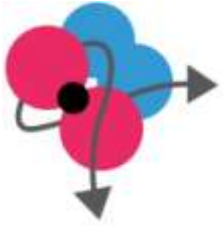


Dynamic simulation of CO₂ injection wells taking the near-well reservoir into account

Svend Tollak Munkejord, Morten Hammer, Åsmund Ervik,
Halvor Lund, Hans L. Skarsvåg, Lars Hov Odsæter

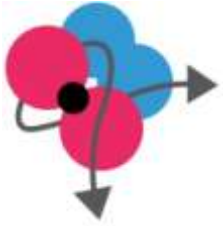
SINTEF Energy Research, Trondheim, Norway

<http://www.elegancy.no/>



Outline of presentation

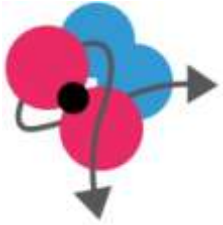
- Motivation
- Models
 - Well flow model
 - Near-well reservoir flow model
 - Thermodynamics
 - Coupling
- Results



Motivation

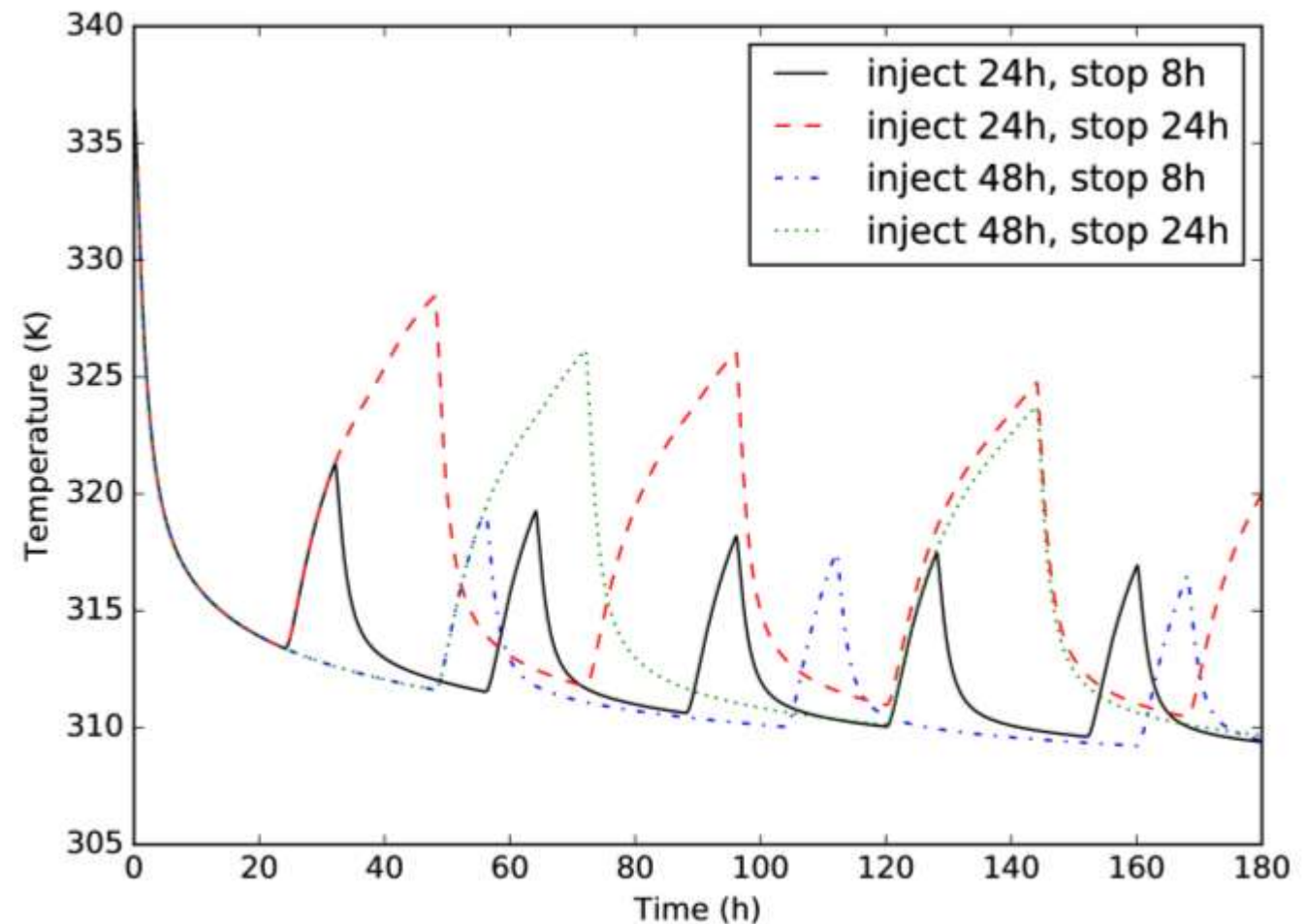
- Injection of CO₂ is different from production of oil and natural gas, and this has implications on operation and design of wells
- Relevant scenarios
 - Intermittent injection (e.g. from ships)
 - Shut-in and start-up
 - Blow-out
 - Possible back-flow of brine into well
 - Thermal cycling and implications of well integrity
- Multiple phases may occur in the well (gas, CO₂-rich liquid, water-rich liquid, solid)
- The well dynamics are influenced by the reservoir dynamics
- We would like to couple a well model with a near-well reservoir model

CO₂ well integrity – thermal cycling

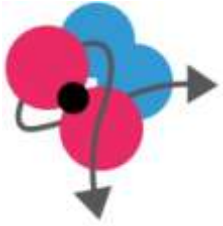


- Intermittent injection of CO₂ gives thermal cycling in the well materials.
- In some cases this may lead to debonding and affect well integrity.
- Worst case: High mass flow, low temperature and long injection and stop intervals

P. Aursand et al., *Int. J. Greenh. Gas Con.* **62** (2017)



Temperature near bottomhole

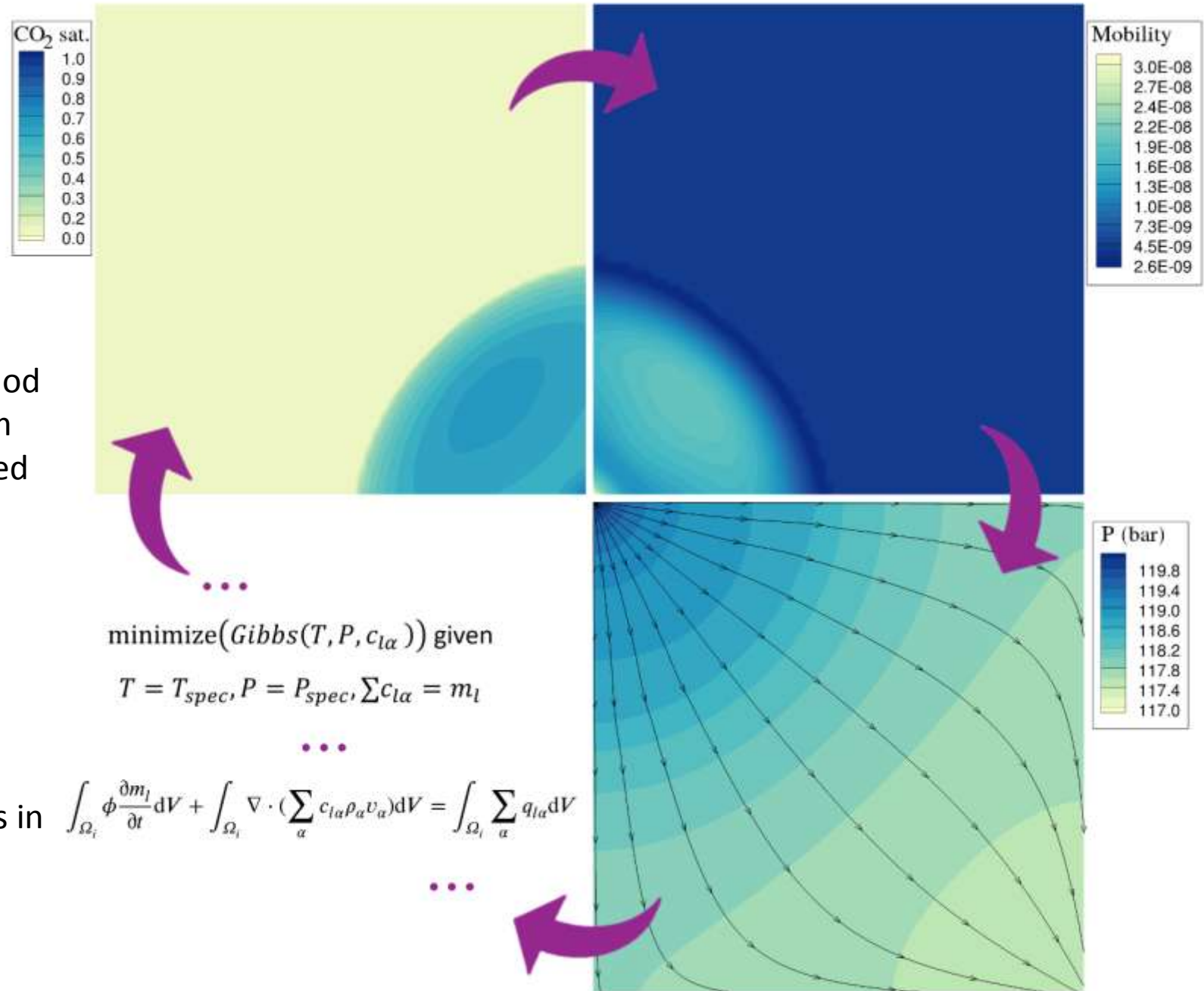


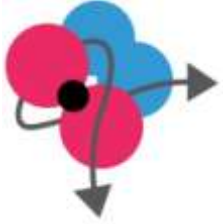
Well model

- Model formulation (drift-flux model)
 - Conservation of mass for each component
 - Momentum balance for the one/two/three phase mixture
 - Total-energy balance for the mixture
 - The phasic velocities are found from an algebraic slip relation
 - Equilibrium in pressure, temperature and chemical potential between the phases
- Flexible choice of equation of state
- Numerical method
 - Fully implicit Jacobian-free Newton-Krylov method
 - Solution using the PETSc library with a Newton-Raphson method as fallback

Reservoir model

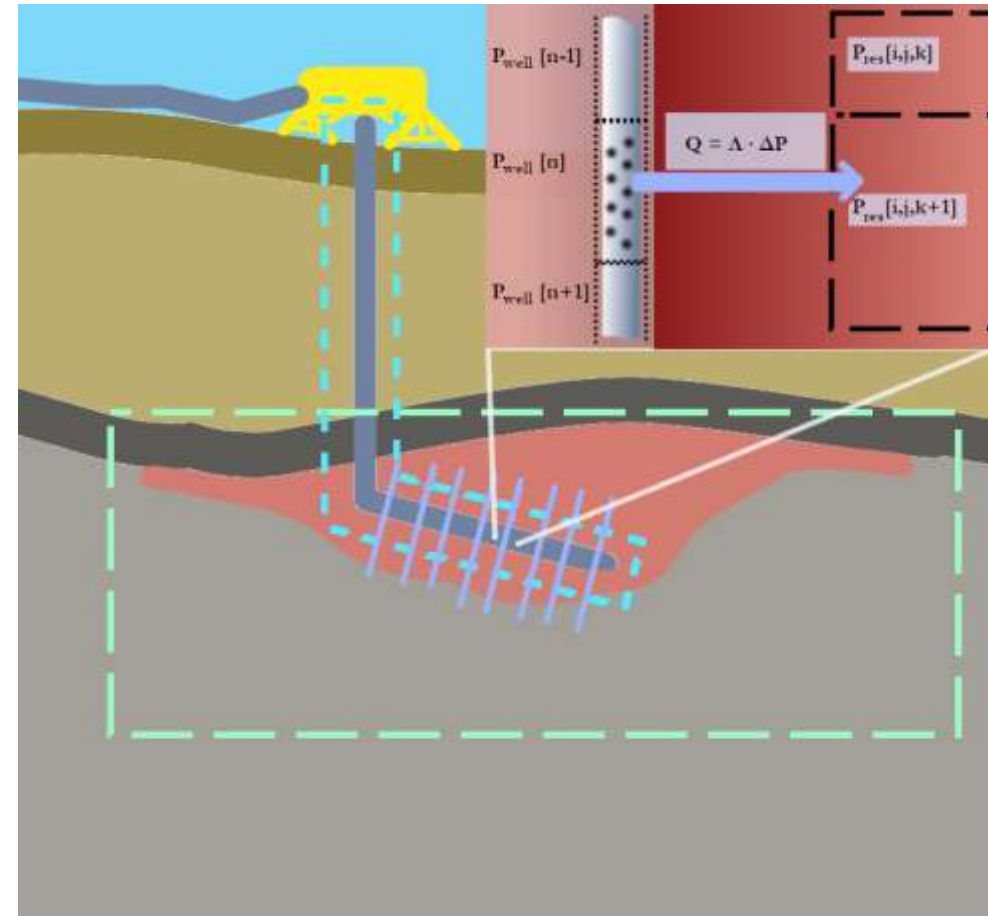
- Purpose-built reservoir simulation code using a variant of the IMPES method
- Pressure is computed from mobility, which is computed from saturations
- Mass is then transported according to the phase velocities (Darcy's law)
- Thermodynamic flash calculation updates saturations, densities, dissolution of components in phases etc.
- Example: 10 m x 10 m domain, 0.78 kg/sec. injection, after 650 sec.

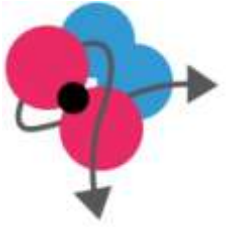




Coupling of well and reservoir model

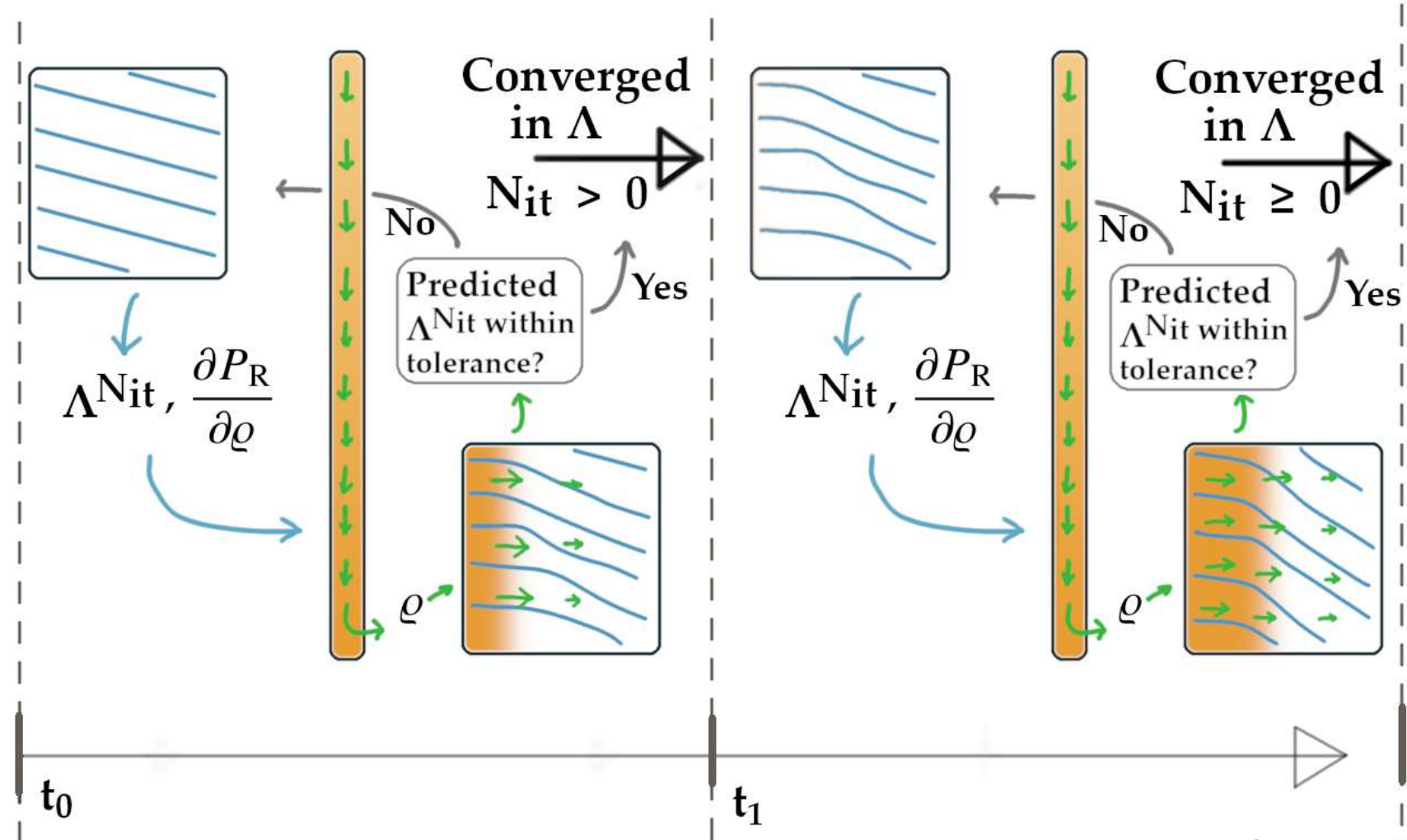
- Well model is 1D (averaged over cross-section)
 - Well can be straight vertical or more complicated
- Reservoir model is 2D/3D
 - Focused on near-well region, assumed homogeneous rock with flow at boundaries
- Coupling is done at one or several locations
 - Partitioned coupling
 - Mass flow out of well proportional to pressure difference between well and reservoir
 - Using relative permeabilities etc. from the reservoir model to compute the well index Λ
 - Mass flow out of well becomes source term in the reservoir model

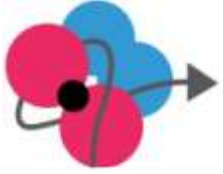




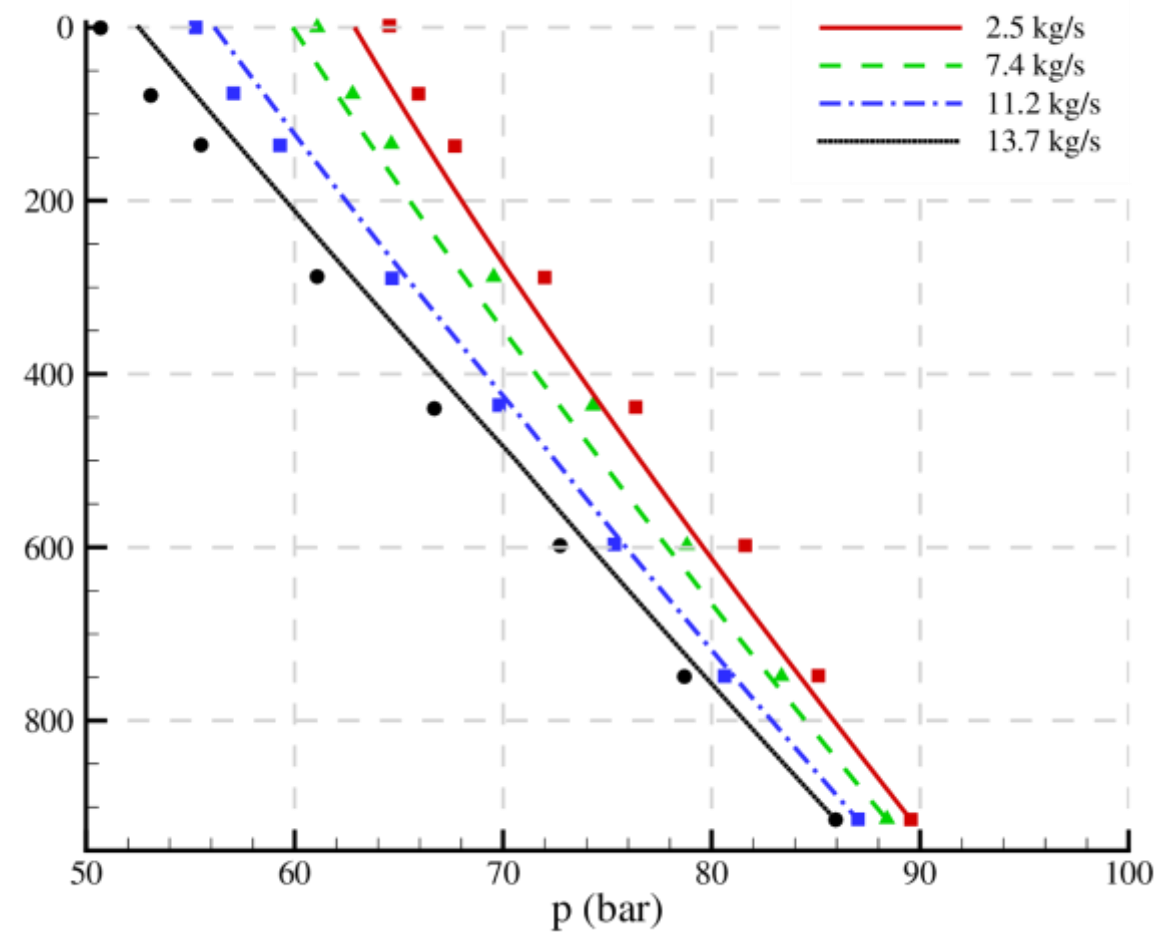
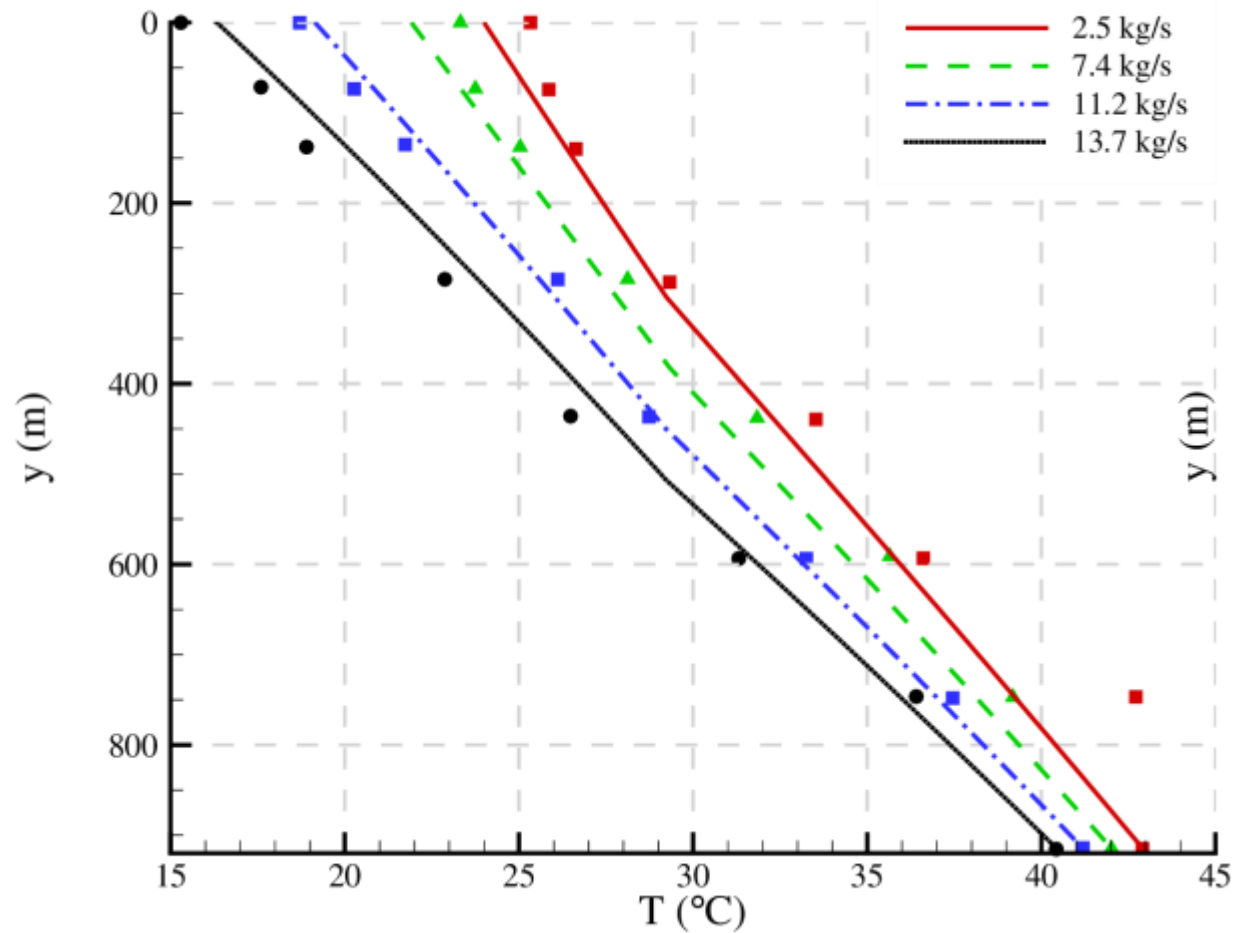
Coupling of well and reservoir model

- Well index (Λ) determines volume flow from well to reservoir
- It depends on saturation, which again depends on volume flow
- Stable coupling requires that the scheme is implicit in Λ
- Thus in situations where Λ changes quickly, we must iterate to obtain correct Λ at the end of the time step





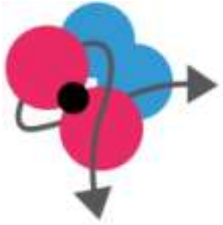
Validation of well model



- Steady flow in a CO₂-production well
- Data from Cronshaw and Bolling (1982)

- Assumptions: Adiabatic flow and pure CO₂
- The case is sensitive to the way boundary conditions are set

Coupled case



Well conditions:

- 1500 m vertical well (ID=0.0883m)
- Initially
 - P = 150 bar at bottom hole
 - Pure CO₂.
 - No flow.
 - Hydrostatic pressure profile in pipe
- Start simulation by ramping linearly from 0 to 25kg/s in 60s at the well head
- Enthalpy specified at inlet, to give approximately 300K

Reservoir conditions:

- P = 150 bar initial and boundary condition, outflow from near-well reservoir domain (30m height x 40m radius, cylindrically symmetric)
- T = 310 K isothermal
- Permability 3.0 Darcy, porosity 0.3 for 'Case A'
- Permability 0.3 Darcy, porosity 0.15 for 'Case B'
- Consider three situations for each case:
 - Neglect gravity
 - Include gravity
 - Spatially varying rock permeability (log-normal distribution)

Coupled case

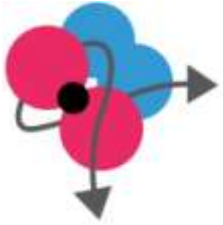
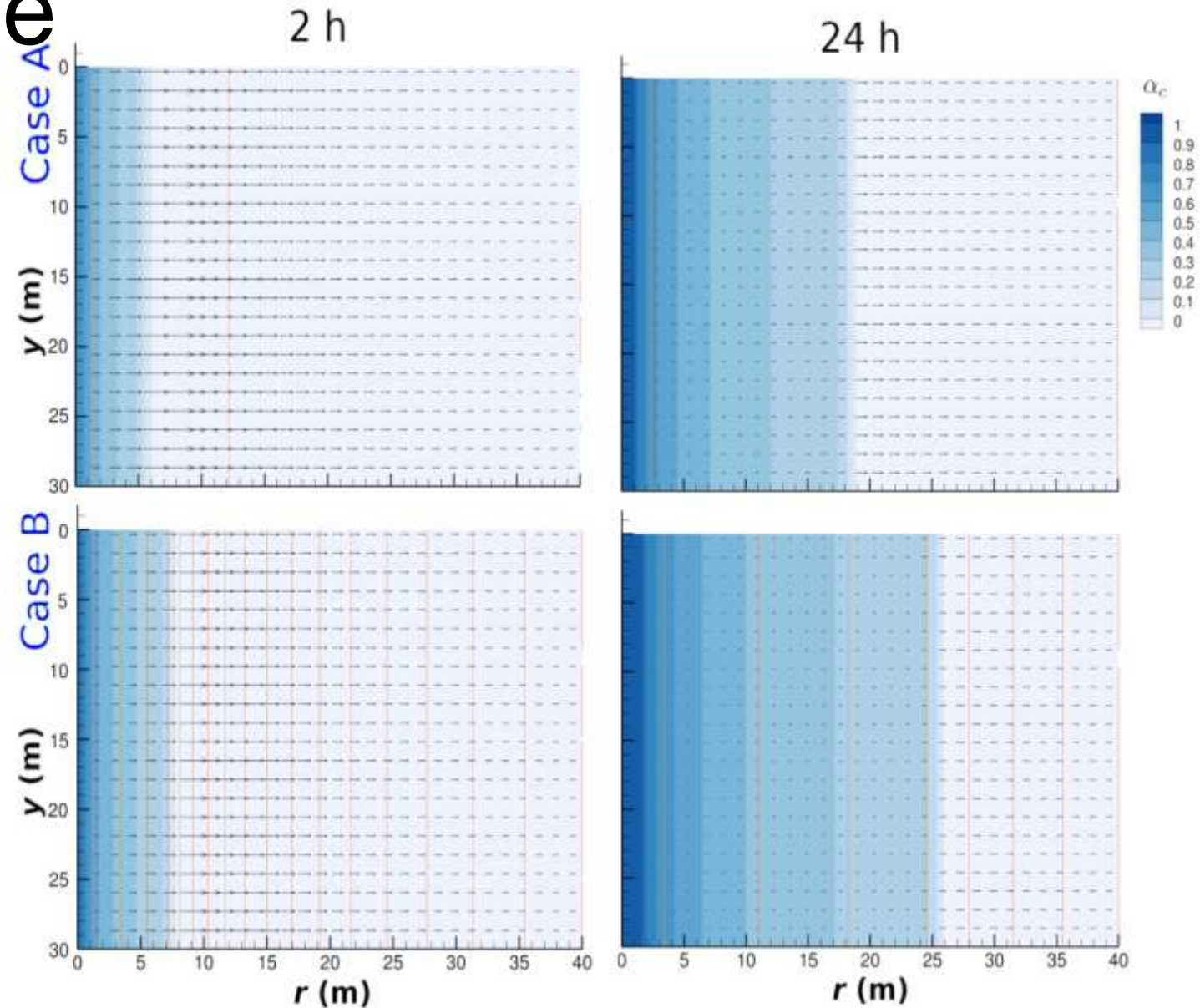
Neglecting gravity

CO₂ volume fraction in blue

Pressure contours in orange

Water flow as vectors

For Case B with lower porosity, front advances further.



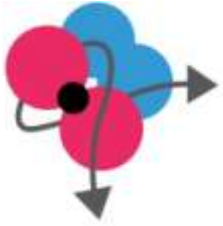
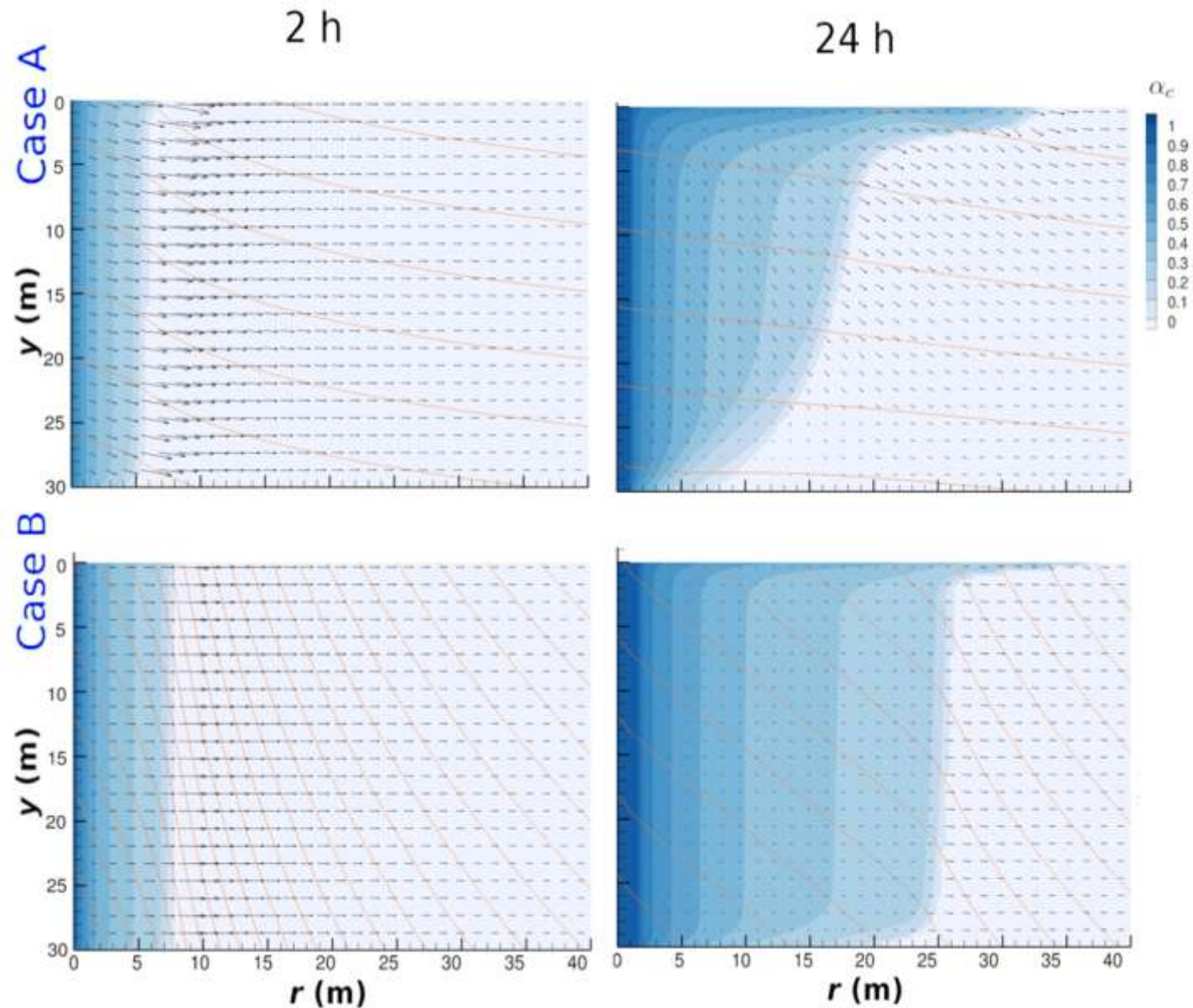
Coupled cas

Including gravity

CO₂ volume fraction in blue
Pressure contours in orange
Water flow as vectors

For Case A with higher permeability, gravity has bigger effect.

For this reason, leading CO₂ edge catches up to Case B



Coupled case

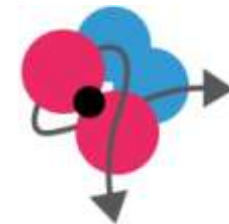
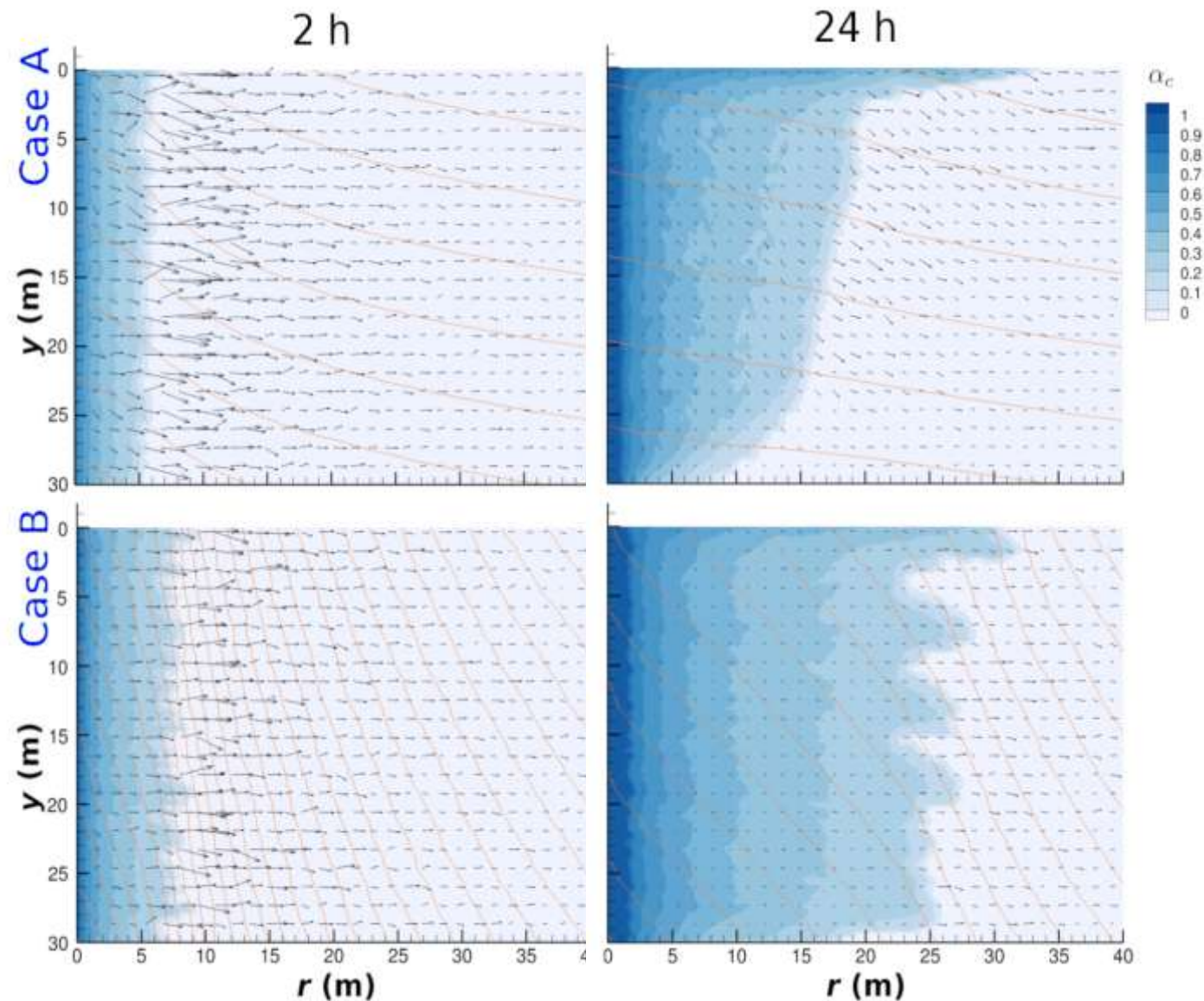
With varying permeability

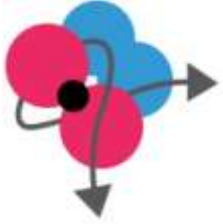
CO₂ volume fraction in blue

Pressure contours in orange

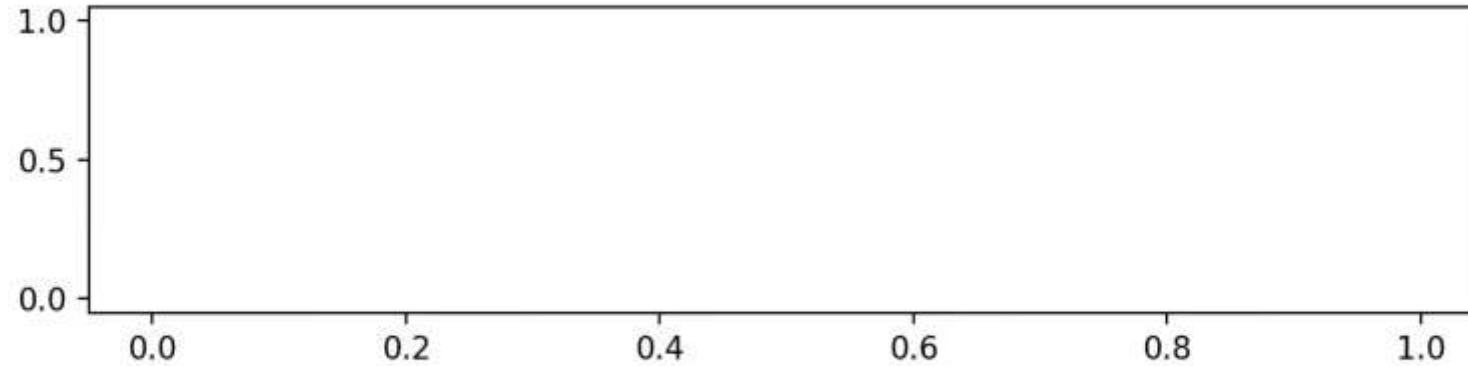
Water flow as vectors

For Case A, overall trend is unchanged. For Case B, viscous fingering is observed.

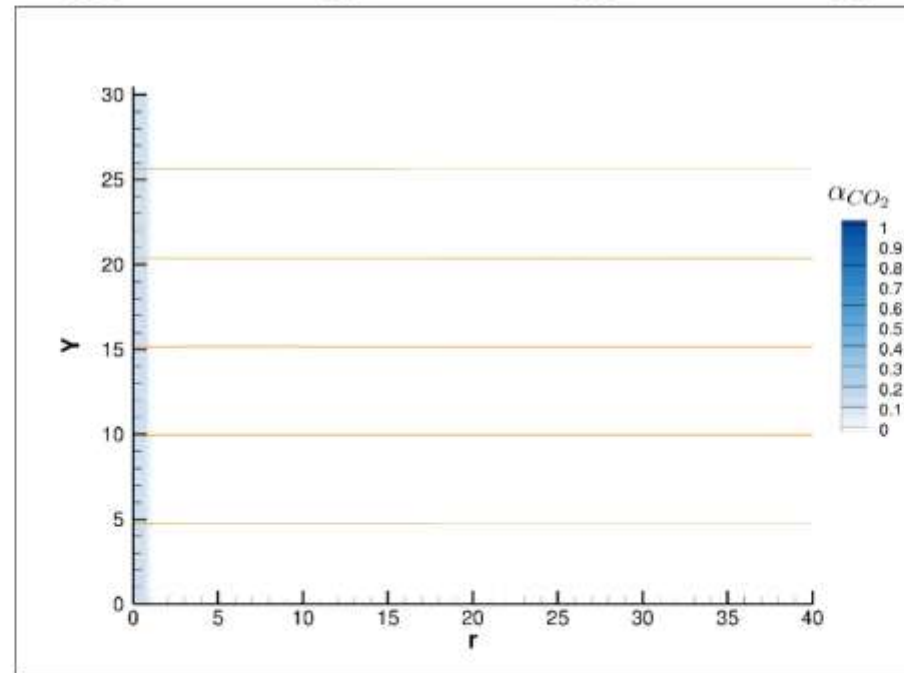




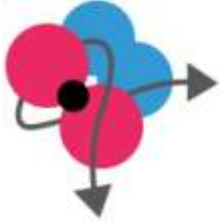
Coupled case



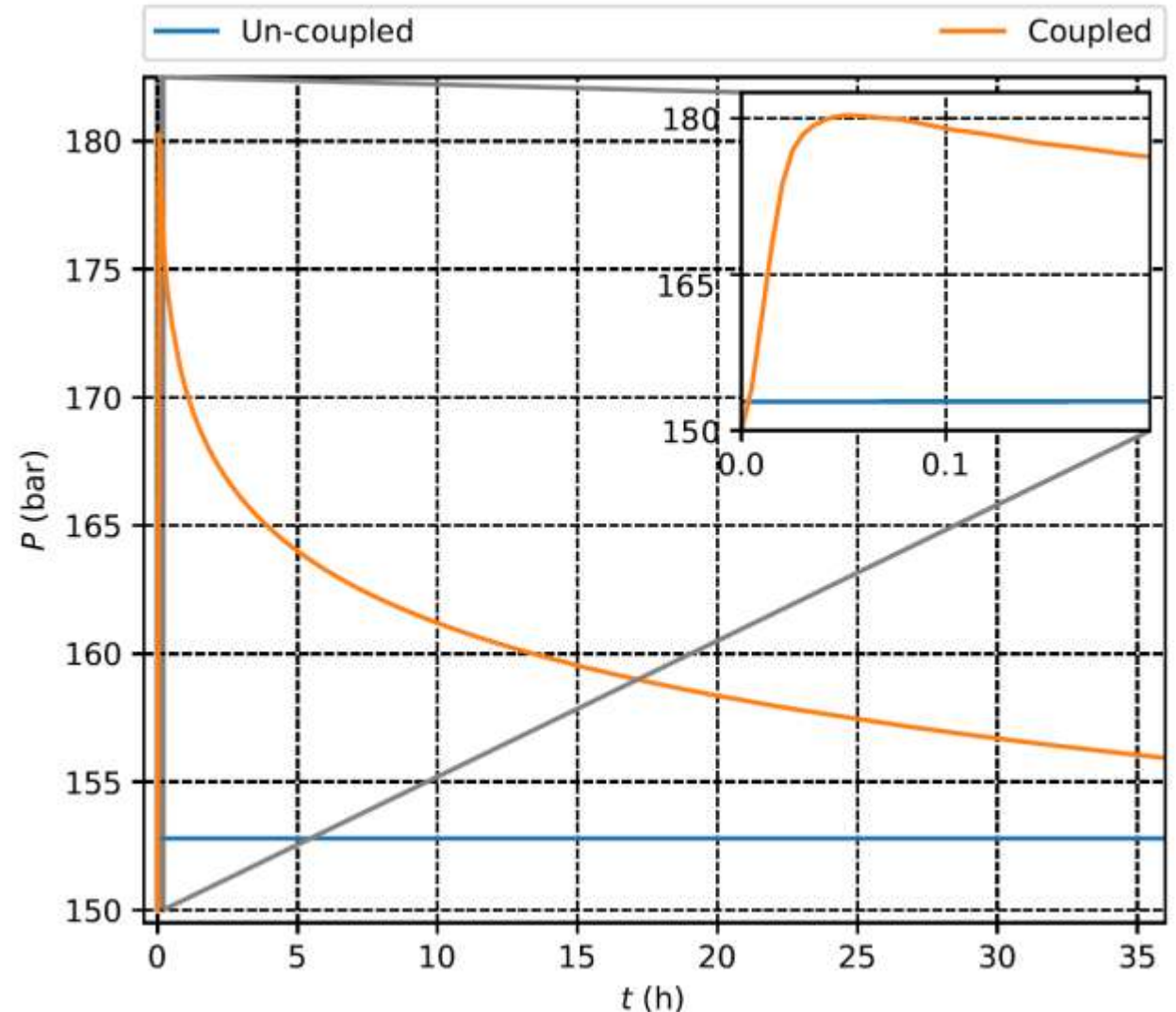
- "Case B" with gravity and varying permeability
- Top: pressure in well at the coupling point
- Bottom: CO₂ volume fraction (blue) and pressure (orange lines) in the reservoir

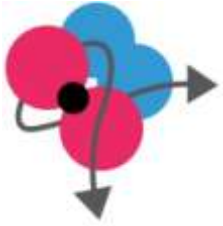


Coupled vs. uncoupled case B



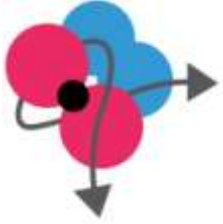
- Uncoupled well case identical to coupled case, except the reservoir in-flow model:
 - $Q = \Lambda \frac{\rho}{\mu} \left(P_w - \left[P_R^0 + \frac{dP_R}{dQ} Q \right] \right)$
 - For illustration, the reservoir pressure is set to match $P_{far} + (P_{max} - P_{far}) \frac{\mu_{CO_2}}{\mu_{water}}$
- Plot shows bottom hole pressure. Zoom of first 0.2h.





Conclusion

- Coupled model with three building blocks:
 - Well model
 - Near-well reservoir model
 - Thermodynamics
 - Partitioned coupling means these can be developed independently
- Full thermodynamic model is employed in the reservoir under the assumption of constant temperature
 - Future work to implement an energy transport equation in the reservoir, and possibly to take fluid compressibility into account
- Results indicate the versatility of the model
 - Results emphasize the need for a near-well model to describe the reservoir pressure response from an injection well.
 - The specific nature of the reservoir needs to be modelled, in particular for tighter formations, and the effect of buoyancy as well as heterogeneities may be important.



Acknowledgement

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