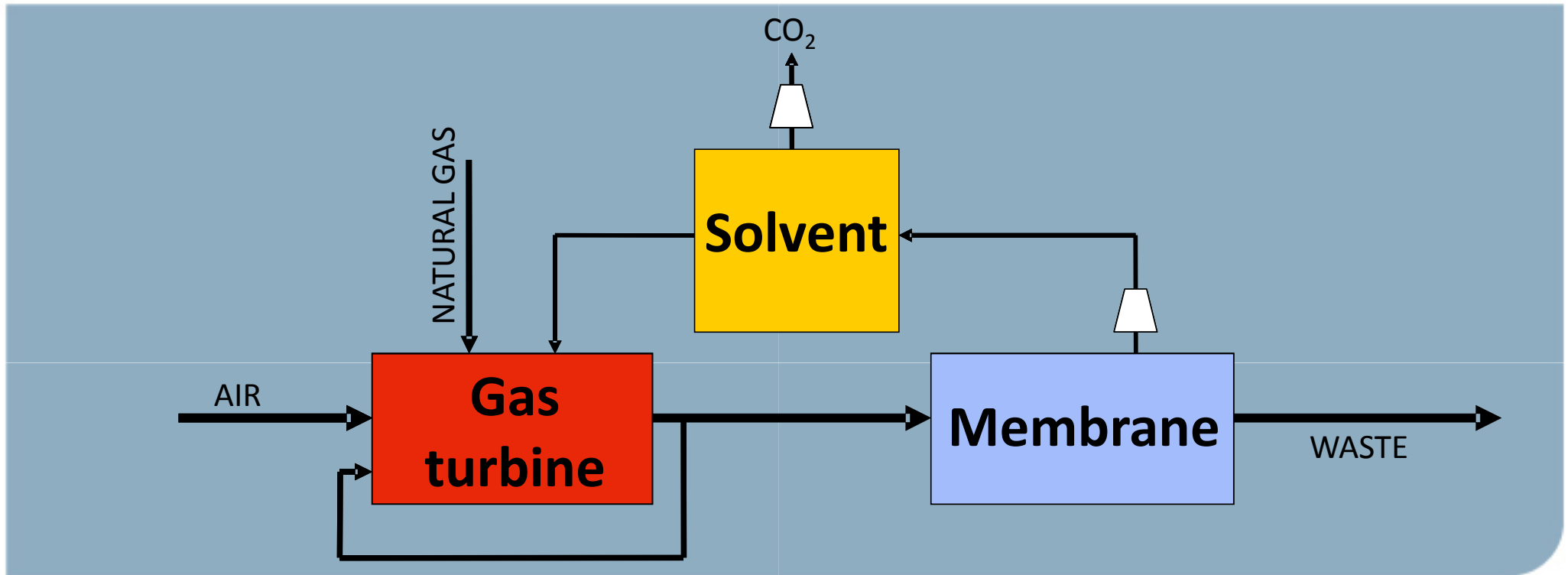


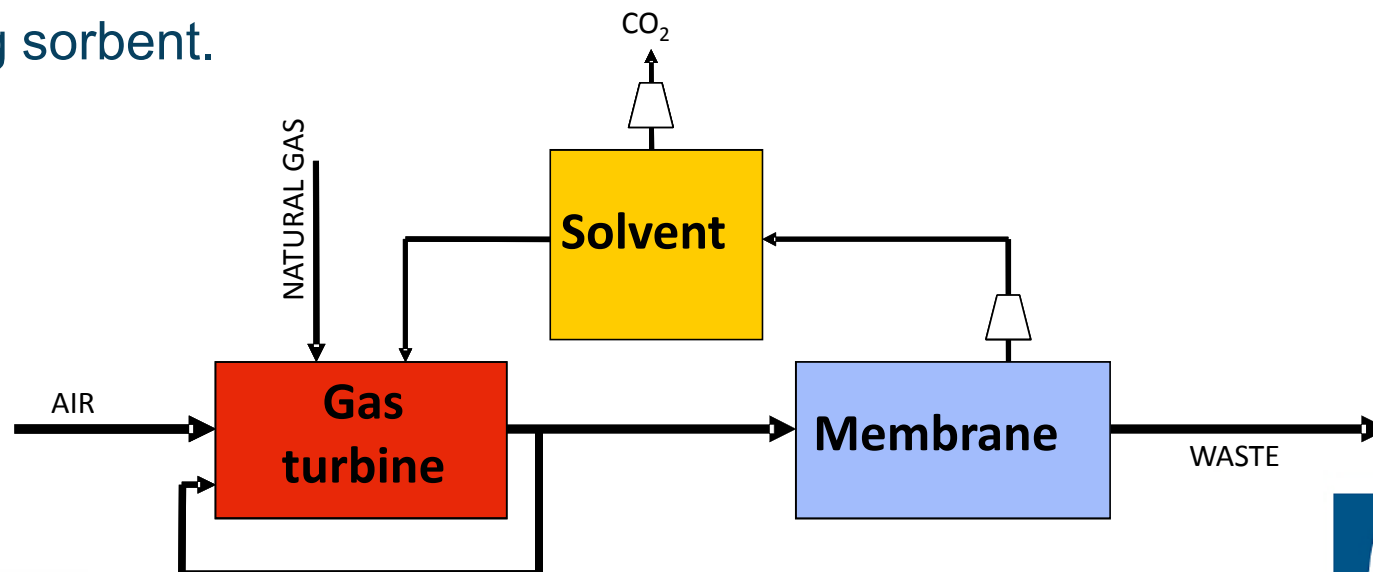
Hybrid absorber-membrane CO₂ capture



*Paul Raats, Nick ten Asbroek, Martijn Huibers
TCCS-6 Trondheim, June 16th, 2011*

Idea for post-combustion CO₂ capture from gas-fired installations

- Recycling: looping back a fraction of the flue gas to the gas turbine to double the CO₂-concentration;
- Membrane preconcentration: applying CO₂-selective membranes sequentially leading to a CO₂-concentration of e.g. 50%;
- Absorber final capture: compressing this carbon dioxide rich flow and feed to a pressurized absorber where the CO₂ will be absorbed using a low energy consuming sorbent.

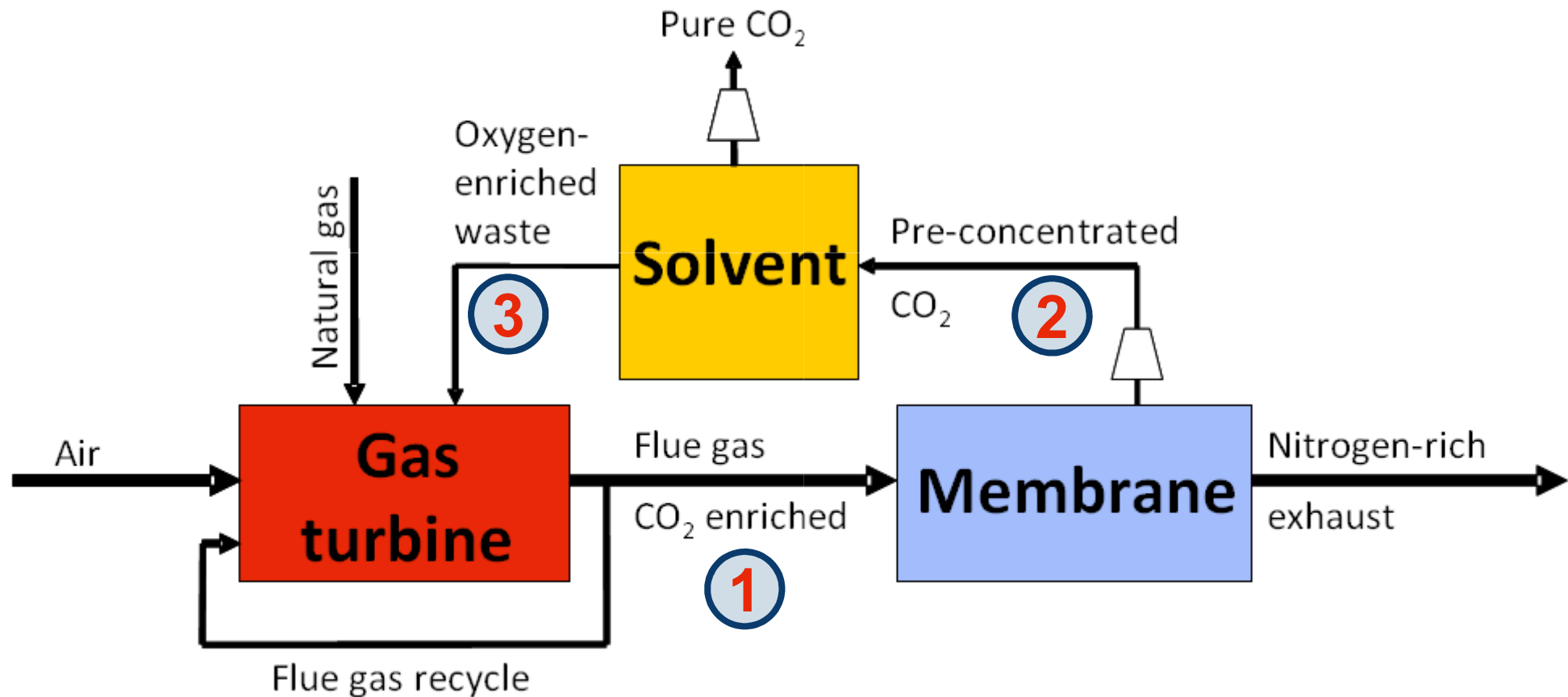


Contents

- Concept overview
- Parameters at interfaces
- Issues
- Membrane modelling
- Solvent selection
- Progress



Concept overview *(patent granted)*



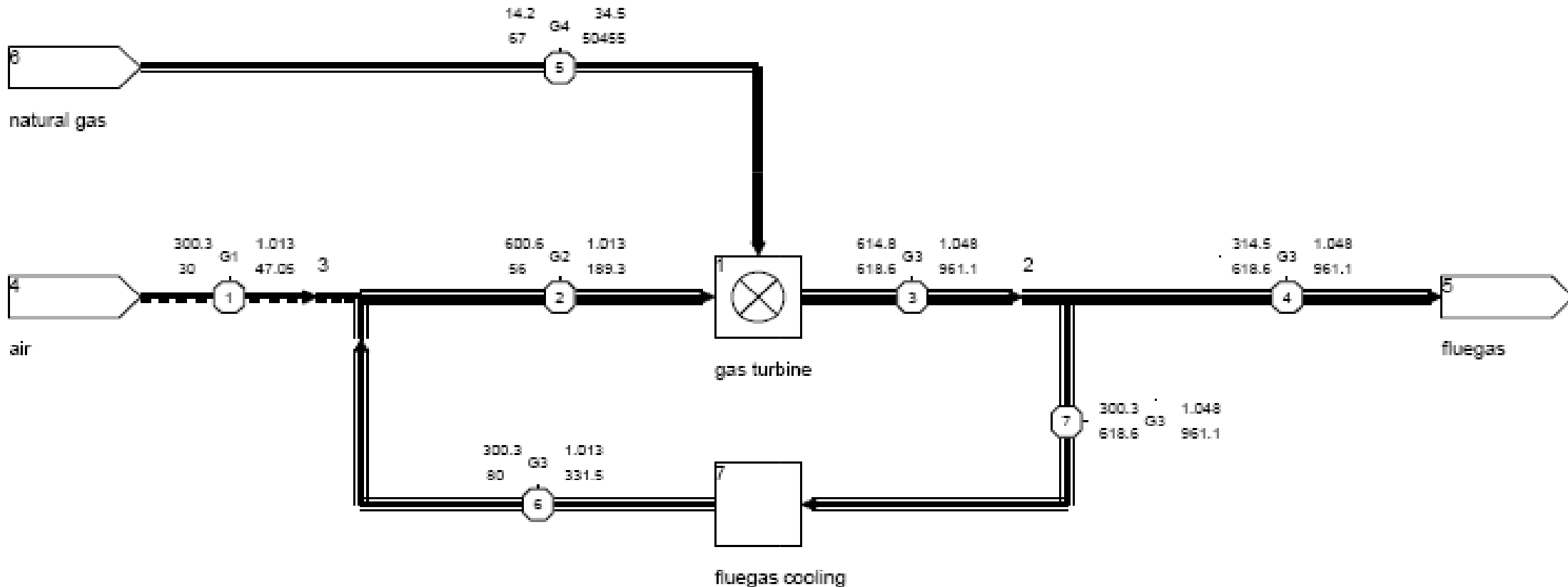
- Optimal performance membrane + absorber
 - Energetically favourable
- Enables post-combustion CCS for gas turbines
 - Major CO₂ emitters at low concentration

Parameters at interface 1

1. Gas turbine – membrane unit

- 100 °C, but can be lowered as desired (heat exch.)
- Pressure ~1 bar (gas turbine durability and efficiency)
- Flue gas looping: modelled in KEMA's SPENCE ® model
 - for simulation of processes for energy conversion and electricity production
 - plant design and performance calculations
 - online process calculations to control operation processes
 - 400 MW combined cycle power plant (2/3 of power originates from the gas turbine)

Flue gas looping in SPENCE: scheme



m [kg/s]	p [bar]
t [°C]	h [kJ/kg]
SPENCE 7.1	
GRASP 2.72	
GTmodel.STM	

gas nr.	1	2	3	4
Ar	0.0092	0.00885	0.00851	
O2	0.20723	0.12708	0.04942	
N2	0.77237	0.7447	0.71788	0.0445
H2O	0.01089	0.08254	0.15195	
CO2	0.0003	0.03683	0.07223	0.0079
CH4				0.9365
C2H6				0.0107
C3H8				0.0004
Molweight [kg/kmol]	28.845	28.3895	27.9482	16.9579

KEMA	Operating Power Generation	CATO-2
project		
instructor		drafterman
proj.nr.		programmer
file D:\SPENCE\SPENCE projecter\CATO-2\FluegasLooping date 11/12/		

Flue gas looping in SPENCE: results

- Obviously dependent on specific GT, amount of looping etc.
- Indicative set of parameters and conditions chosen

<i>Gas composition</i>	<i>Without looping</i>	<i>With looping</i>
Oxygen	12%	5%
Nitrogen	77.5%	72%
Water	6%	15%
Carbon dioxide	3.5%	7%
Flow temperature	50 °C	70-75 °C
Flow volume	600 kg/s	300 kg/s

Parameters at interface 2 & 3

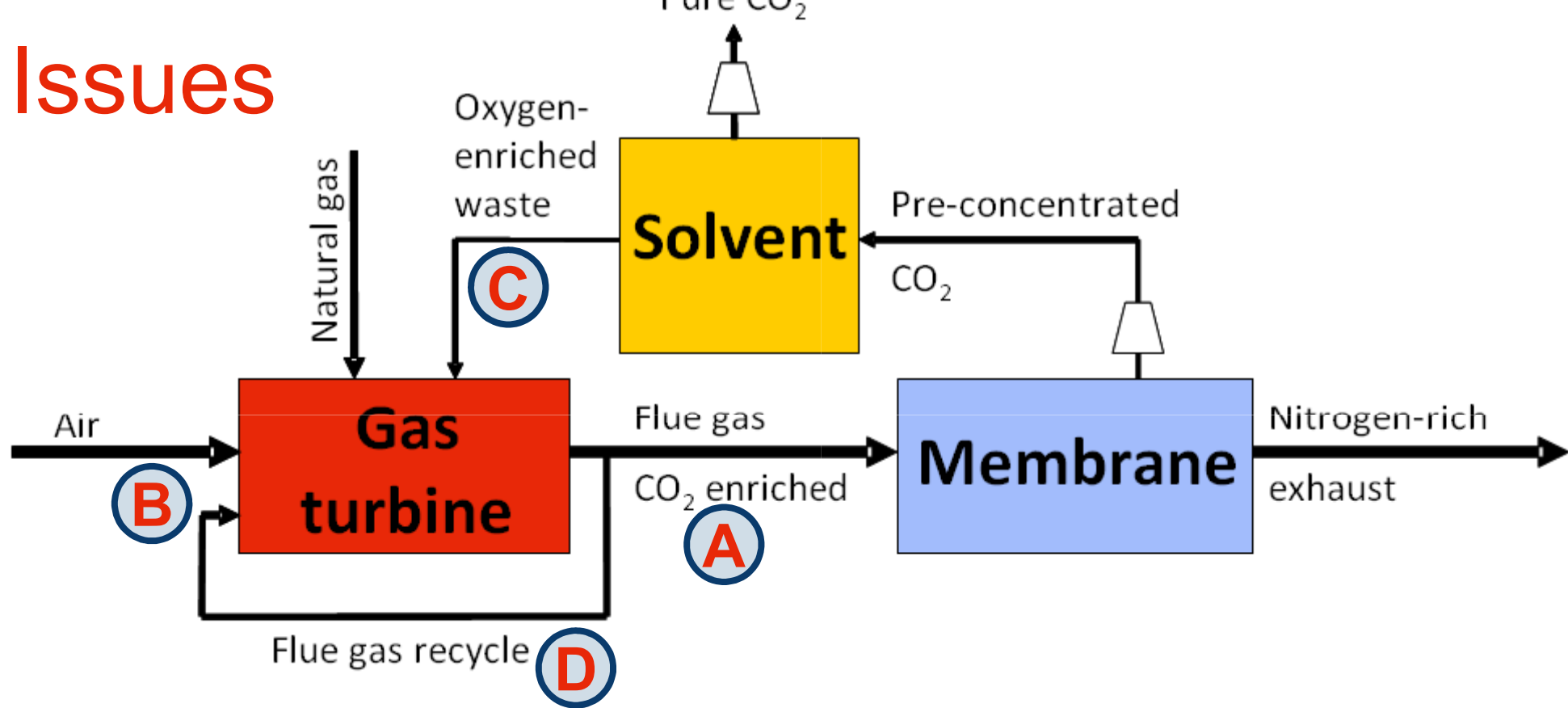
2. Membrane unit – solvent unit

- Optimisation: lower CO₂ permeate purity means lower *membrane* energy use, but higher = lower *absorber* energy
- Preliminary target 50-70% CO₂
- Feasibility investigated by modelling

3. Solvent unit – gas turbine (waste recycle)

- O₂-rich waste stream: how to inject? Construct entrance, add expander, ...?

Issues



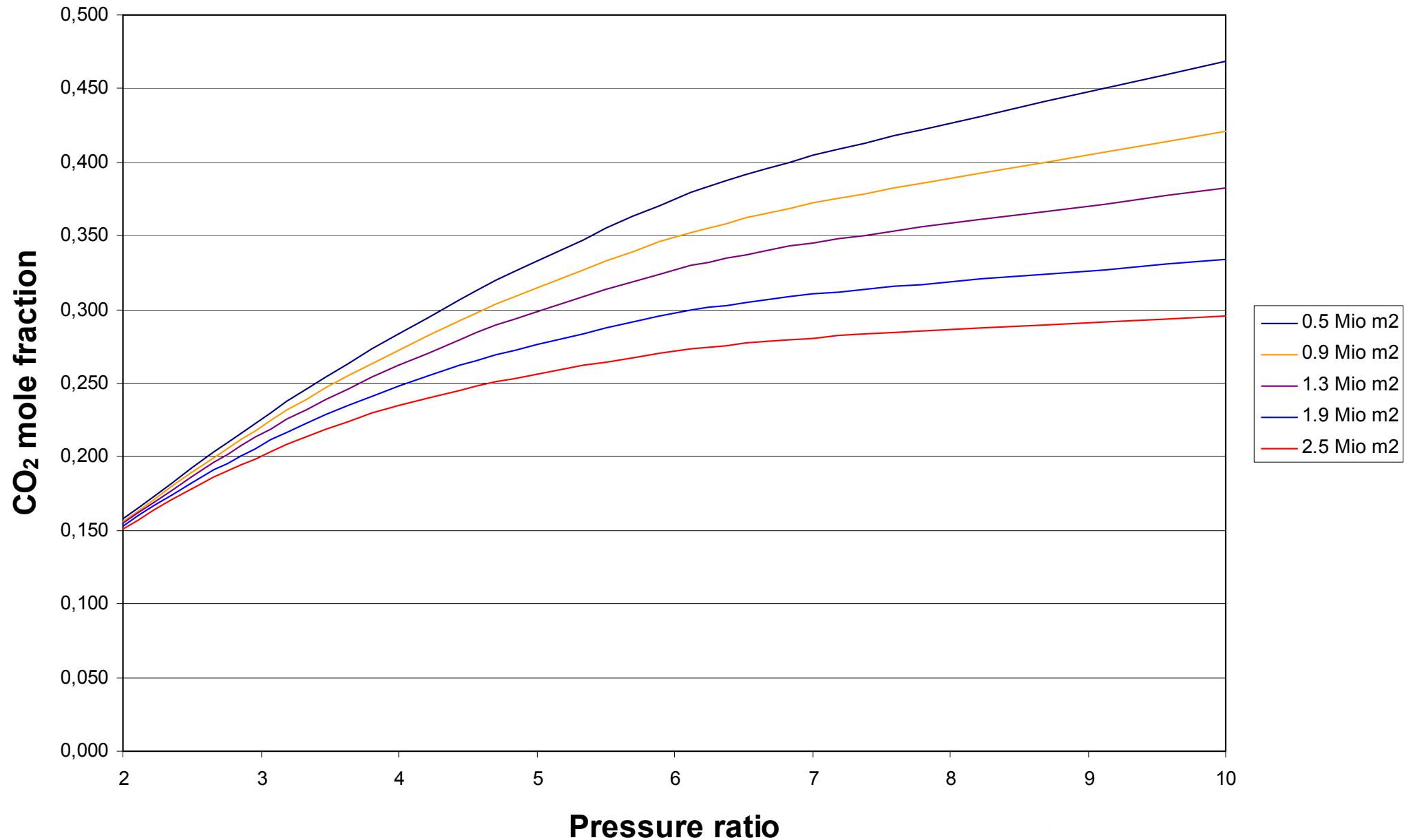
- (A) $T = 100\text{ }^{\circ}\text{C}$ high for polymers; ceramics or heat exchanger.
- (B) SO_2 and trace elements in compressor. Corrosion?
- (C) High pressure O_2 -enriched stream: how to inject in GT?
- (D) Looping means different inlet mix; how to deal with it?
 - Flow / compression / combustion / process startup.

Membrane modelling: starting params

	<i>Permeance</i> <i>[Nm³/m².h.bar]</i>	<i>Selectivity</i> <i>over N₂ (α)</i>
Carbon dioxide	2.7	50
Nitrogen	0.05	-
Oxygen	0.14	2.5

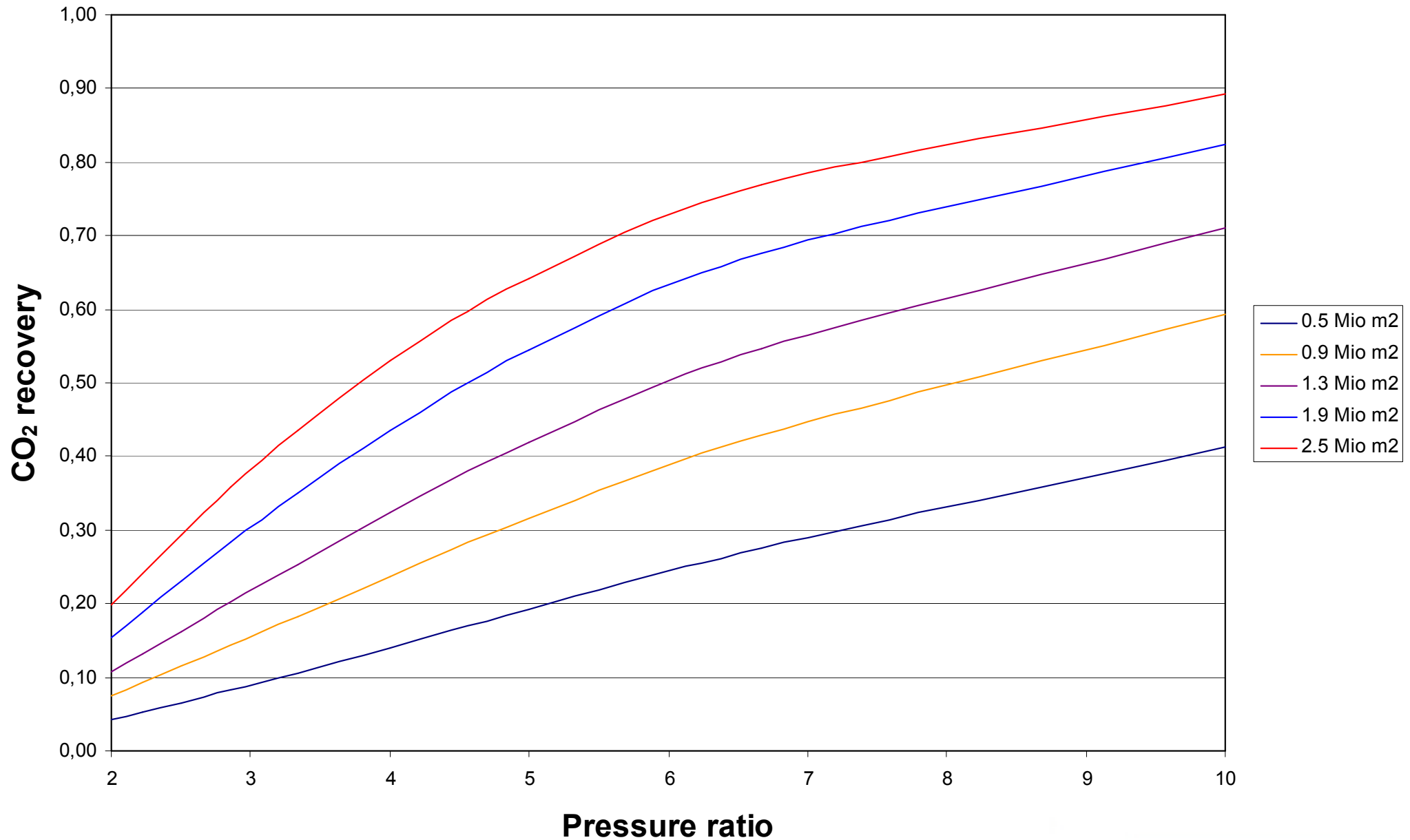
- Corresponding to one commercial preselection membrane
- Input for modelling → determine absorber conditions
- In a later stage: combine with absorber modelling and energetic evaluation

Membrane modelling: example



CO₂ permeate purity versus pressure ratio

Membrane modelling: example

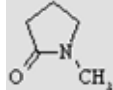
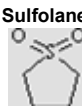
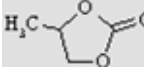
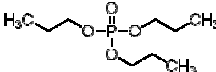


CO₂ recovery versus pressure ratio

Solvent selection for hybrid system

- Most promising look physical/hybrid solvents

- NMP
- Sulfolane
- PC (*less stable, probably unsuitable*)
- Tripropyl Phosphate
- DEPG (*dimethyl ethers of polyethylene glycol*)
- Sulfolane/amine mix

Solvent	m [C _l /C _G]	Viscosity solvent [mPa.s]	Density Solvent [kg/m ³]	Vapour pressure of solvent
NMP (N-Methyl 2 Pyrrolidone) 	3.7 4.03 3.84	1.8	1028	0.00045
Sulfolane 	3.32 2.98 3.07 [303K]	10.10	1260	0.000013
Propylene Carbonate 	2.95 3.66[293K] 4.25 3.55 3.54	2.51	1200	0.000039
Tripropyl Phosphate 	3.93		1012	

- Conclusion: solubility data of oxygen/nitrogen is mostly lacking or very limited

Process modeling of hybrid systems

- Base case:
 - Combined cycle power plant
 - Flue gas recycling
 - MEA absorption process
- Hybrid systems:
 - Combined cycle power plant
 - Hybrid membrane solvent system
 - Commercially available membranes
 - DEPG solvent



For more information:

- Participate in NanoGLOWA's Workshop at ICOM 2011, July 24th, Amsterdam (www.icom2011.org)
- paul.raats@kema.com
- nicktenasbroek@procede.nl