

Carbon-free firing of state-of-the-art gas turbines: technology readiness, potential impact and research challenges



Andrea Gruber & James Dawson

TCCS-10, Trondheim, June 18-19 2019





Outline

- The context: zero-emission thermal power cycles
- Carbon-free firing of gas turbines: technology readiness & potential impact
- Research challenges: stabilize flame, minimize fuel-dilution and emissions

Acknowledgments:



Air-breathing thermal power cycles: powering the world



2-stroke, low-rpm ICEs:

- 10-80 MW
- Cycle efficiency ~ 55%
- HFO, Diesel and NG
- MAN 'upgrades' to NH₃



Gas + steam turbine (combined cycle):

- 50-800 MW
- Cycle efficiency ~ 63%
- 6100 TWh installed capacity (NG-fired)
- Carbon-free firing of GTs 'within grasp'



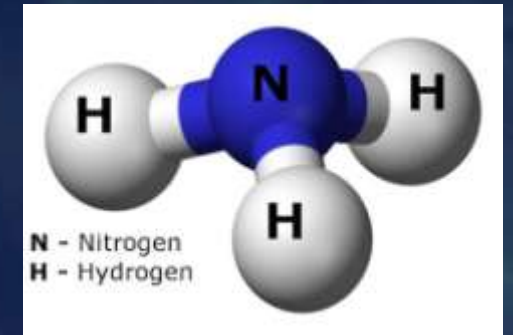
High-bypass turbofan engine:

- 100-600 kN thrust
- Cycle efficiency ~ 30-36%
- +30000 CFM56 sold
- Enough biofuel?

Thermal cycles are not intrinsically dirty but as clean as the fuel and combustion technology they utilize!



Why hydrogen (and ammonia)?



Hydrogen (H₂)

- H₂ to power completes pre-combustion CCS value chains
- Provides an optimal energy-carrier in large-scale energy storage schemes for integration of non-dispatchable & intermittent RES (power-to-gas-to-power)
- Effectively a bridge between “fossil” and “green” energy sources (blue and green H₂)

Ammonia (NH₃)

- Convenient H₂-carrier for remote transport and/or long-term storage in all of the above
- Represent a useful H₂-diluent (for stable combustion in gas turbines)

Both are carbon-free fuels: zero CO₂ emissions!

Why gas turbines?

High cycle efficiency up to ~63% in CCGT

Switch to H₂ (or NH₃) only requires burner modifications

Well-established reliability and lifetime +25 yrs

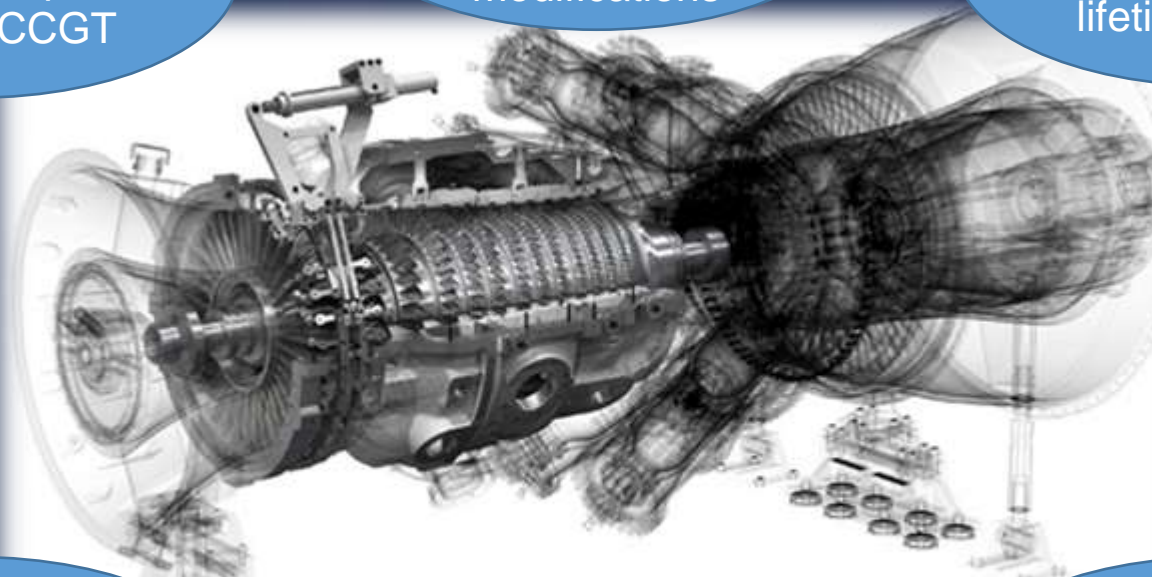
Relatively «low cost» at 200-1200 USD/kW_e (SCGT-CCGT)

Fast response to load variations up to ~50 MW_e/min

High fuel flexibility from liquid HC and NG to H₂ and NH₃

Unmatched specific power ~2-10 kW/kg

GTs handle well impurities & «minor» species in fuel (e.g. CO₂)



SGT-750 / Courtesy of Siemens



H₂-fired GTs: brief history and state of the art

FP6 ENCAPCO2
(2004-2009):
preliminary
investigations

FP7 DECARBit and
BIGH2/Phase I&II
(2008-2015): 50% by
vol H₂ in NG is
achieved in rig

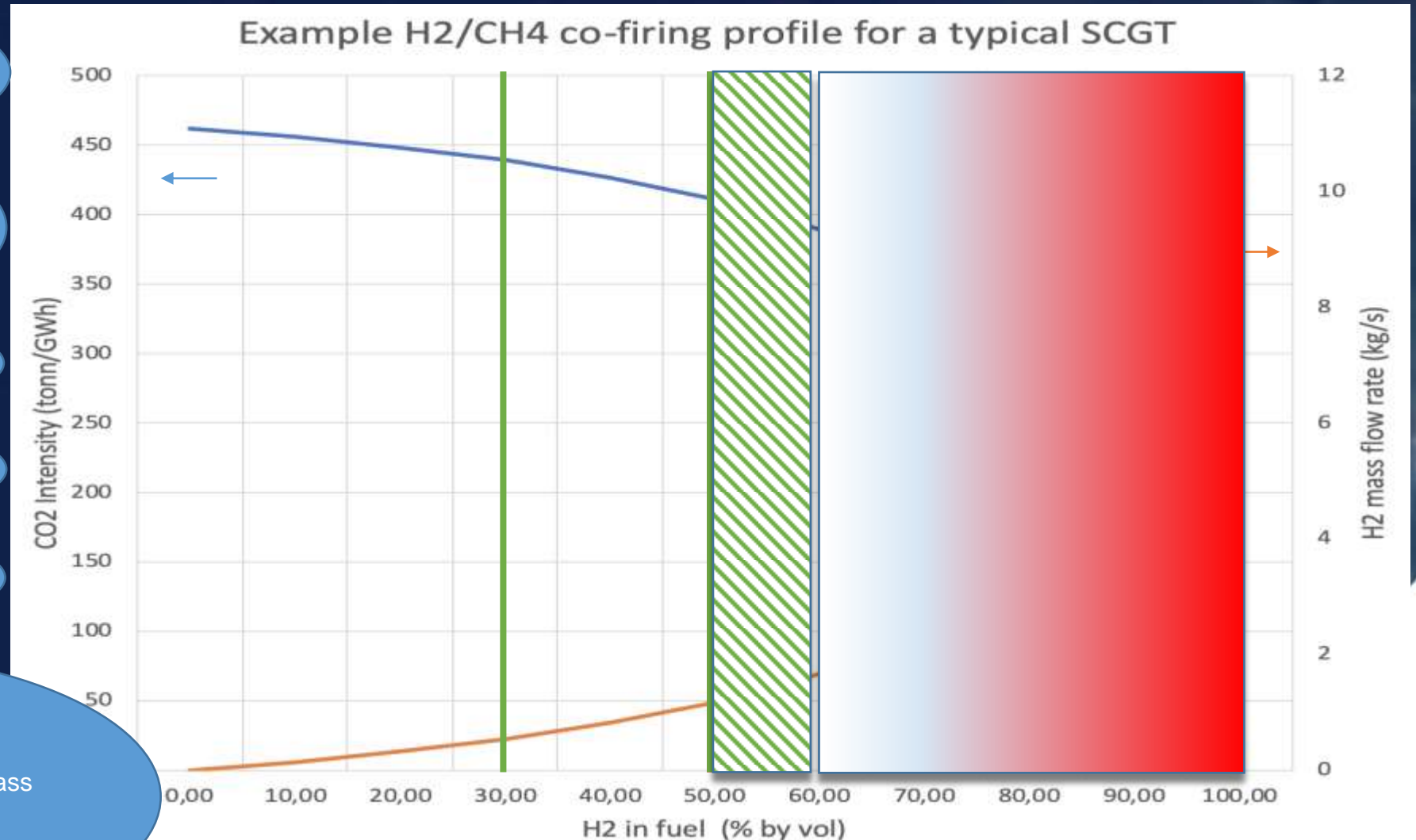
MHPS provides 30% H₂
in H-class GT (2017)

AE provides 50% H₂ in
H-class GT36 (2018)

SIT provides 50-60% H₂
in GT600/700/800 (2018)

The race is on (2019)!

- AE achieves 70% H₂ in rig @ H-class temperature (baseload GTs)
- SIT achieves 100% H₂ in rig @ F-class temperature (industrial GTs)



GT OEMs committed to 100% H₂ firing by 2030

GT-industry's expertise and resources committed to achieve 100% H₂, however:

- High-pressure/full-size R&D of GT combustion system is extremely expensive and cash-flow is limiting factor
- Interest by committed customers is needed
- Public intervention is beneficial in the form of
 - A legal framework for non-conventional fuels
 - Set goals, do not pre-select technologies
 - Public co-funding of RD&D efforts



The challenge: the high reactivity of hydrogen

Key factors in design of gas turbine combustors include:

- the combustion velocity (flame speed)
- the fuel reactivity and flammability (time and composition needed for ignition)
- the flame temperature (controlling dilatation and acceleration of the working fluid)

Stoichiometric combustion properties at 1 bar and 300 K	CH ₄	H ₂	NH ₃
Flame Speed	40 cm/s	300 cm/s	20 cm/s
Flame Temperature	~2200 K	~2400 K	~2050K
Flammability Limits (by volume %)	5-15	4-75	15-28
Ignition Energy (mJ)	0.28	0.011	680
Ignition Delay Time (ms) @ 1000K/17bar	45.6	6.2	N/A
LHV (MJ/Kg)	50	120	18





How to address hydrogen's high reactivity

Two strategies at hand for clean, stable and efficient hydrogen combustion in GTs:

- “handle H_2 reactivity” (e.g. combustion staging) → relies on autoignition for flame stabilization
- “reduce H_2 reactivity” (e.g. fuel blending) → rely on inert gases or less reactive fuels

SINTEF & NTNU work together with gas turbines OEMs at both approaches:

- Auto-ignition H_2 flame stabilization in FME NCCS/Task 5 (+Reheat2H2 KPN) w/Ansaldo
- Hydrogen/nitrogen/ammonia-firing of a Siemens DLE burner (BIGH2/Phase III)
- New activity starting-up in LowEmission Petrosenter w/Siemens & Ansaldo



Example: H₂ co-firing in DLE burner

Siemens Gas Turbines Hydrogen capability with DLE burner

SIEMENS
Ingenuity for life

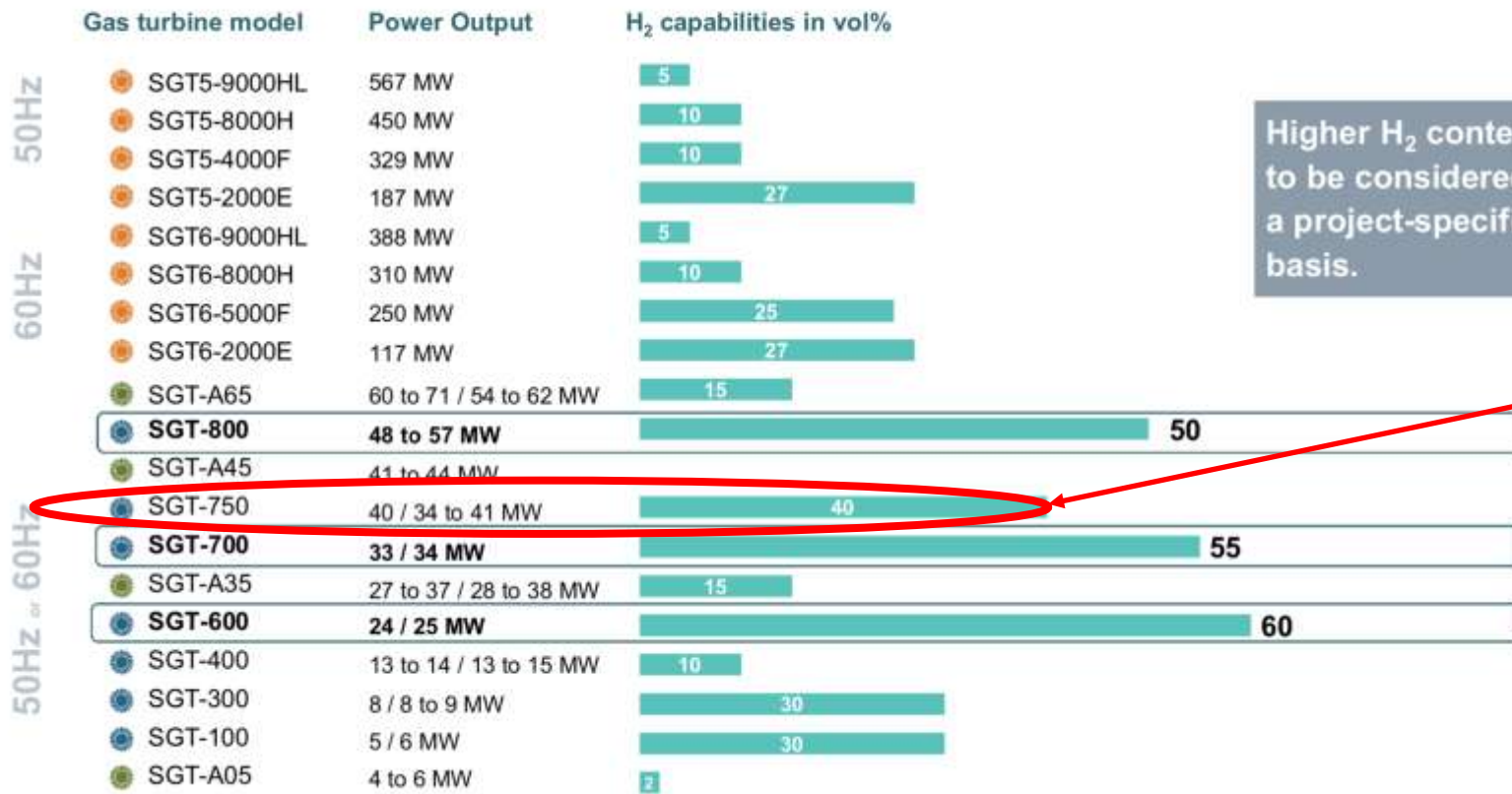
Heavy-duty gas turbines



Industrial gas turbines



Aeroderivative gas turbines



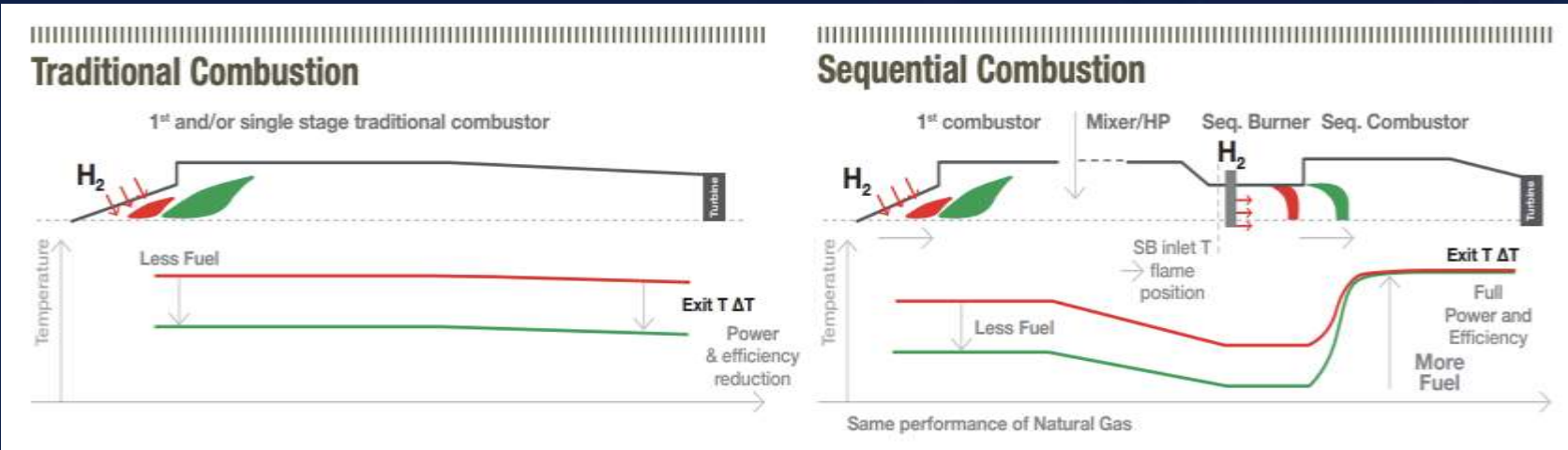
Higher H₂ contents to be considered on a project-specific basis.

BIGH2
Phase III

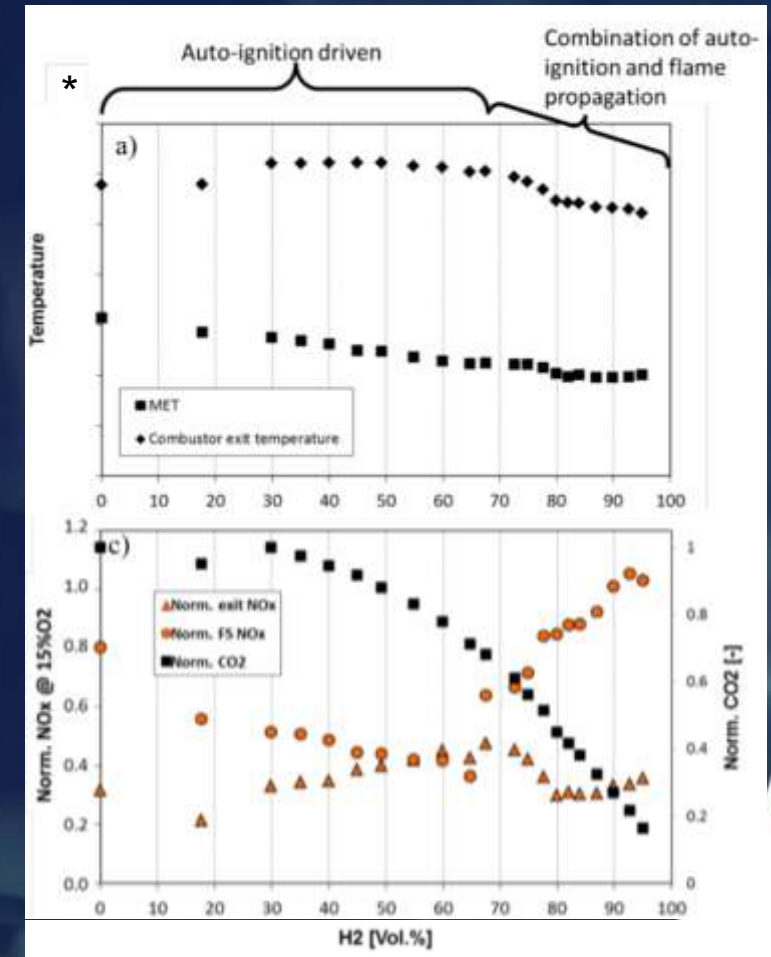


Example: staged combustion

- Ansaldo's reheat scheme: firing temperature of 1st stage controls ignition time (t_{ign}) and flame stabilization in 2nd stage!



Courtesy of Ansaldo Energia



Bottom line: large-scale power generation with hydrogen-rich fuels is feasible and R&D can help filling the remaining gap!





Technical challenges for H₂/H₂-rich fuels

Current GTs are highly “*tuned*” to burn NG-air mixtures and transitioning to H₂ rich fuels needs to maintain:

- low NO_x capabilities
- combustor stability and operating range
- avoid de-rating the engine
- improve dynamic loading (turn down/part load)

*Requires different combustor design strategies for H₂ and H₂ rich fuels
– large innovation potential!*





Knowledge gaps

Scientific (independent of combustor geometry)

- The effect of pressure & temperature of H₂/H₂-rich mixtures on:
 - Flame speed, ignition delay times, chemical kinetics, turbulence-chemistry interaction

Technical (some geometry dependence)

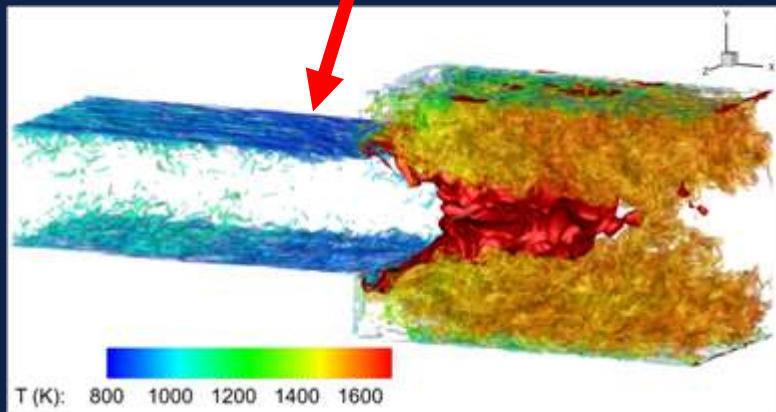
- Ensure stabilisation of H₂/H₂-rich flames to prevent:
 - Static instabilities: flashback and blow-off
 - Dynamic instabilities: thermoacoustic oscillations



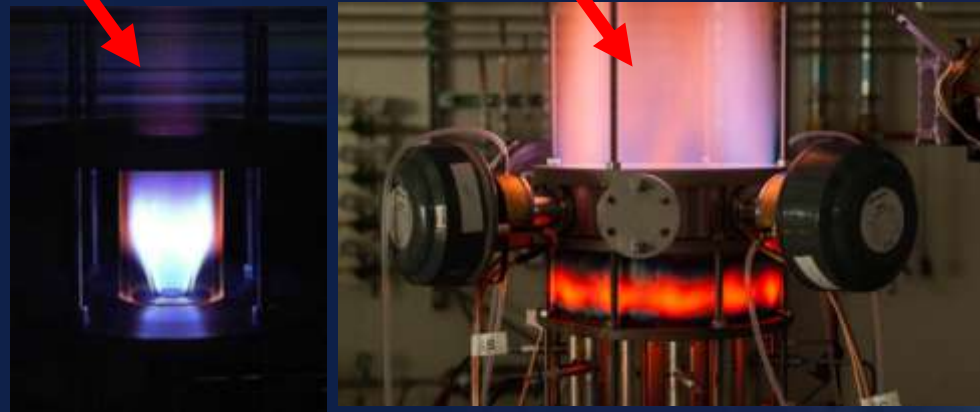
Research methodology

- To understand static and dynamic instabilities we must use simplified geometries enabling detailed measurements and computations
- To solve problems research activities over a range of TRLs is essential

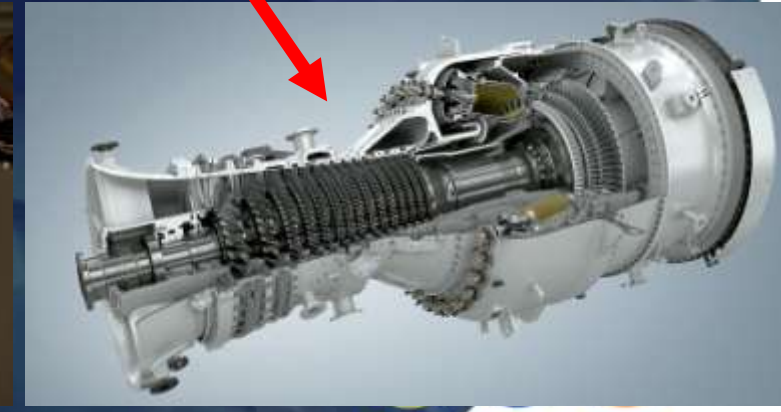
DNS of reheat flame in simplified geometry



Single sector and annular combustor

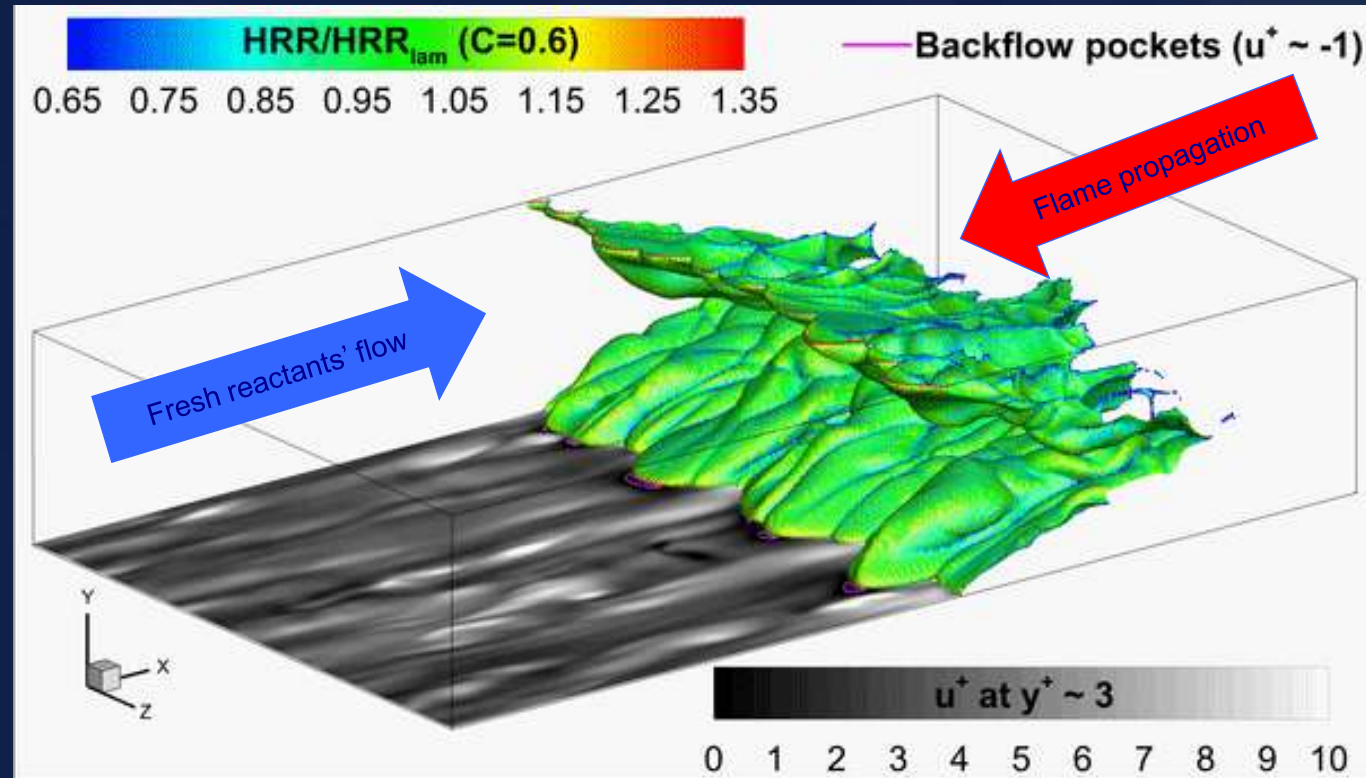
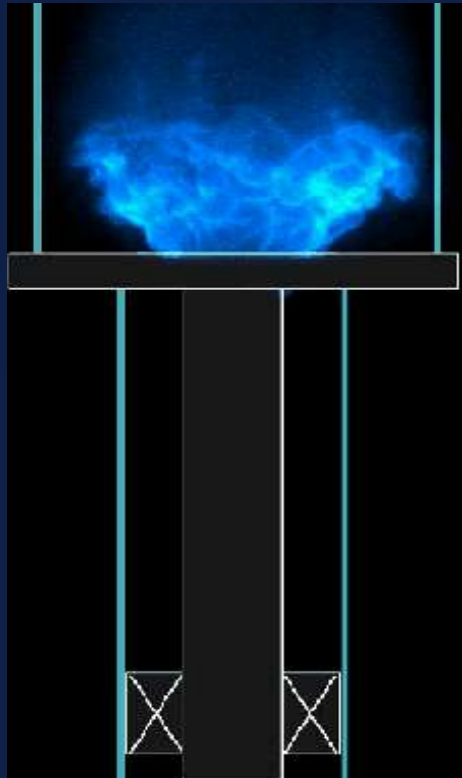


Siemens SGT600/700/800 - Annular combustor



Increasing TRL

Static flame stabilization: avoid flashback!

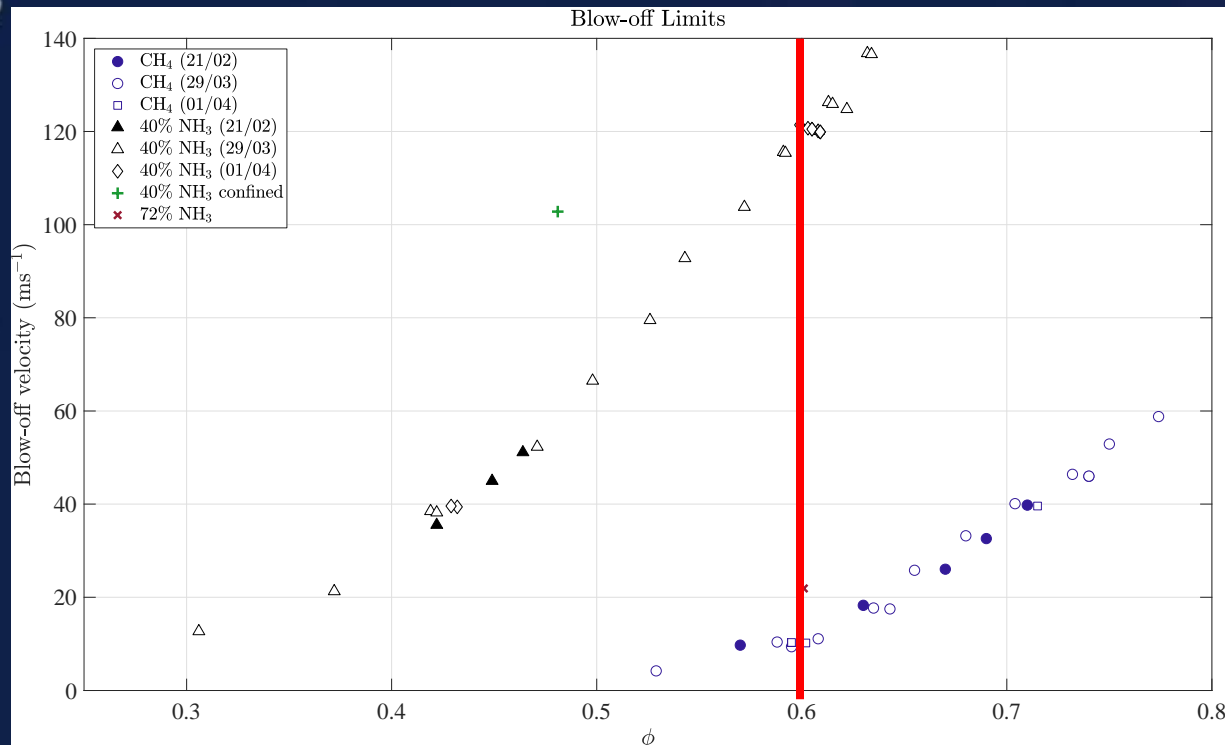


DNS of lean
H₂-air premixed
flame at $\phi=0.55$

- Flashback occurs when the flame propagates much faster than the incoming flow velocity ($S_T \gg U$)
- Always low-velocity regions in wakes and boundary layers



Static flame stabilization: blow-off limits!

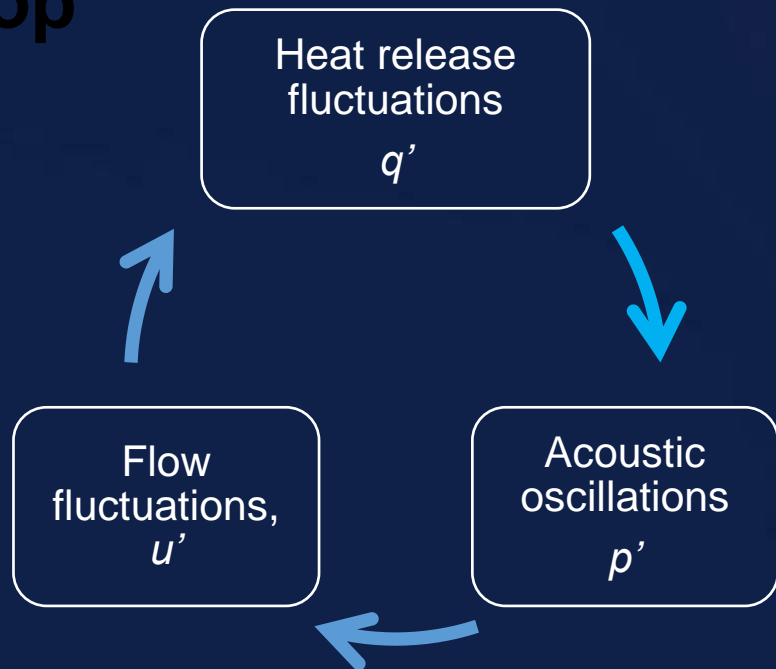


- 40%NH₃/45%H₂/15%N₂ blend matches T_{ad} and S_L for methane but exhibits order-of-magnitude deviation in blow-off limits

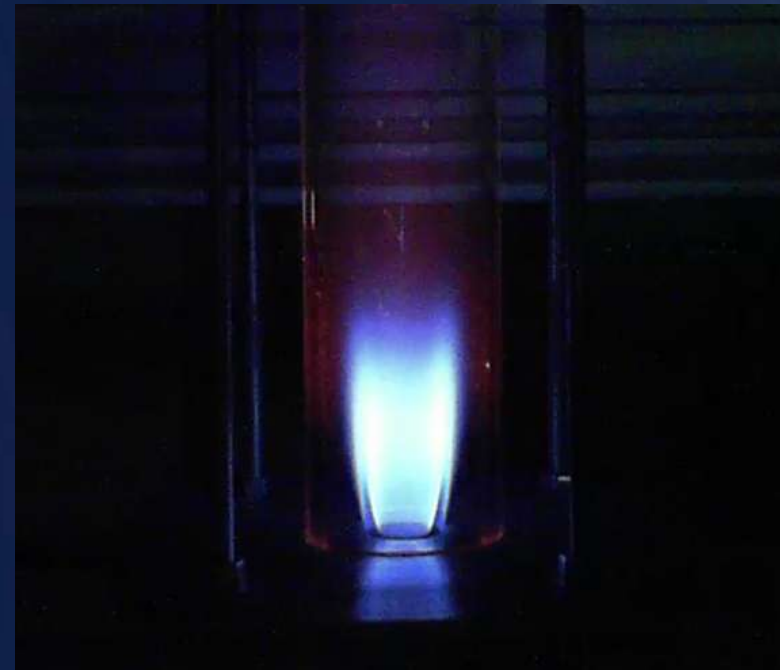


Dynamic instabilities: avoid thermoacoustics!

Thermoacoustic feedback loop



Stable – to violent – to very violent

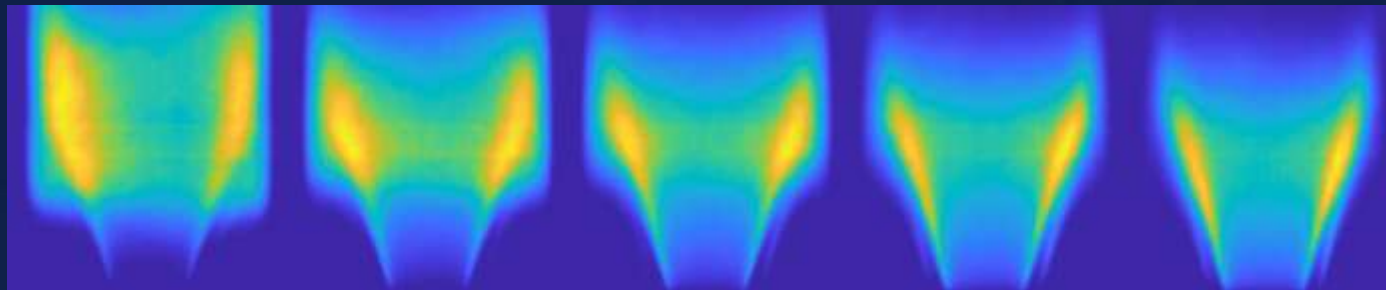


Addition of a small amount of H_2



Effect of increasing H₂ on flame shape

Mean H₂/CH₄ - air flame shapes for increasing H₂



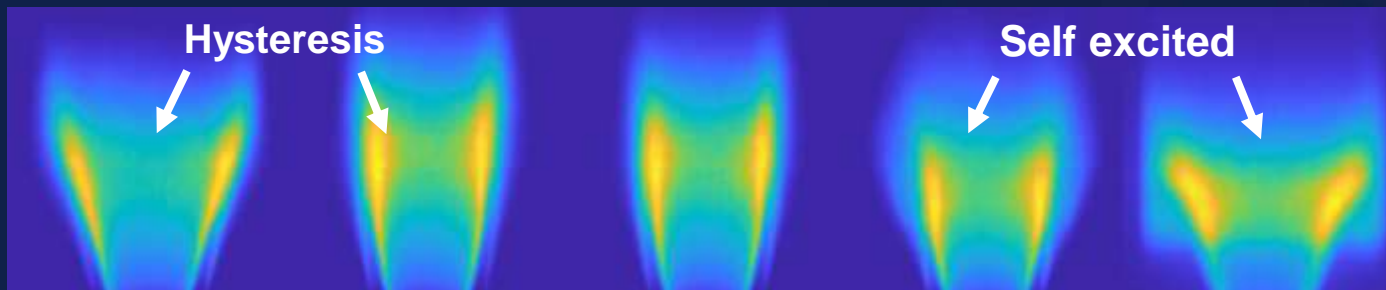
P_{H2} :0%

P_{H2} :5%

P_{H2} :10%

P_{H2} :15%

P_{H2} :20%



Hysteresis

Self excited

P_{H2} :23%

P_{H2} :23%

P_{H2} :25%

P_{H2} :27%

P_{H2} :28%

Conditions:

- Power = 7kW
- Power fraction, P_{H2}: 0-28%
- Volume fraction: 0-50%
- Equivalence ratio = 0.7





Concluding remarks

- Combustion of H₂ fuels are a technically viable route to large-scale decarbonisation for the power generation sector with CCS
- Significant steps forward in co-firing H₂ with CH₄ have been already been made and GTs are commercially available
- There are still significant (and exciting!) scientific and technical challenges in combustion technology to get to zero carbon that need to be addressed

