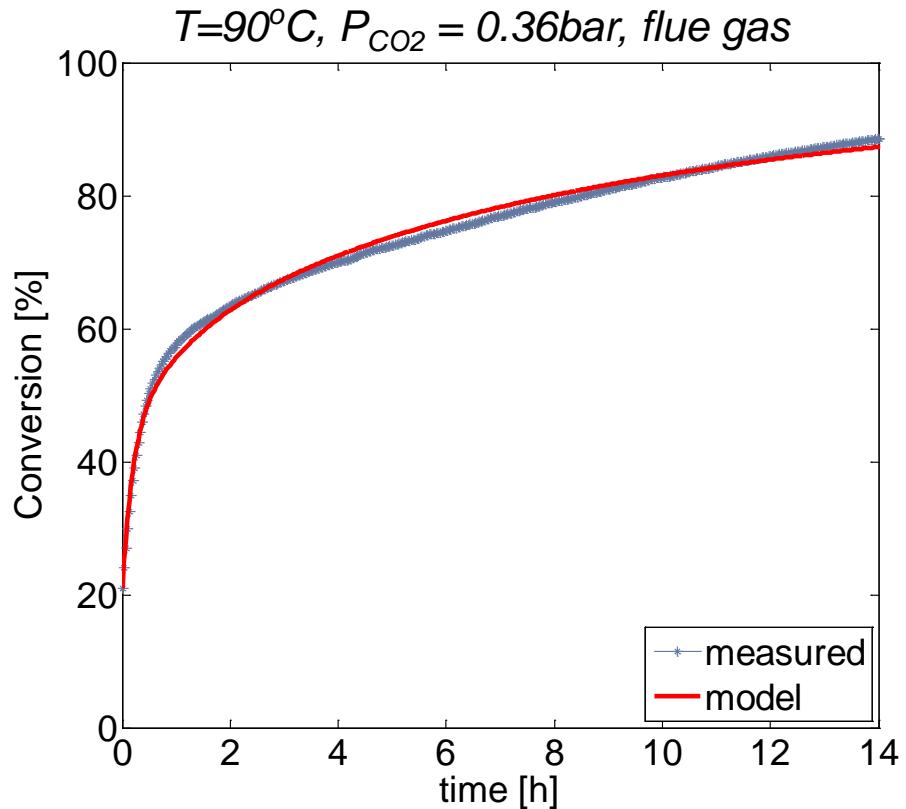
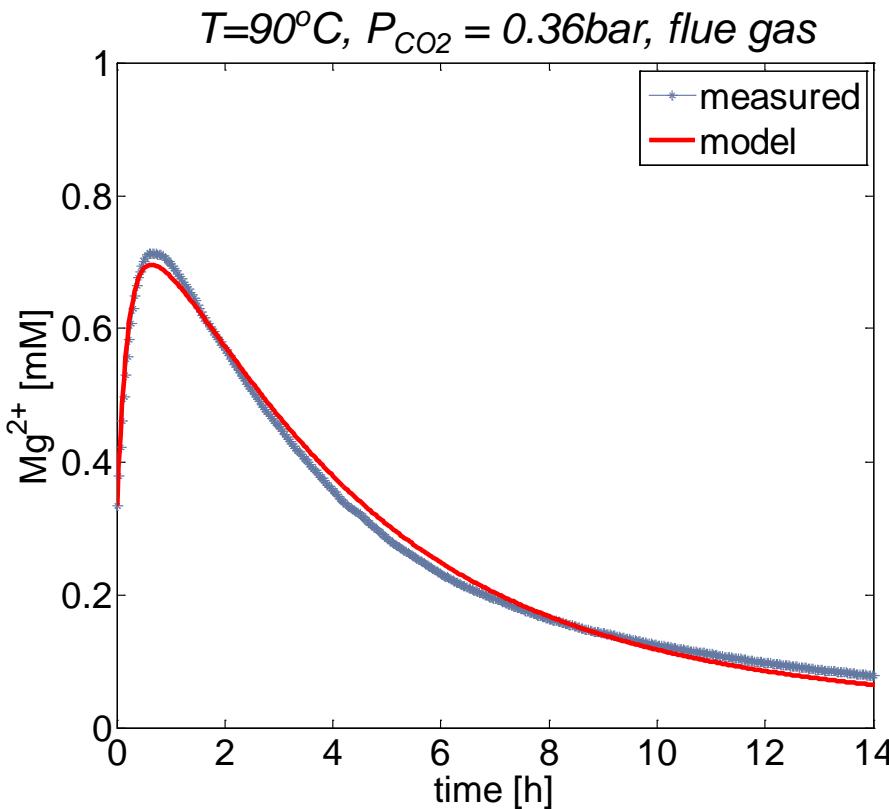
→ Preferential leaching of  $Mg^{2+}$

# Dissolution model for activated serpentine

- Presence of micropores and altered crystal structure cause complex, incongruent dissolution behavior
- Back to single particle model to explore the role of:
  - diffusion
  - counterdiffusion
  - ash layer
  - unreacted core
  - pores
  - reactants ( $H^+$ )
  - products ( $Mg^{2+}$ , silica)
- PSD discretized to perform preliminary simulations
- Single experiments can be fitted nicely, but fitting multiple experiments yet an issue

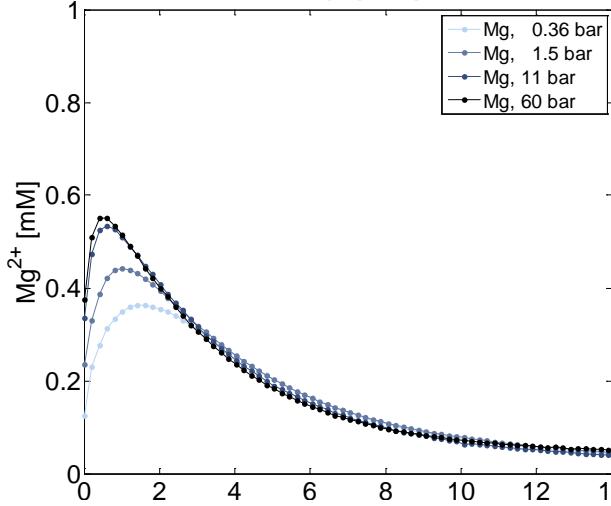
# Dissolution model for activated serpentine

Measured and modelled  $Mg^{2+}$  profile and conversion:

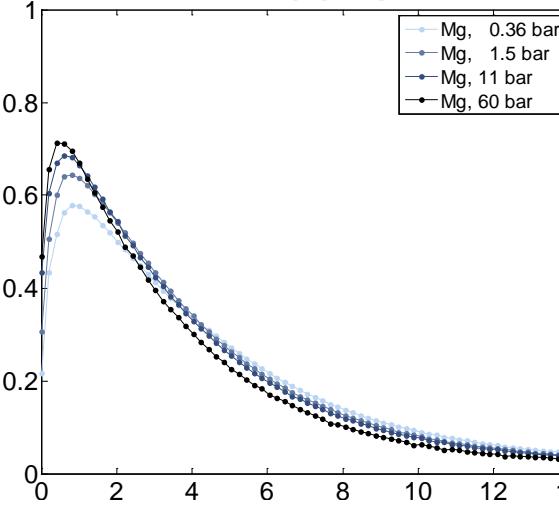


# Serpentine dissolution experiments

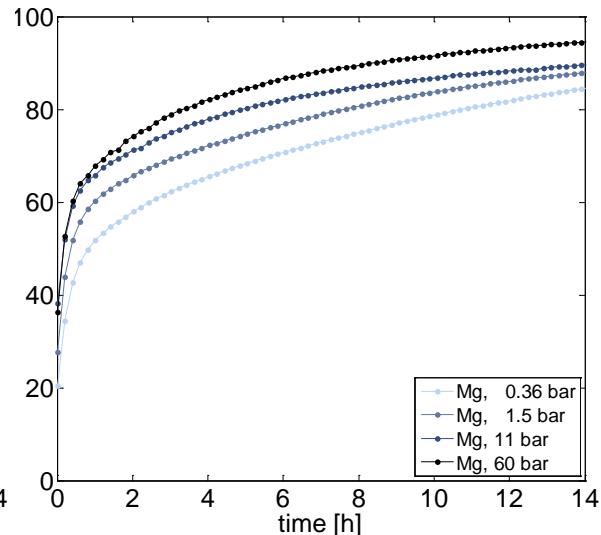
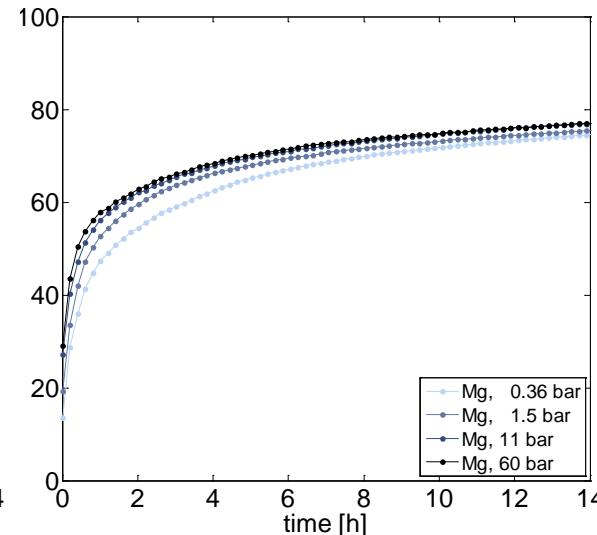
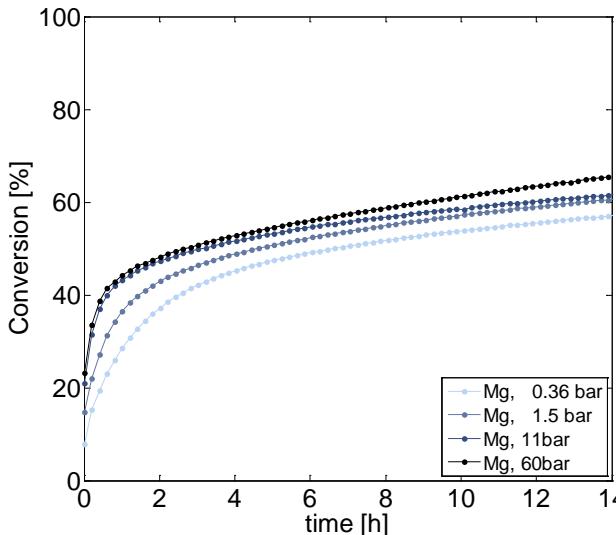
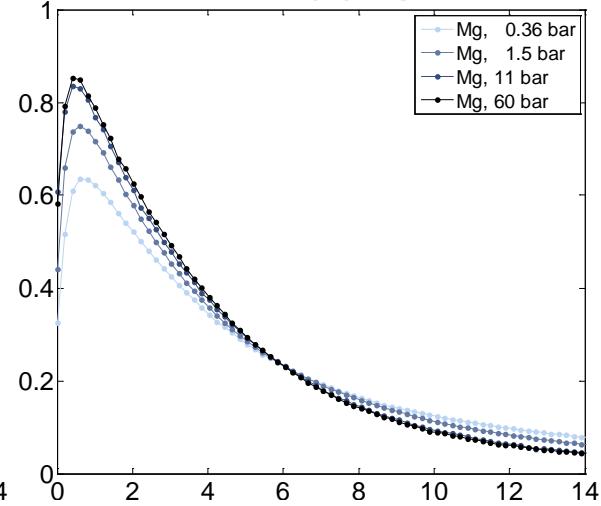
T=30°C



T=60°C

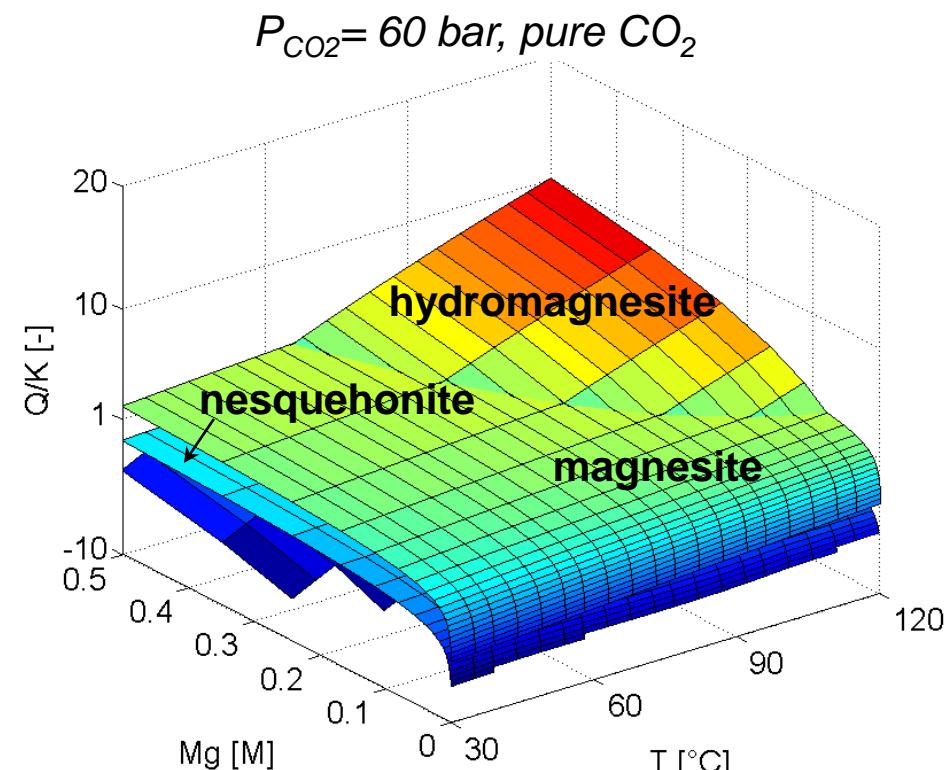
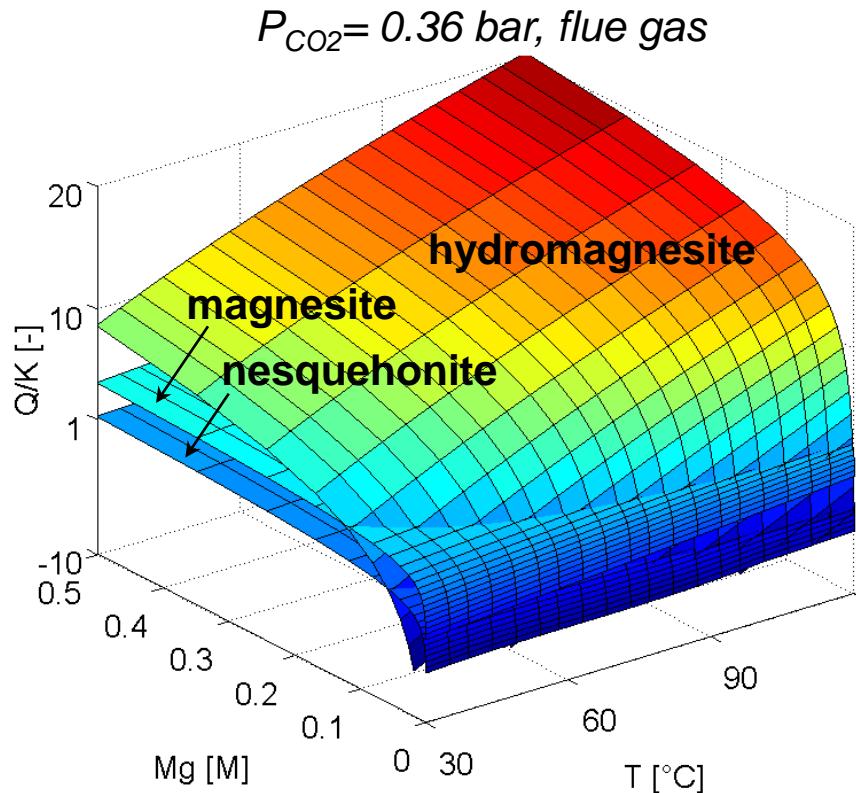


T=90°C



# Storage part: EQ3/6 equilibrium simulations

Thermodynamic driving force ( $Q/K$ ) as function of  $T$  and  $[Mg^{2+}]$ :



- Higher  $T$  favors carbonate precipitation
- High  $P_{CO_2}$  not beneficial, flue gas conditions preferable!

# Concluding remarks

- $\text{CO}_2$  capture into aqueous solution promoted by presence of  $\text{Mg}^{2+}$  from the dissolution process
- Activated serpentine dissolution fast even at low  $P_{\text{CO}_2}$ , thereby preferential leaching of  $\text{Mg}^{2+}$
- Higher T promotes Mg leaching and reduces carbonate solubility
- Thermodynamic driving force for precipitation higher under flue gas conditions

# Acknowledgements

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- Competence Center Energy and Mobility, CH
- Competence Center Environment and Sustainability, CH

# Thanks for your attention

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