

# Study of adsorption-based CCS systems under wet conditions

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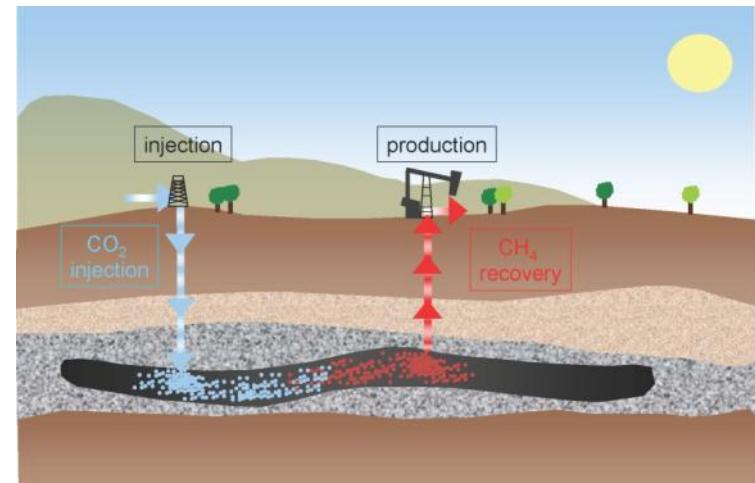
TCCS-6, 15 June 2011,  
Trondheim



# Motivation

Adsorption processes used in CO<sub>2</sub> capture and storage have to deal with the presence of moisture in the system. These include:

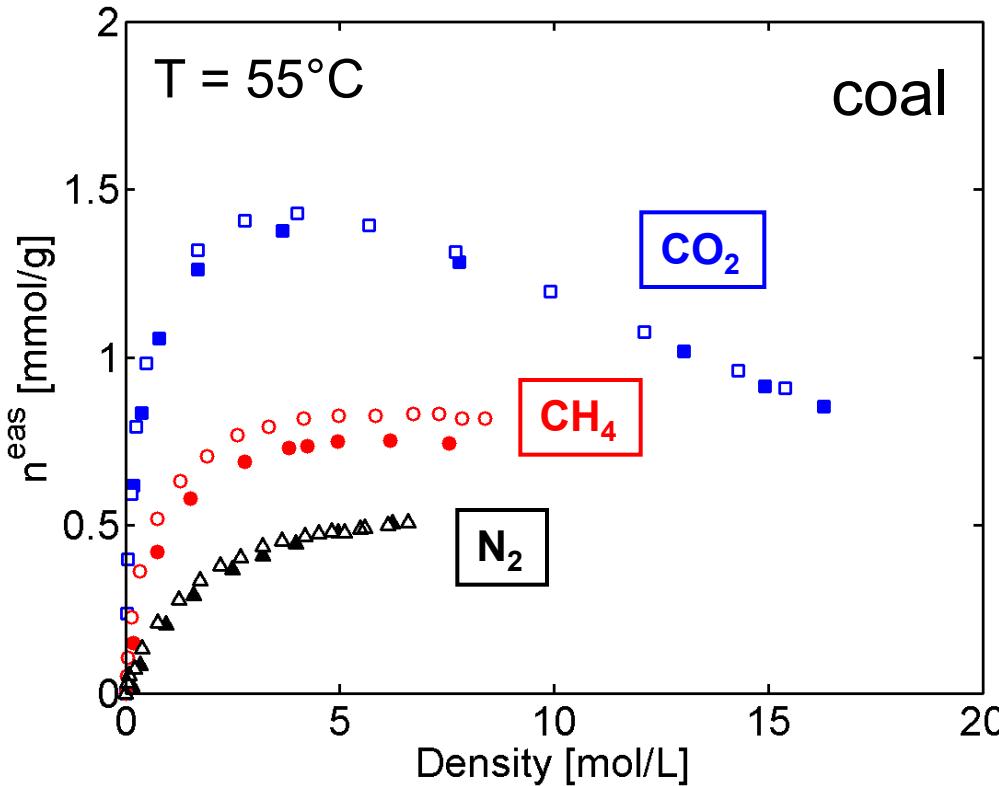
- Flue gases
- Gasification products
- Coal seams used for ECBM



Therefore it is important that we deal with wet sorbents.

# Measurement of dry excess sorption

Dry adsorption-based separation systems are increasingly well studied



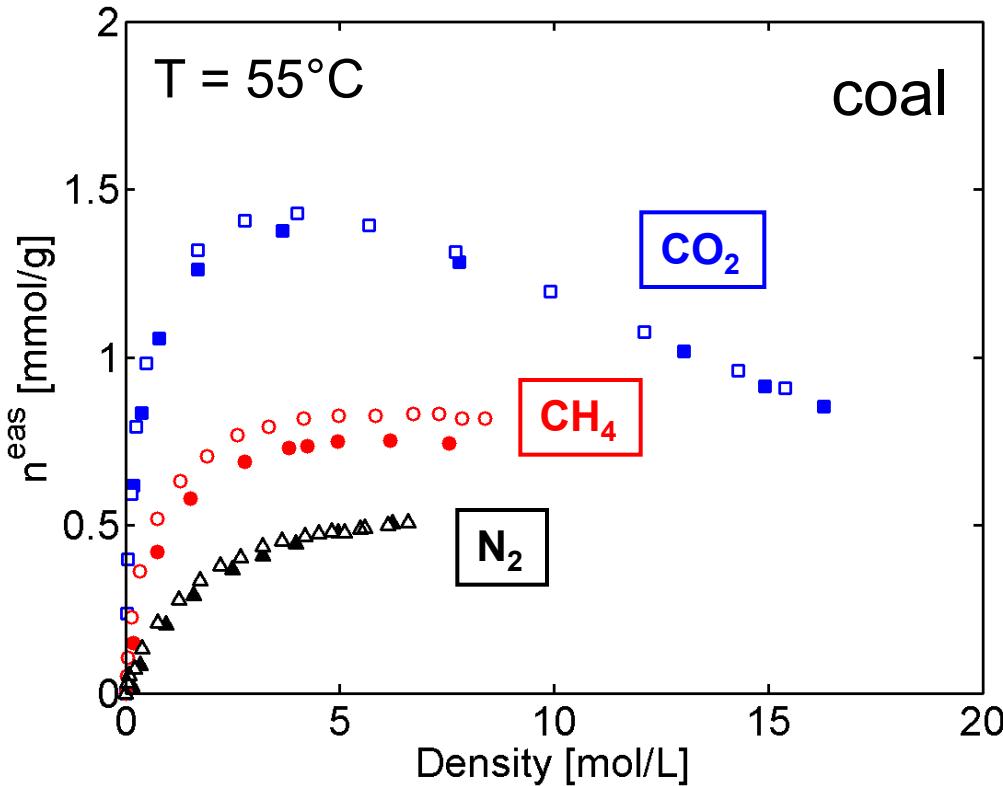
- Methods for measurement are reliable and consistent
- Plot on the left shows data from two separate laboratories
  - CSIRO
  - ETHZ

Sakurovs et al., *Energ. Fuel.* 21 (2007) 992-997

Mazzotti et al., *J. Supercrit. Fluids* 47 (2009) 619-627

# Measurement of dry excess sorption

Excess sorption is the truly measurable quantity



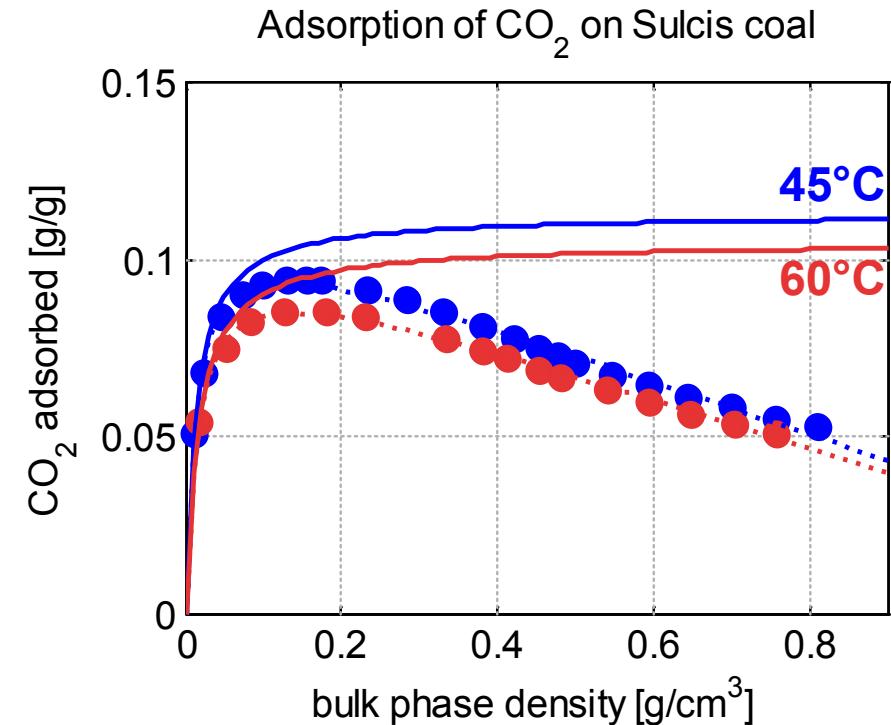
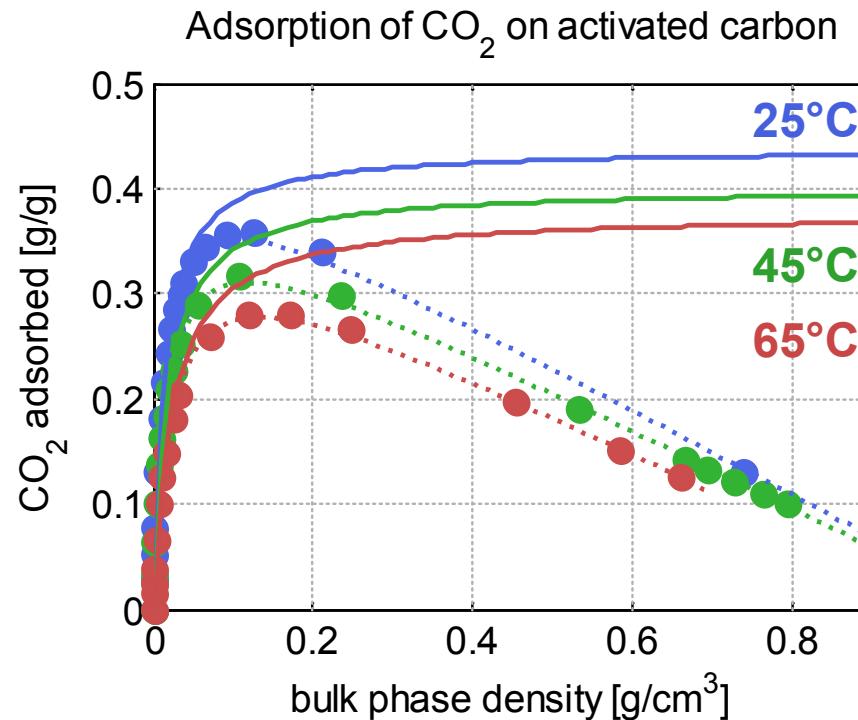
- At high gas densities, the adsorbed phase experiences a buoyancy

$$n^{\text{ex}} = n^a - V^a \rho^b$$

Sakurovs et al., *Energ. Fuel.* 21 (2007) 992-997

Mazzotti et al., *J. Supercrit. Fluids* 47 (2009) 619-627

# Modeling dry gas adsorption on AC and coal



Langmuir model

$$n^{\text{ex}} = \left( \frac{N_{\max} k \rho_b}{1 + k \rho_b} \right) \left( 1 - \frac{\rho_b}{\rho_a} \right)$$

# Research on wet sorbents

		AC	Zeolites	Silica	coal
ETHZ	This work	■	■	■	■
CSIRO	Day et al. 2008				■
Okla. State University	Fitzgerald et al. 2005				■
RWTH Aachen	Kroos et al. 2002				■
Monash	Li et al. 2009		■	■	
Univ. of Maine	Brandani et al. 2004		■		
Univ. of Queensland	Do et al. 2009	■			
Univ. of Illinois	Qi et al. 2000	■			
Vanderbilt University	Qi et al. 2005	■	■		
Univ. of Porto	Ribeiro et al. 2008		■		
Univ. of Stuttgart	Gorbach et al. 2004		■		
Univ. de Mons	Billemont et al. 2011	■			



CO<sub>2</sub>

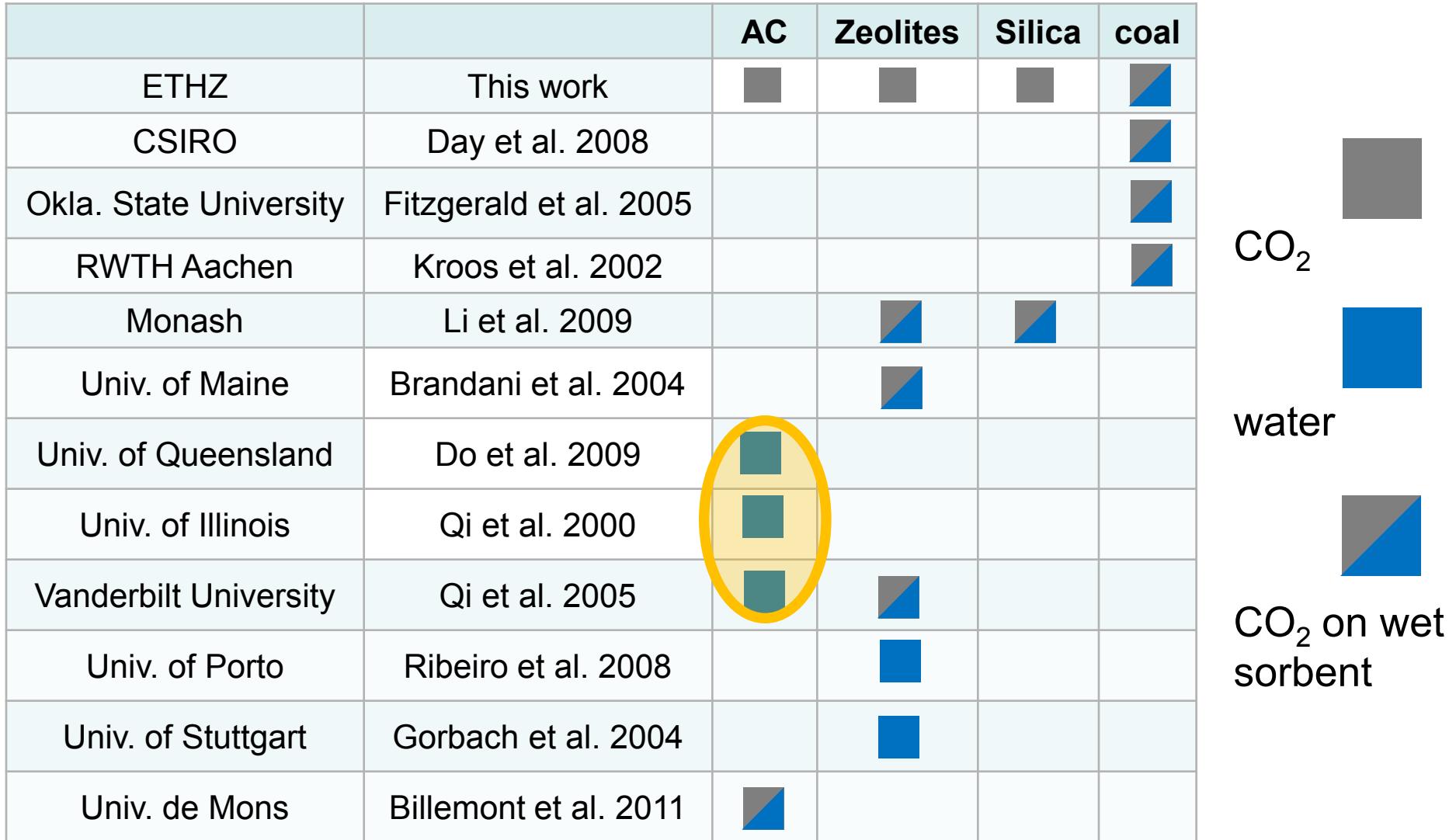


water

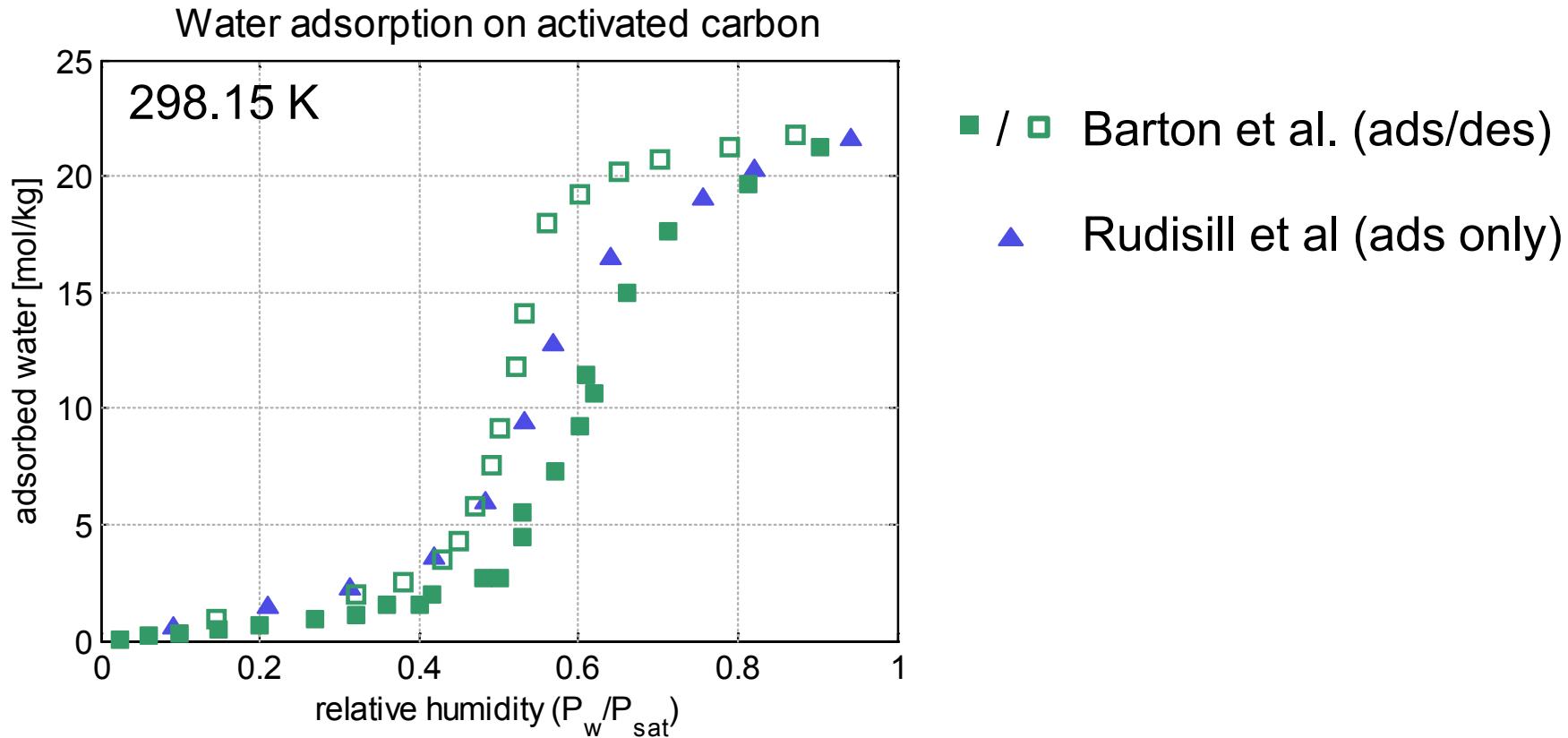


CO<sub>2</sub> on wet sorbent

# Research on wet sorbents

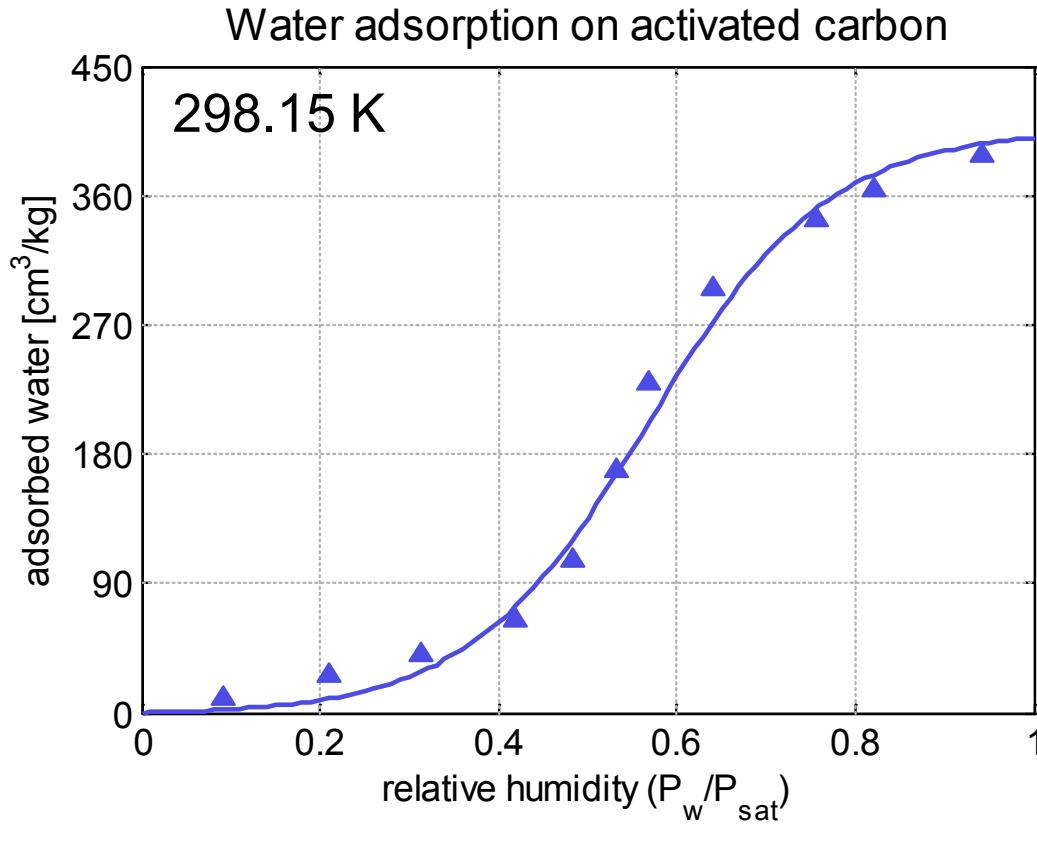


## Pure water data and isotherm on activated carbon



Sources: Barton et al., *Carbon* 22 (1984) 265-272  
Rudisill et al., *Ind. Eng. Chem. Res.* 31 (1992) 1122-30

## Pure water data and isotherm on activated carbon



$$V_w = \frac{V_0}{1 + \exp \left[ k \left( \frac{P_{1/2}}{P_{sat}} - \frac{P_w}{P_{sat}} \right) \right]}$$

where:

- $V_w$  – pore volume filled with water [ $\text{cm}^3/\text{kg}$  sorbent]
- $V_0$  – specific pore volume [ $\text{cm}^3/\text{kg}$  sorbent]
- $P_{sat}$  – saturation pressure of water
- $P_w$  – partial pressure of water
- $k, P_{1/2}$  – model parameters

Sources: (data) Rudisill et al., *Ind. Eng. Chem. Res.* 31 (1992) 1122-30  
 (model) Qi et al. *J. Env. Eng.* 126. (2000) 267-271

# Research on wet sorbents

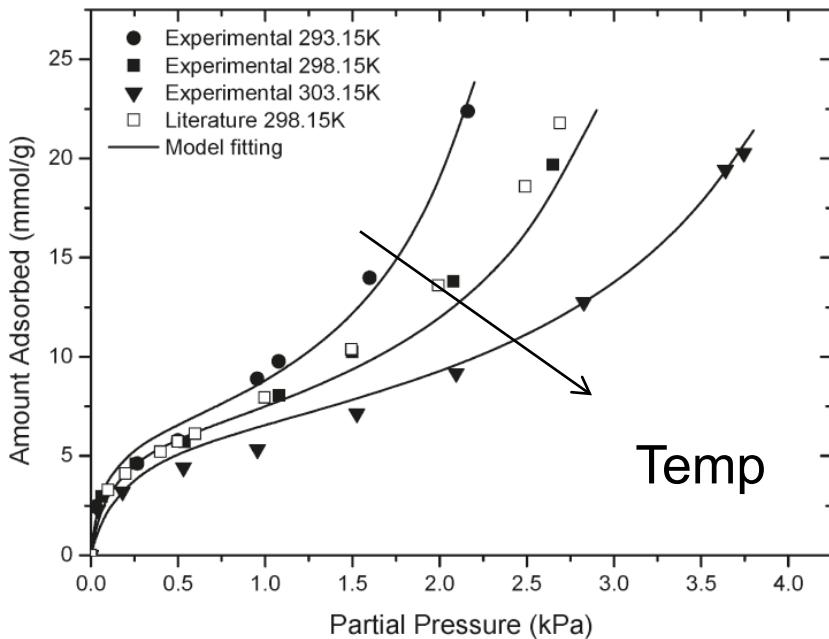
		AC	Zeolites	Silica	coal
ETHZ	This work	■	■	■	■
CSIRO	Day et al. 2008				■
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Univ. of Porto	Ribeiro et al. 2008		■		
Univ. of Stuttgart	Gorbach et al. 2004		■		
Univ. de Mons	Billemont et al. 2011	■			

Legend:

- $\text{CO}_2$
- water
- $\text{CO}_2$  on wet sorbent

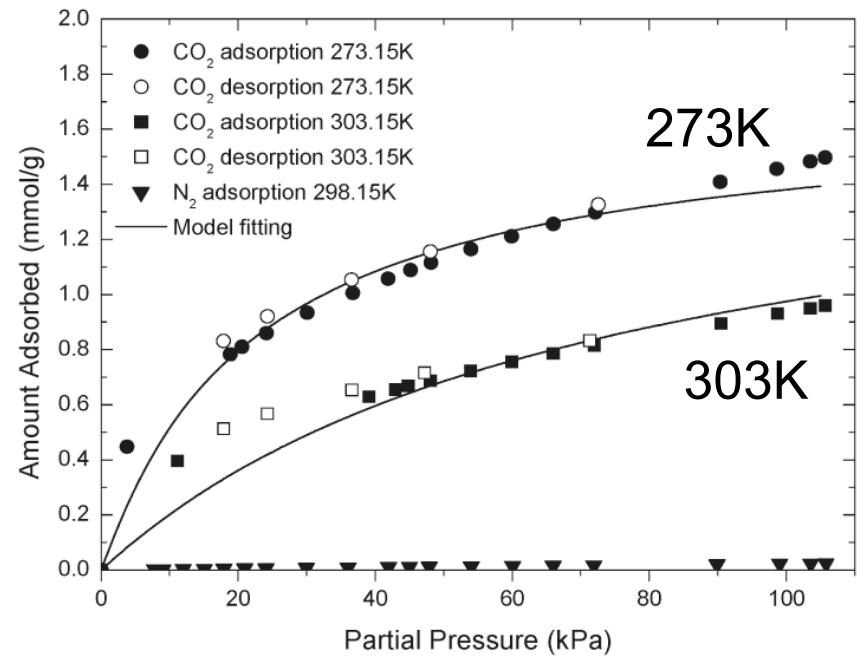
## Data from Li et al. on activated silica

### Pure water isotherms



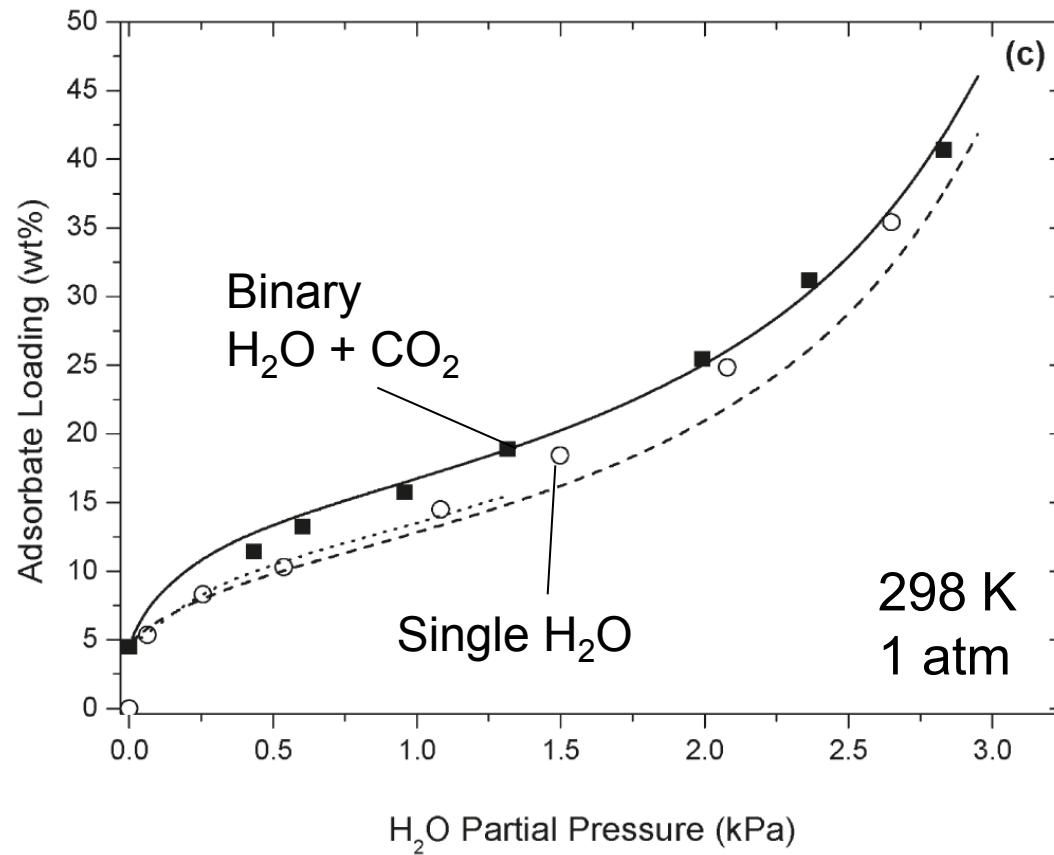
Water adsorption described by modified BET model

### $\text{CO}_2, \text{N}_2$ isotherms



$\text{CO}_2$  adsorption described by Langmuir model

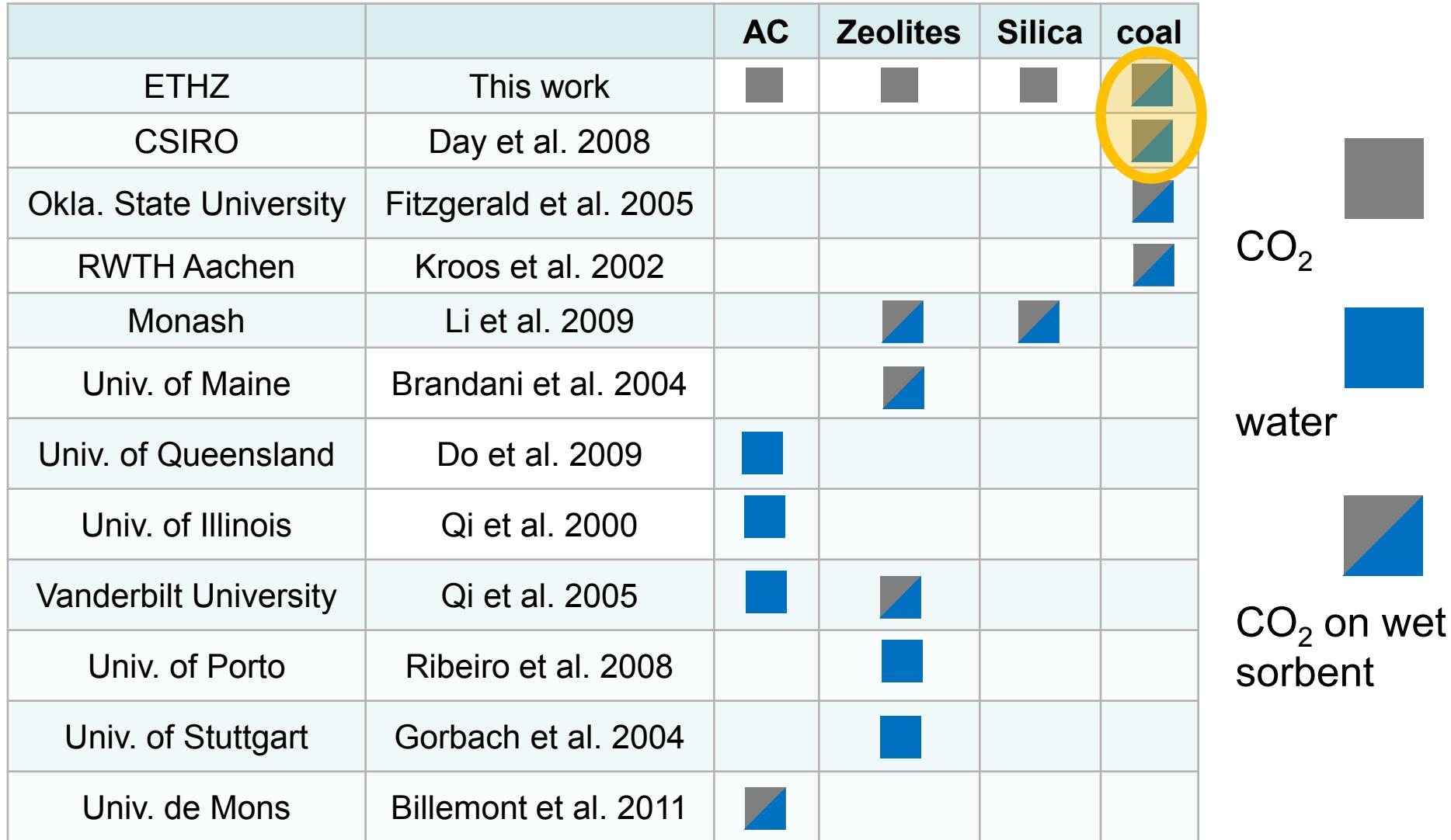
## Data from Li et al. for CO<sub>2</sub>/water isotherm



For a good description, it is necessary to fit parameters for the interaction of water and CO<sub>2</sub>

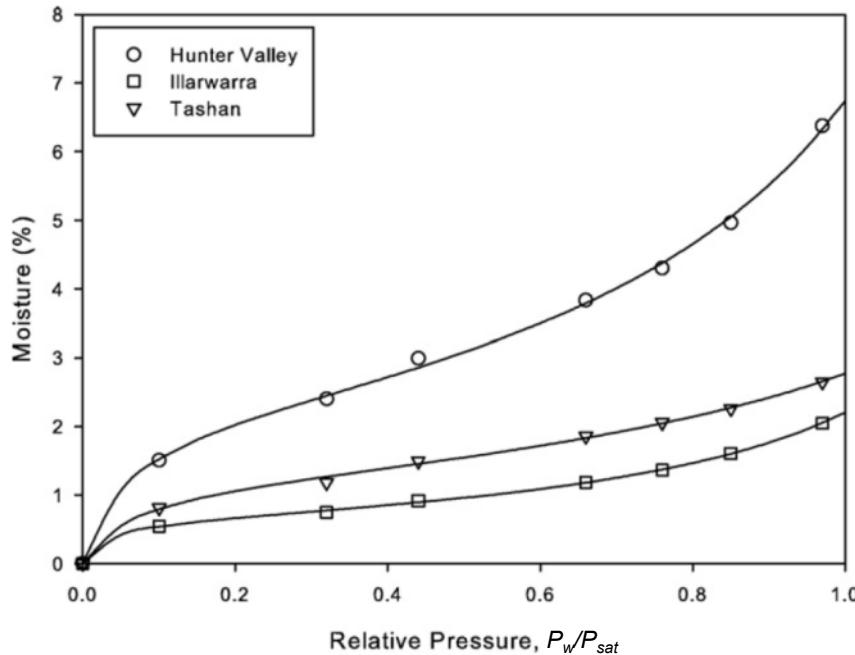
Li et al. *Langmuir* 25 (2009) 10666-10675

# Research on wet sorbents

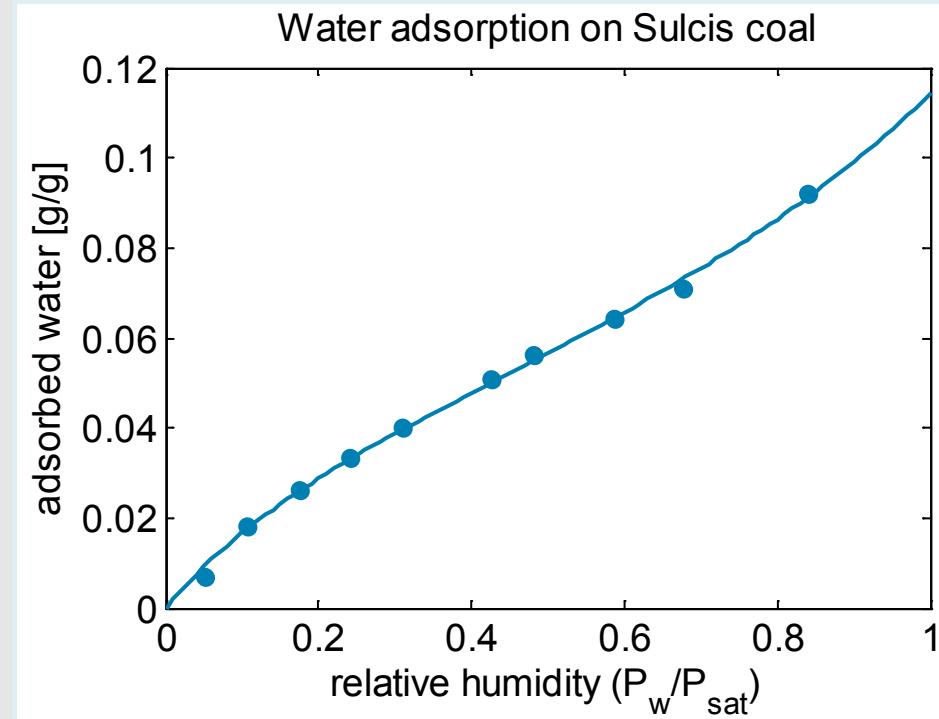


# Work on coal – CSIRO and ETHZ

CSIRO



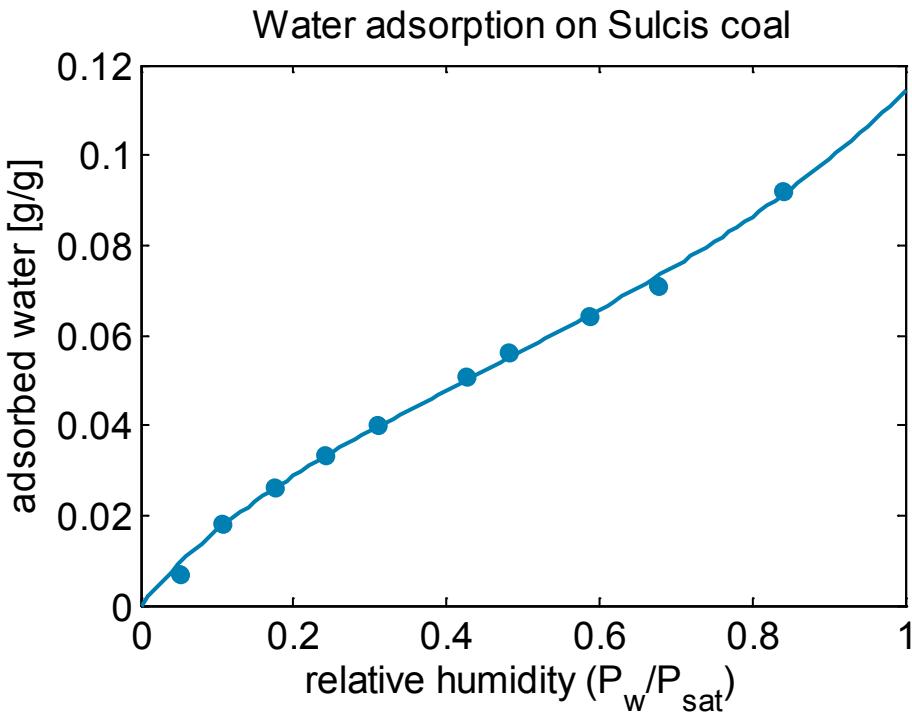
ETHZ



Pure water adsorption data, described by the Guggenheim-Anderson-de Boer model (GAB)

# Model for adsorption of water on coal

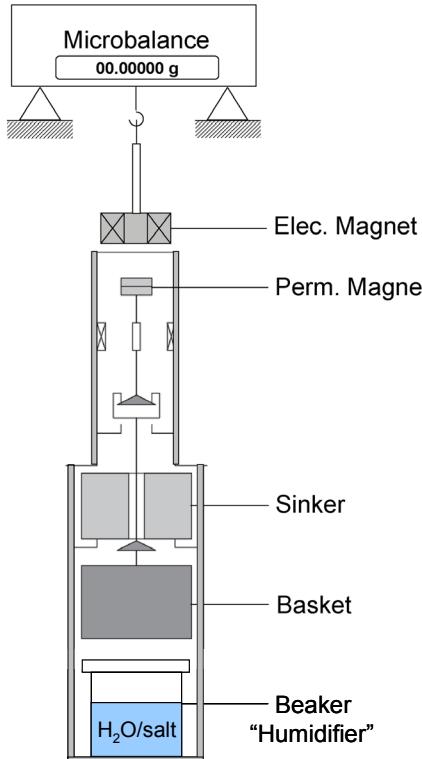
Adsorption of pure water vapor onto coal has been described using the Guggenheim-Anderson-de Boer (GAB) model.



$$W = \frac{W_m C_G \frac{P_w}{P_{sat}}}{\left(1 - K \frac{P_w}{P_{sat}}\right) \left(1 + (C_G - 1)K \frac{P_w}{P_{sat}}\right)}$$

model parameters	
$W_m$ [g/g]	0.032
$C_G$ [-]	6.43
$K$ [-]	0.55

# Measurements of sorption on wet coal



MSB slightly modified to ensure constant humidity during the adsorption experiments.

## Procedure:

- Saturated salt solutions used to control relative humidity.
- Beaker with saturated salt solution inserted at the bottom of the cell.
- Coal sample let saturate under a constant humidity atmosphere for 2 days.
- Coal sample exposed to the high pressure CO<sub>2</sub>.

# Interpretation of the results

- Total excess sorption ( $\text{CO}_2$  and water) with respect to dry sample

$$\begin{aligned}m^{\text{eas}}(\rho^{\text{b}}, T) &= M_1(\rho^{\text{b}}, T) - M_1^0 + \rho^{\text{b}}(V^{\text{met}} + V_0^{\text{coal}}) \\&= m^* - \rho^{\text{b}}\Delta V^*\end{aligned}$$

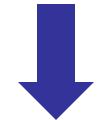
- $m^* = m_{\text{CO}_2}^{\text{a}} + m_w \rightarrow$  total sorption
- $\Delta V^* \rightarrow$  total volume increase due to adsorption

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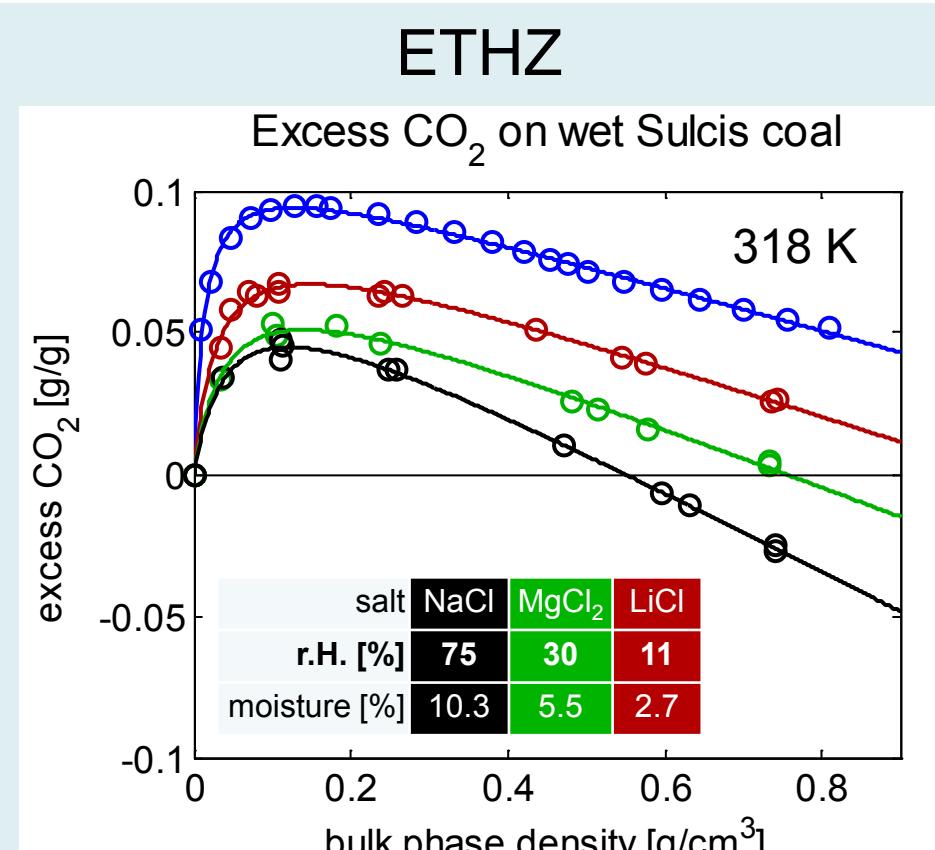
- $m^* = m_{\text{CO}_2}^{\text{a}} + m_w \rightarrow$  total sorption
- $\Delta V^* \rightarrow$  total volume increase due to adsorption

  $m_w$  is constant

- $\text{CO}_2$  excess sorption

$$\begin{aligned}m_{\text{CO}_2}^{\text{eas}}(\rho^{\text{b}}, T) &= M_1(\rho^{\text{b}}, T) - (M_1^0 + m_w) + \rho^{\text{b}}(V^{\text{met}} + V_0^{\text{coal}}) \\&= m_{\text{CO}_2}^{\text{a}} - \rho^{\text{b}}\Delta V^*\end{aligned}$$

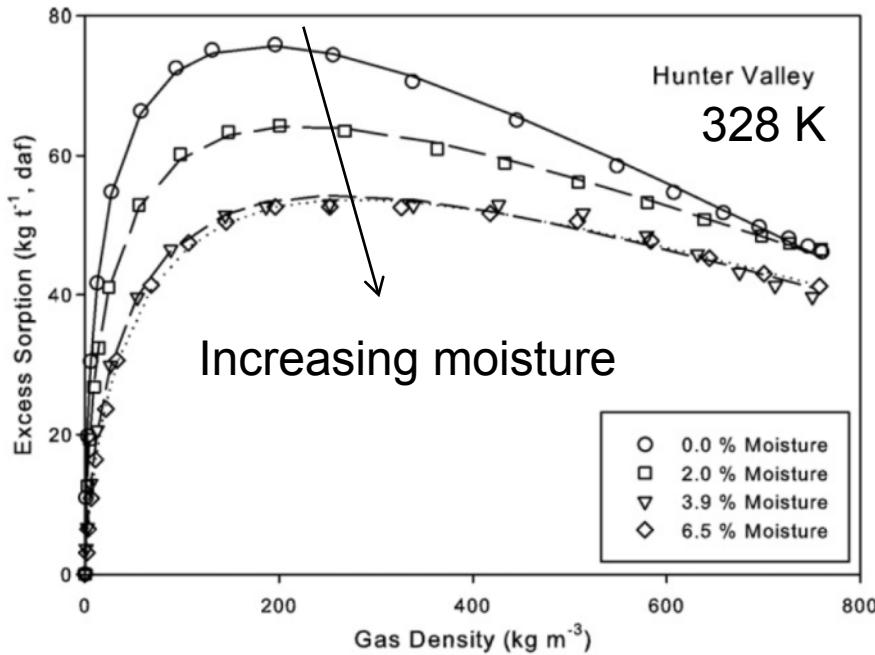
# CO<sub>2</sub> adsorption on wet coal



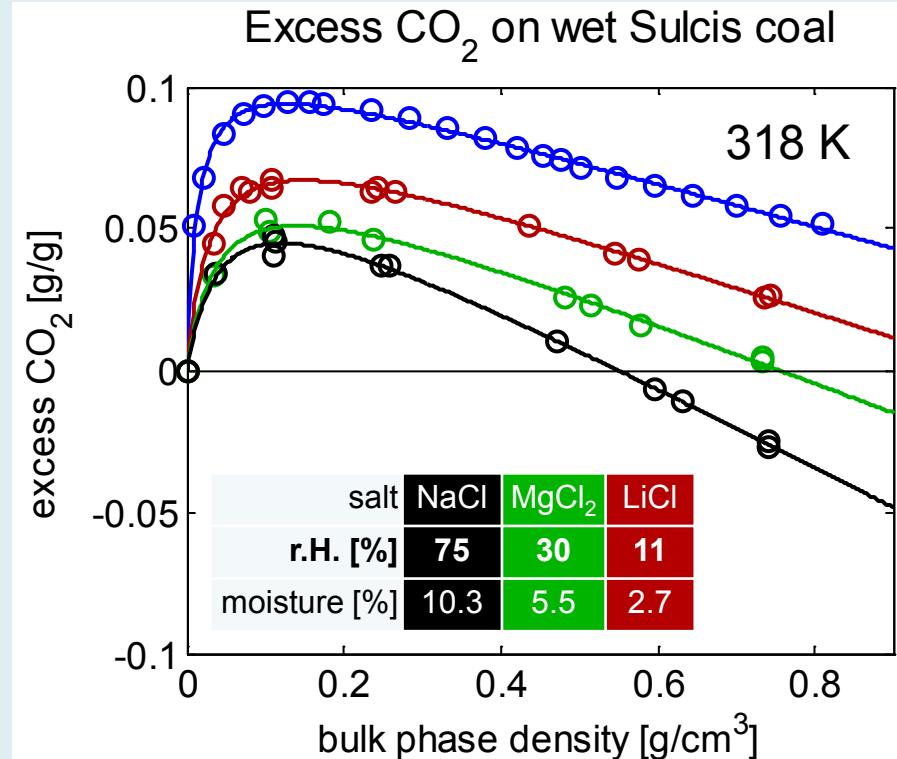
excess calculated with  
respect to *dry* sample

# CO<sub>2</sub> adsorption on wet coal

CSIRO



ETHZ



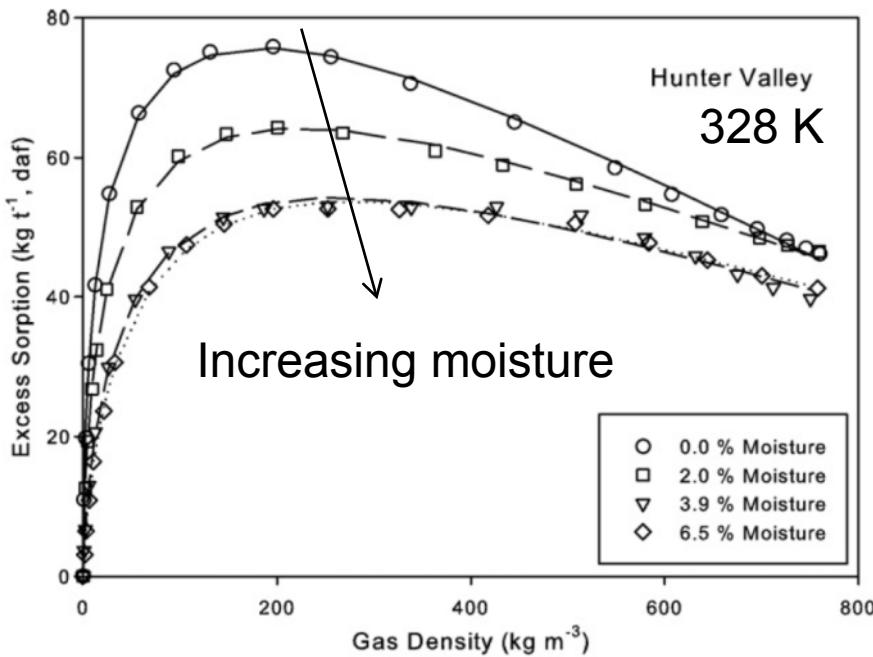
excess calculated with  
respect to *wet* sample

Day et al., Int. J. Coal Geol. 74 (2008) 203-214

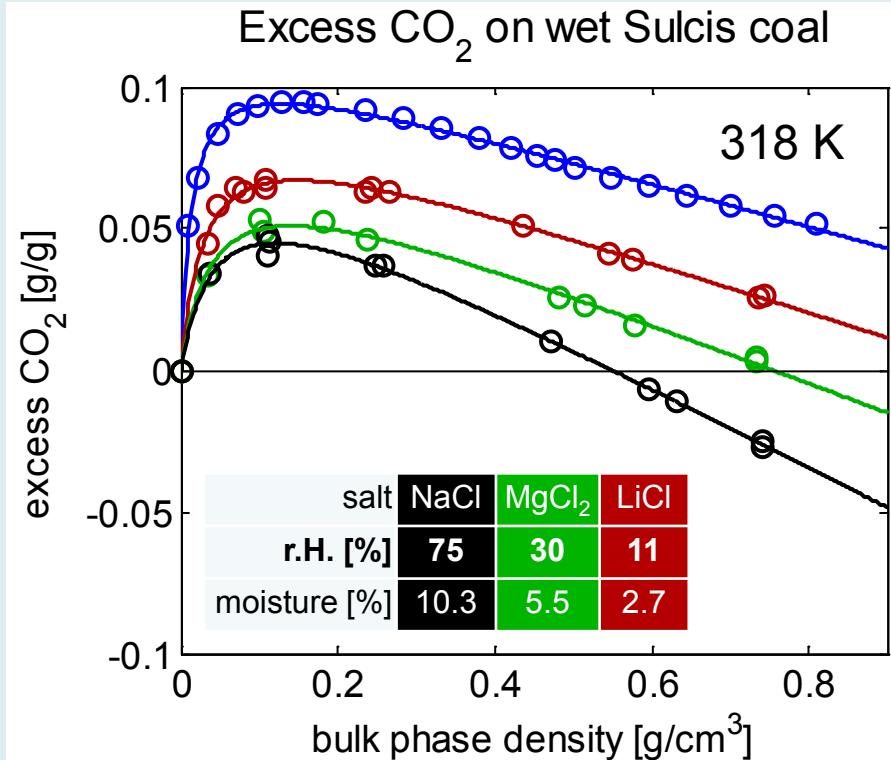
excess calculated with  
respect to *dry* sample

# CO<sub>2</sub> adsorption on wet coal

CSIRO

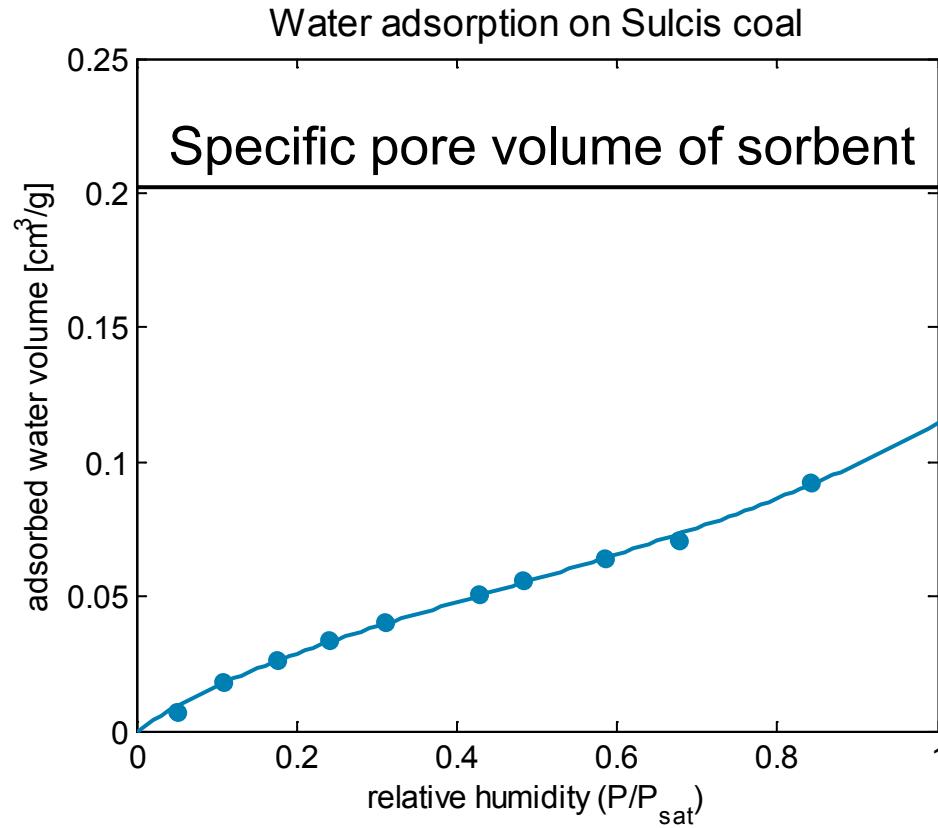


ETHZ



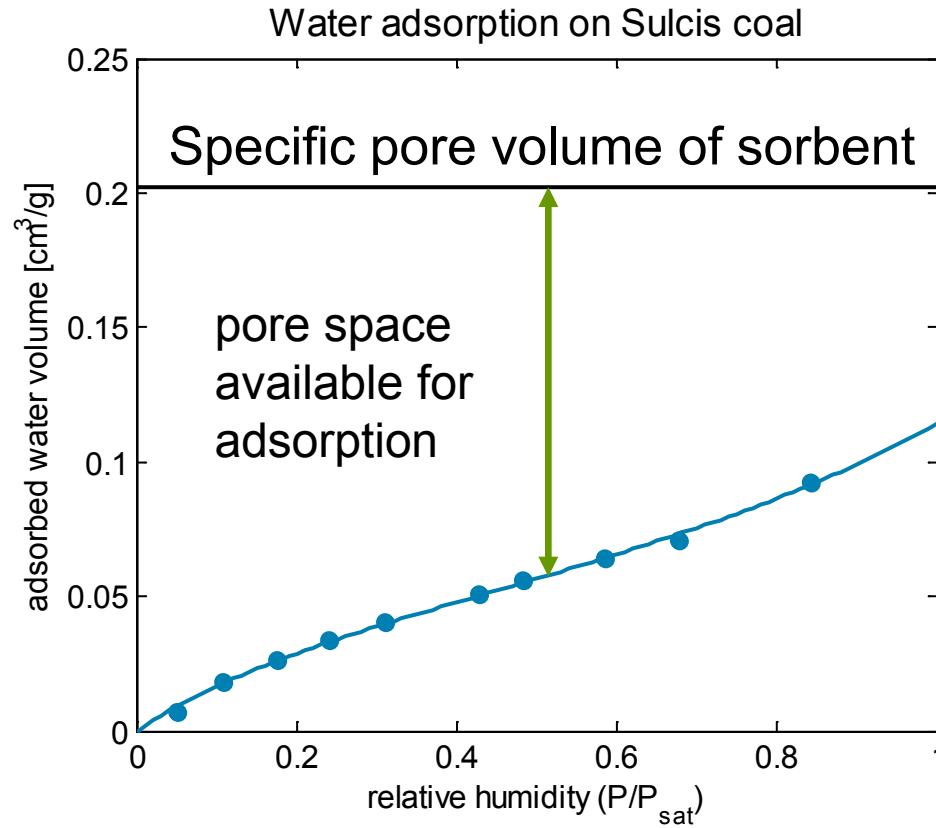
Separate model parameters fit to each moisture level

# Proposed modeling approach



$$V_w = \frac{W_m C_G \frac{P_w}{P_{sat}}}{\left(1 - K \frac{P_w}{P_{sat}}\right) \left(1 + (C_G - 1)K \frac{P_w}{P_{sat}}\right) \rho_w}$$

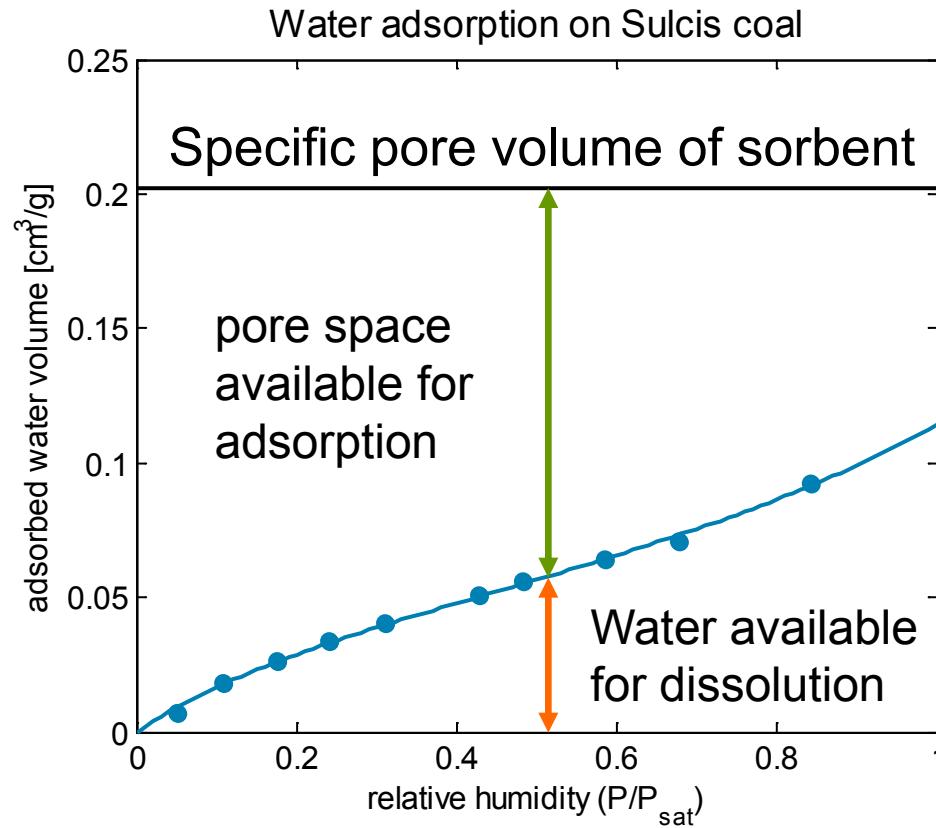
# Proposed modeling approach



$$n_{CO_2,L} = \frac{N_{CO_2} k \rho_{CO_2}}{1 + k \rho_{CO_2}}$$

$$V_w = \frac{W_m C_G \frac{P_w}{P_{sat}}}{\left(1 - K \frac{P_w}{P_{sat}}\right) \left(1 + (C_G - 1)K \frac{P_w}{P_{sat}}\right) \rho_w}$$

# Proposed modeling approach

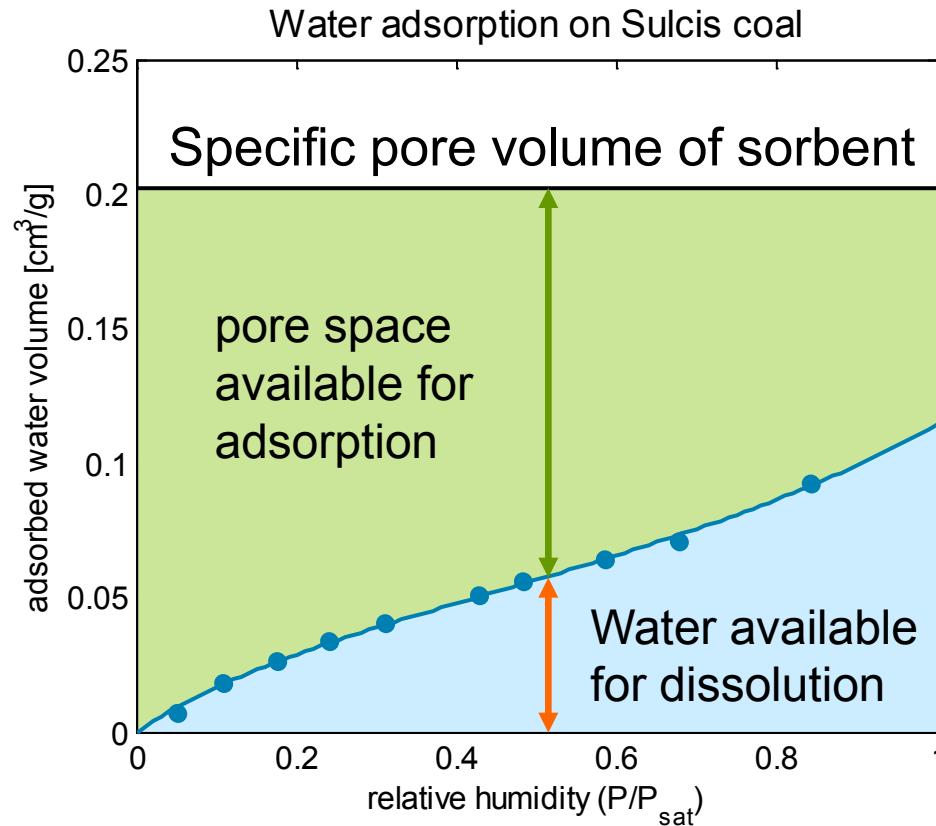


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$$C^{diss} = [\text{CO}_{2(\text{aq})}] = k_H(T) f_{CO_2}$$

# Proposed modeling approach



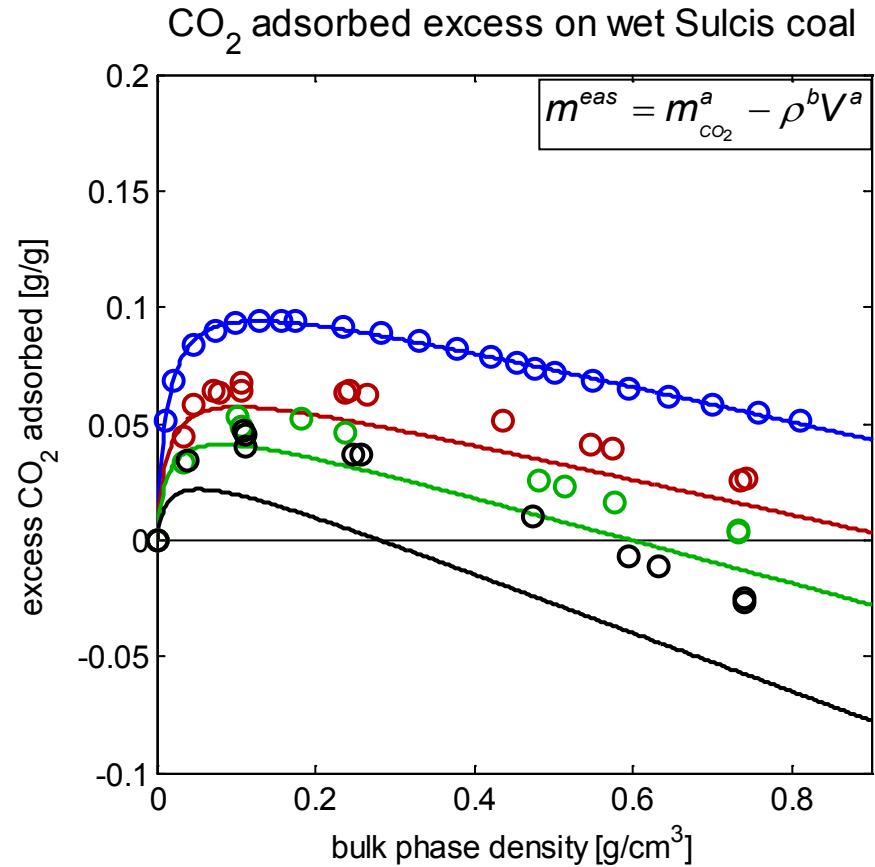
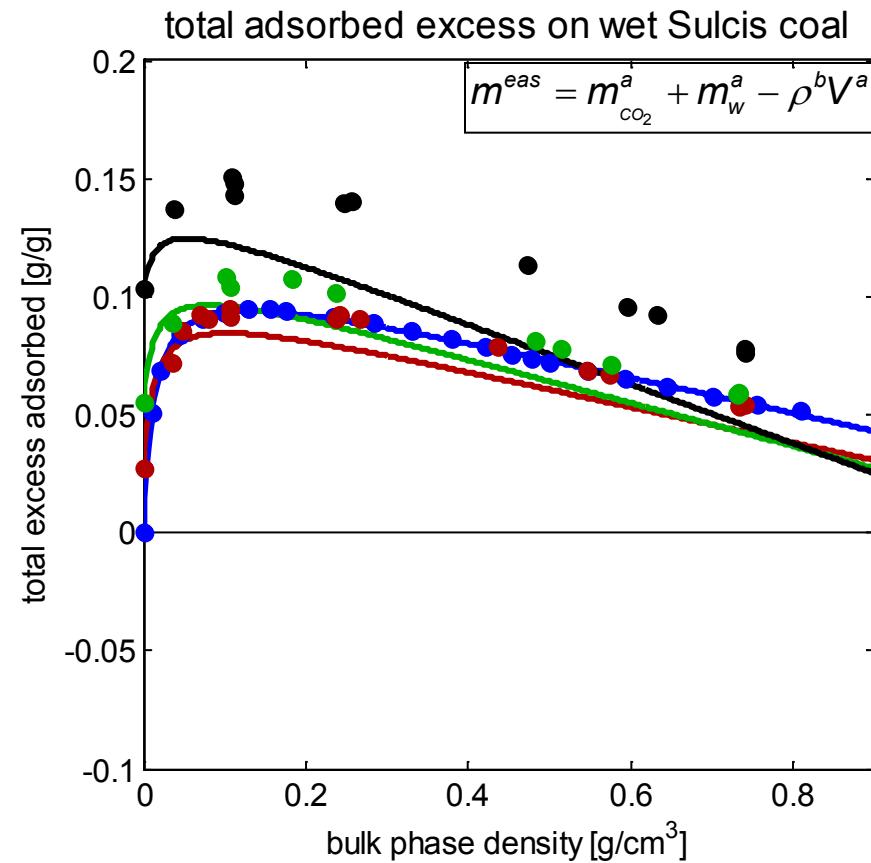
$$n_{CO_2,L} = \frac{N_{CO_2} k \rho_{CO_2}}{1 + k \rho_{CO_2}}$$

$$V_w = \frac{W_m C_G \frac{P_w}{P_{sat}}}{\left(1 - K \frac{P_w}{P_{sat}}\right) \left(1 + (C_G - 1)K \frac{P_w}{P_{sat}}\right) \rho_w}$$

$$C^{diss} = [\text{CO}_{2(\text{aq})}] = k_H(T) f_{CO_2}$$

$$n_{CO_2} = V_w C^{diss} + \left( \frac{V_0 - V_w}{V_0} \right) n_{CO_2,L}$$

# Results of the proposed model



# Conclusions

- Proposed model delivers encouraging results
  - Extension to other adsorbent materials
- Model is simple enough to have low computational requirements
  - Use in simulation software for separation columns
- Water/gas interactions still need to be better understood
- Assumption of constant water content needs testing
  - Modified experimental procedure
  - Monitoring of gas phase composition