

# PIPERAZINE (PZ) AND METHYLDIETHANOLAMINE (MDEA) INTERRELATIONSHIPS IN CO<sub>2</sub> ABSORPTION BY AQUEOUS AMINE MIXTURES

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# Summary

- The use of ***a*-MDEA (MDEA + PZ)** as industrial solvent in CO<sub>2</sub> capture process is highlighted
- Very little however is known on the actual behaviour of the absorbent mixture
- Experiments were carried out to throw some light on the problem
- Main results show that interaction between PZ and MDEA is quite limited (e.g. no shuttle effect)

# a-MDEA as absorbent medium

22/5/2019

Amines washing machine - BASF Intermediates

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## Amines washing machine BASF's process makes gas treatment history

From the pilot plant to leading supplier status for natural gas treatment: success stories like BASF's aMDEA® technology are few and far between.

It all started with ammonia. BASF wanted to reduce the cost of producing ammonia. In the early 1970s, BASF was therefore exploring methods for separating carbon dioxide (CO<sub>2</sub>) more efficiently from the synthetic gas used in the production process.



This is one of the places where aMDEA is used: production of natural gas on Melkoya island off the coast of Norway.

BASF's researchers succeeded: they invented a process relying on methyldiethanolamine (MDEA) as a "gas-scrubbing agent" to which a special activator lends exceptional reactivity. This "activated methyldiethanolamine" - aMDEA, for short - combines more easily with CO<sub>2</sub>, separating it more efficiently from the syngas than the traditional monoethanolamine or potassium carbonate. The process requires clearly less energy input and achieves much higher plant capacity.

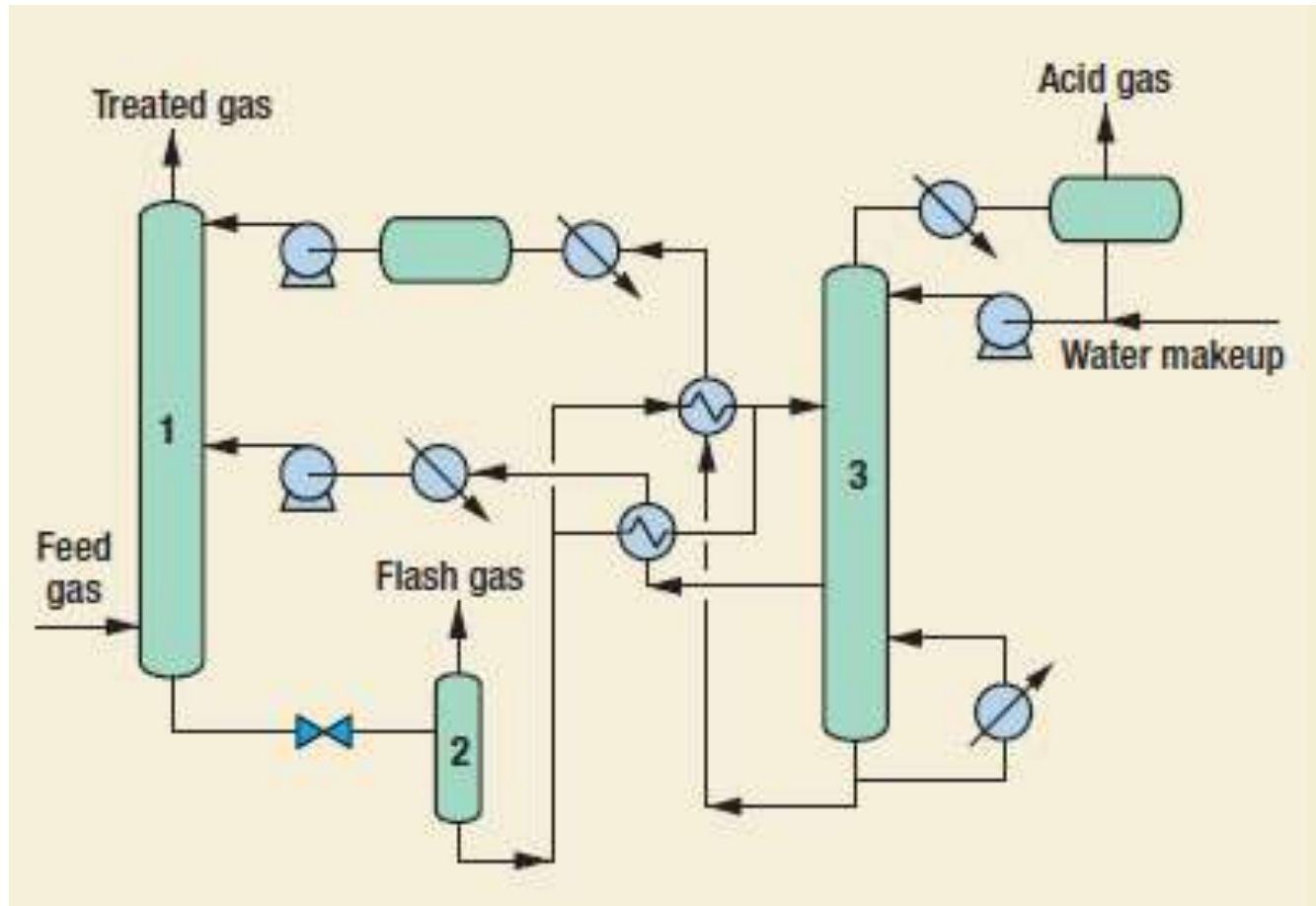
BASF originally used the process in its own ammonia and syngas plants only but then started licensing it to other ammonia manufacturers. The idea of selling the aMDEA technology to oil and gas companies occurred to some clever BASF employees in the early 1990s. After all, gases like liquefied natural gas (LNG) also need to be scrubbed, i.e., freed of any impurities like CO<sub>2</sub> or hydrogen sulfide. Potential customers were reluctant, however. Never before had the aMDEA process been used in an LNG facility. There was simply no plant that could serve as a reference.

Breakthrough was achieved in 1997 on the Indonesian island of Borneo, two hours by car north of the equator. Here, right in the jungle of Kalimantan, was the location of what was then the world's largest LNG facility. And national operator Pertamina had been convinced to try out aMDEA in one of its seven production lines. The trial was an overwhelming success, the new process proved to be highly efficient.

News

BASF to increase capacity for Alkylethanolamines in Ludwigshafen  
April 10, 2010  
[Read more...](#)

# $\alpha$ -MDEA PROCESS



# advantages lauded...

**Table 2**  
**ECONOMIC COMPARISON OF RYAN HOLMES AND BASF aMDEA PROCESSES**

	<b>RYAN-HOLMES</b>	<b>BASF aMDEA</b>
<b>CAPITAL COST</b>		
Acid Gas Removal	233% Base	Base
CO <sub>2</sub> LP Compression	60% Base	Base
CO <sub>2</sub> Dehydration	Not Required	Base
Feed Gas Dehydration	78% Base	Base
<b>Total</b>	<b>154% Base</b>	<b>Base</b>
<b>OPERATING COST</b>		
Power	87% Base	Base
Fuel Gas	117% Base	Base
<b>Total</b>	<b>106% Base</b>	<b>Base</b>



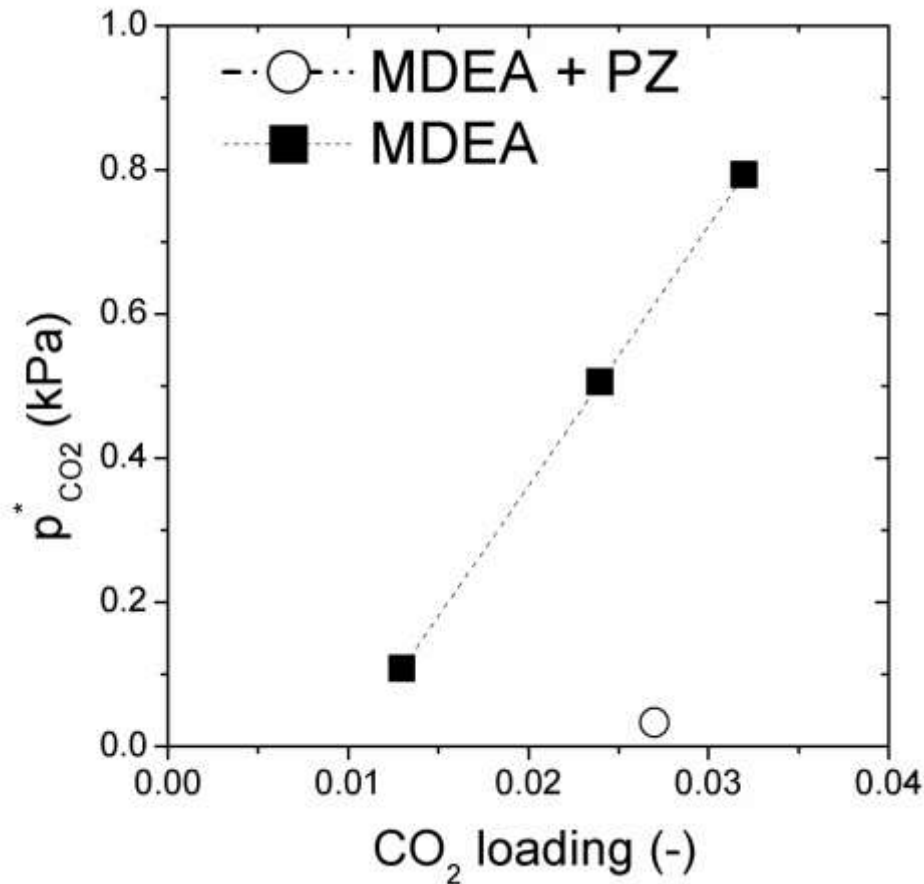
# more advantages lauded...

**Table 2 Effect of Piperazine on Treating**

Wt% Piperazine	Treat (ppm CO <sub>2</sub> )	Lean Load (mol/mol)	% Rich Equilib'm	Reflux Ratio
0 (22 trays)	85,300	0.0015	70	2.2
0 (50 trays)	48,300	0.0015	83	2.0
0 (100 trays)	48,000	0.0015	83	2.0
5 (22 trays)	51	0.016	91	1.2
7 (22 trays)	39	0.021	89	1.1
9 (22 trays)	10	0.026	87	1.0

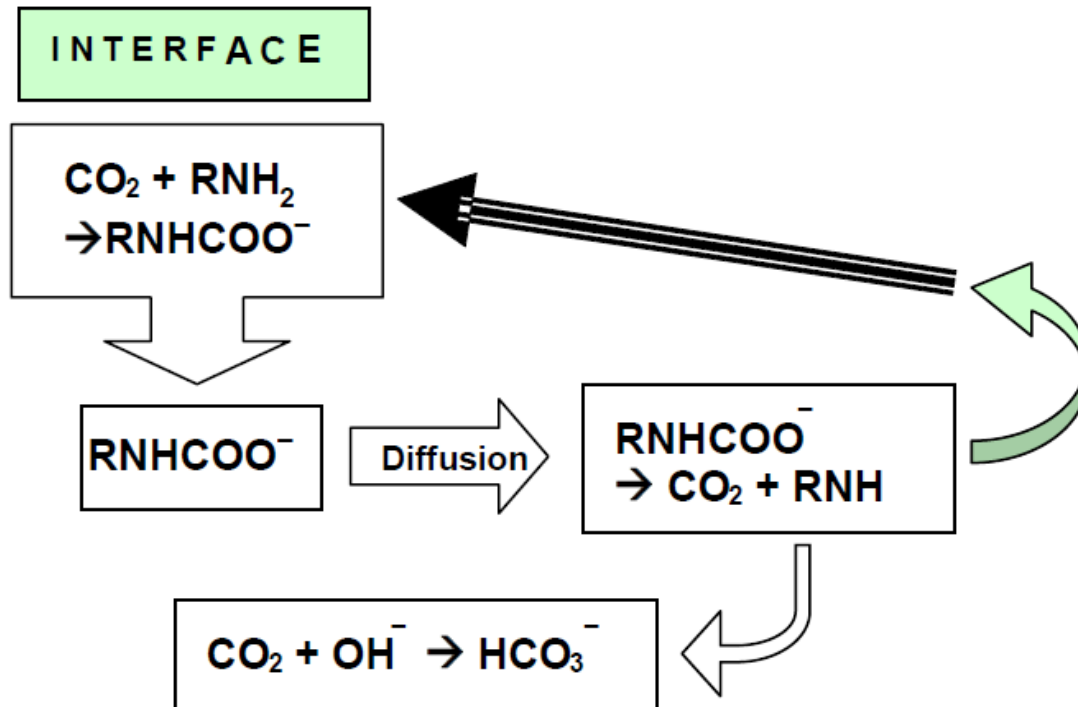
The effect of piperazine on CO<sub>2</sub> treat is nothing short of stupendous—it allows promoted MDEA to reach a few tens of ppmv while MDEA alone cannot do better than 8.5% in the same equipment, and it cannot reach below 4.8 mol% CO<sub>2</sub> even with 100 trays in the column under otherwise identical conditions.

# gas-liquid CO<sub>2</sub> equilibrium



*data taken from  
Bishnoi (2000)*

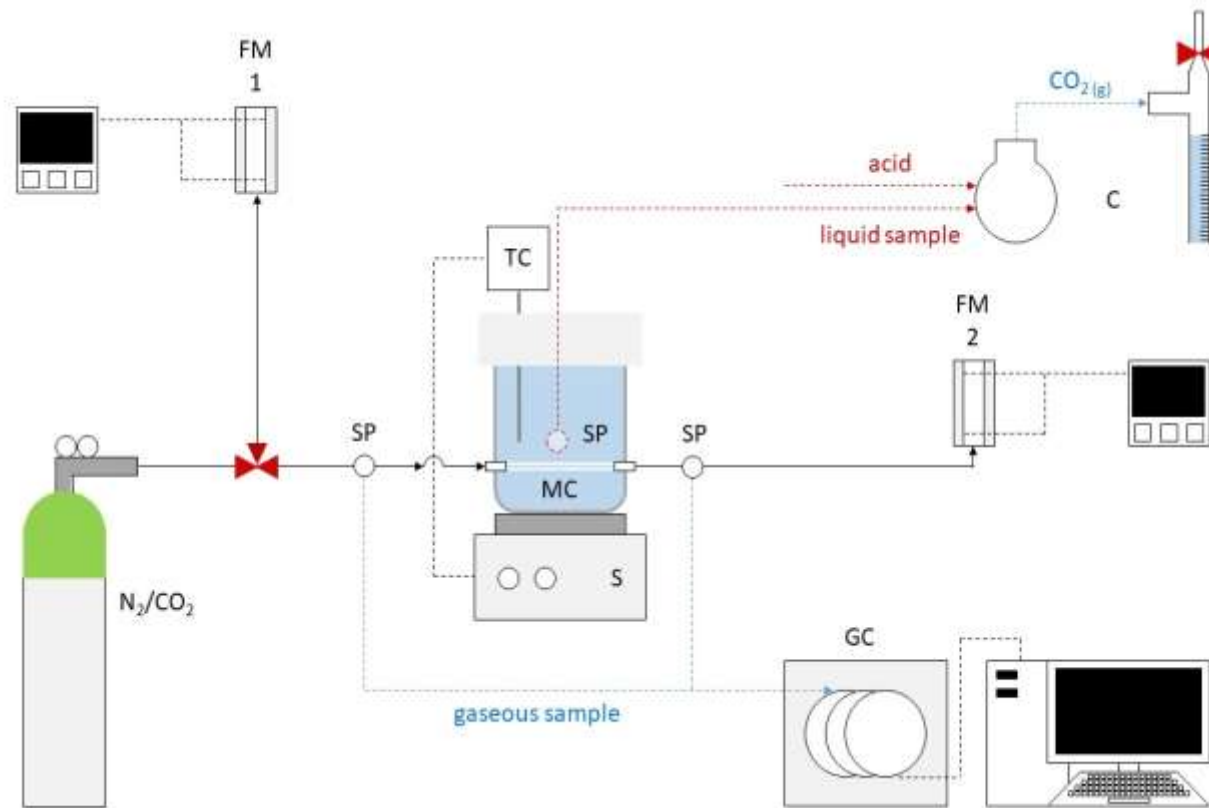
# not quite clear how it works!



**Figure 1** Schematic of Shuttle Mechanism



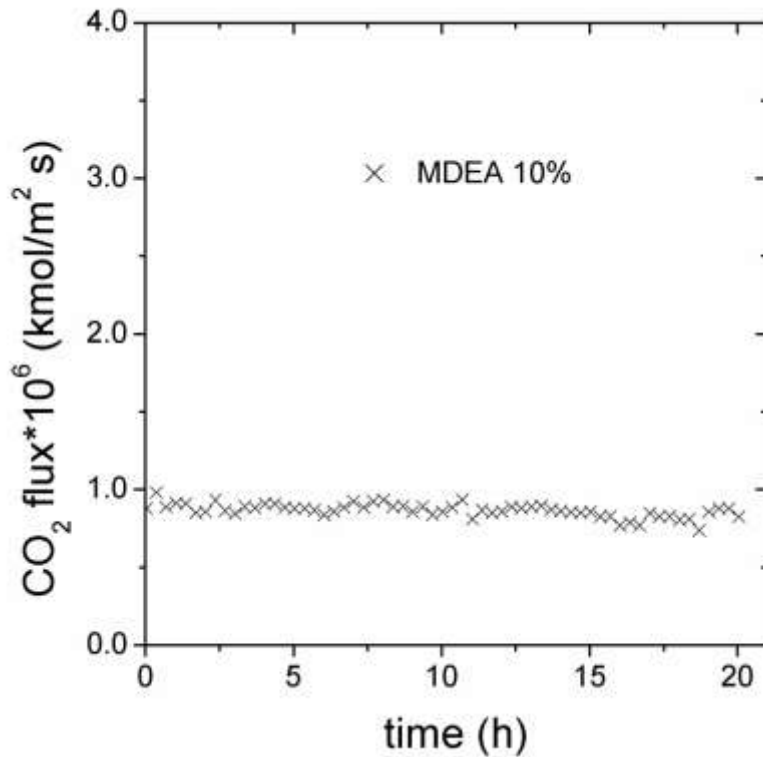
# experimental investigation



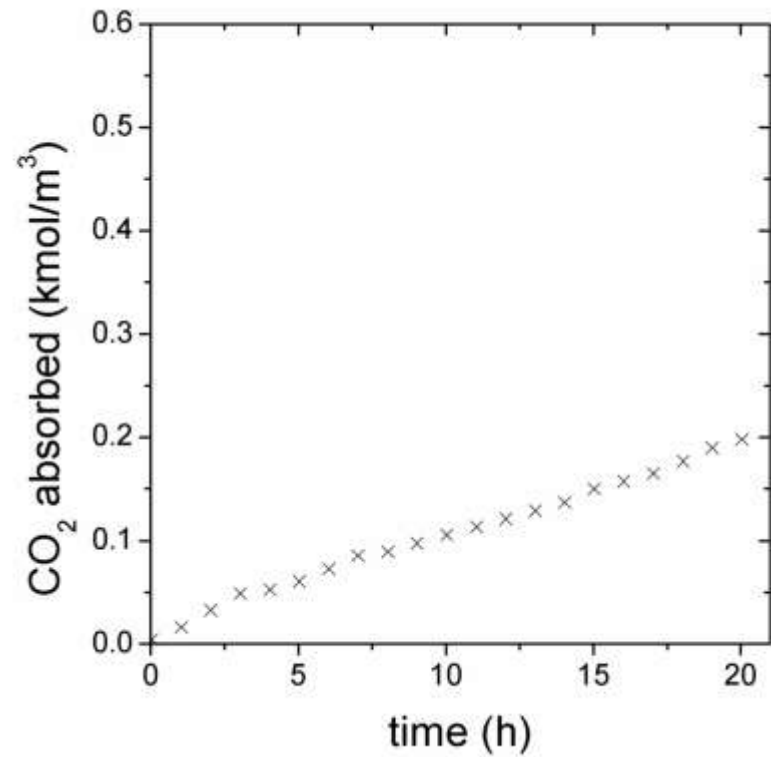
FM: flow meter; SP: sampling point; TC: temperature controller; MC: membrane contactor; S: magnetic stirrer; GC: gas chromatograph; C: calcimeter

# MDEA 10% (0.84 M)

gas side

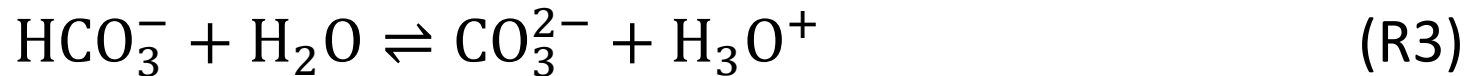
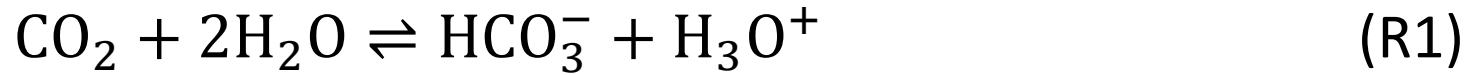


liquid side

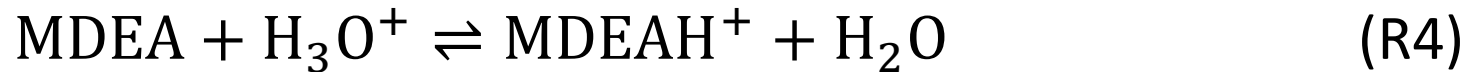


*(practically no enhancement on the process rate compared to pure water)*

# MDEA + CO<sub>2</sub> (*chemistry*)

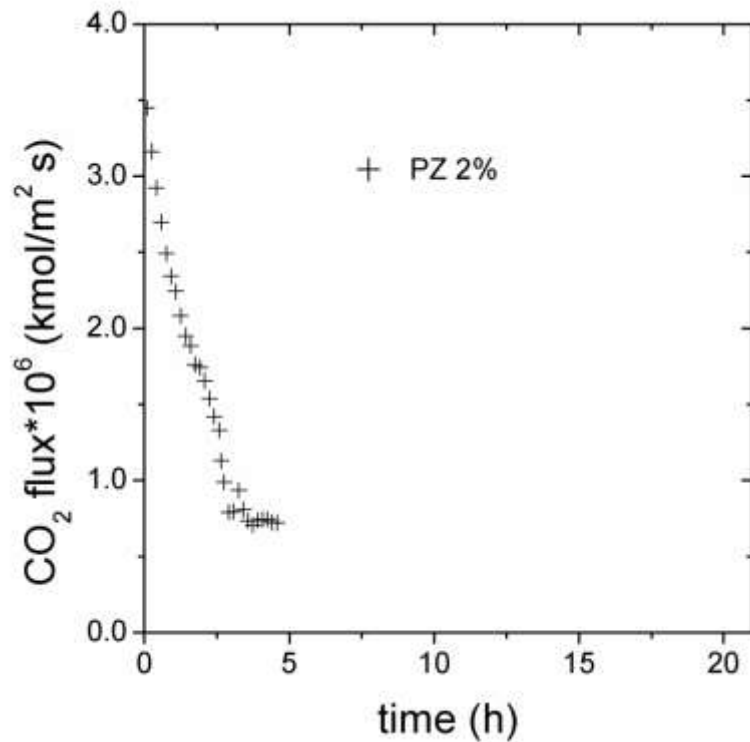


*Protonation:*

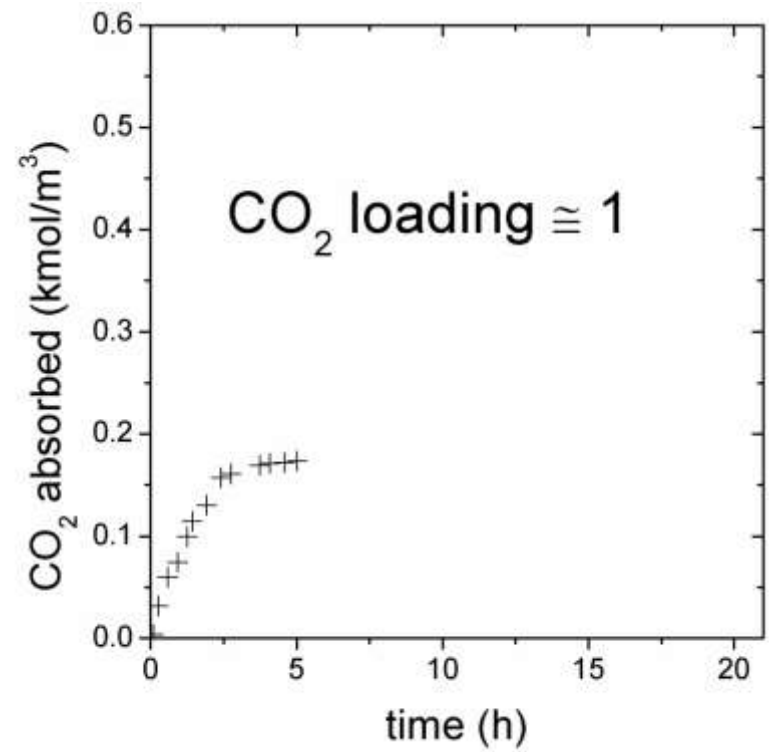


# PZ 2% (0.23 M)

gas side

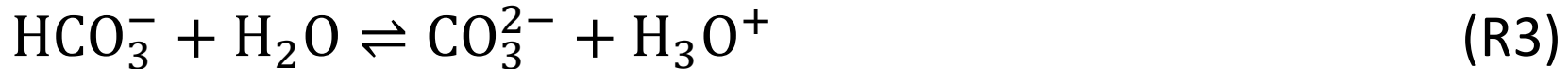
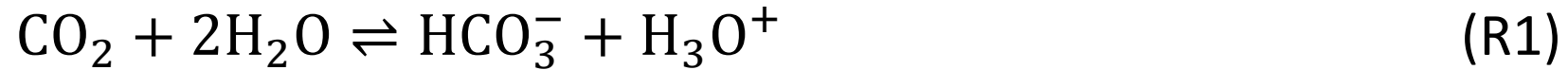


liquid side



*(the enhancement on the process rate evident for about 3 h)*

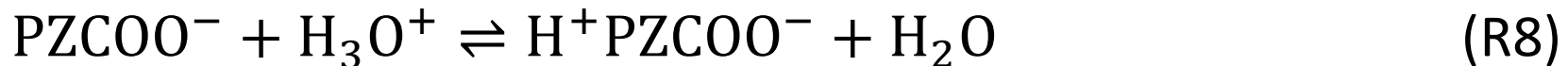
# PZ + CO<sub>2</sub> (Chemistry)



*Carbamate and dicarbamate formation:*

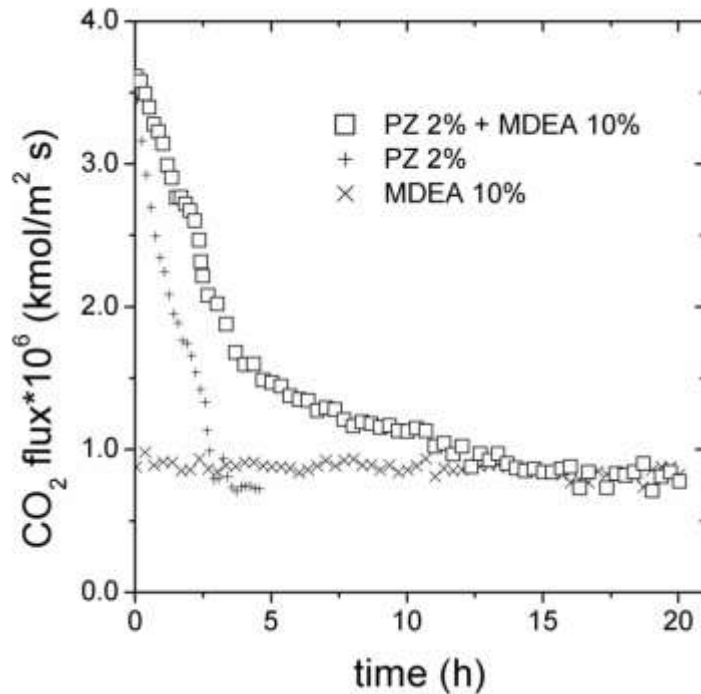


*Protonations:*

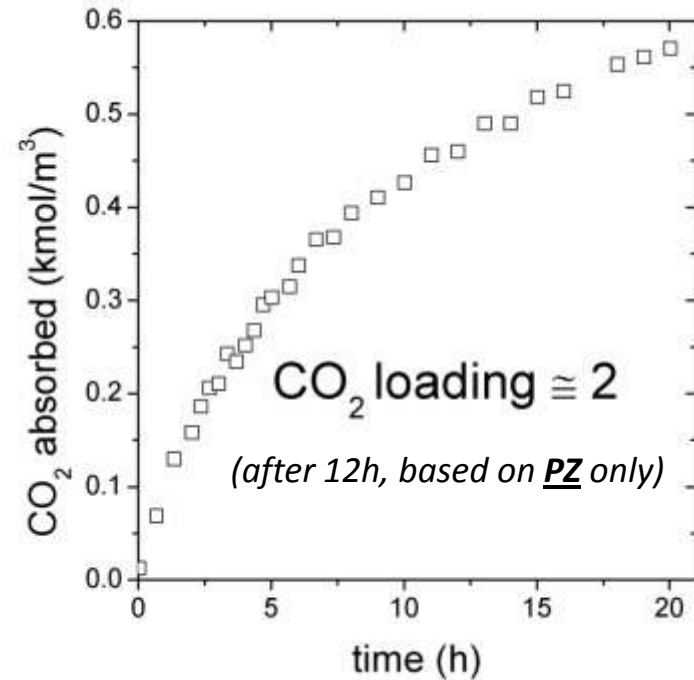


# 10% MDEA + 2% PZ

gas side

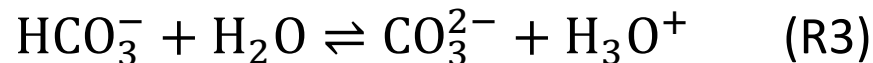
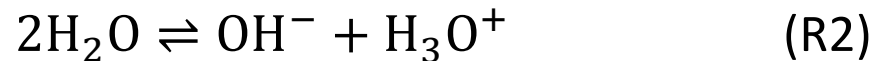


liquid side

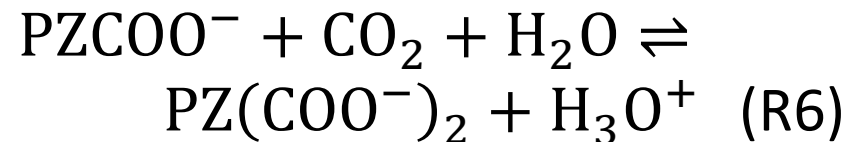


*(the enhancement on the process rate evident for about 12 h)*

# MDEA + PZ + CO<sub>2</sub> CHEMISTRY



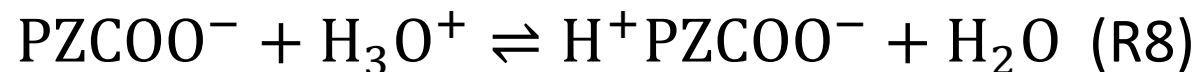
*Carbamate and bicarbamate formation:*



*Protonation:*



*Protonations:*



# which protonation will prevail?

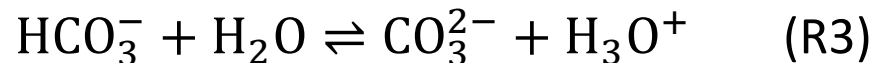
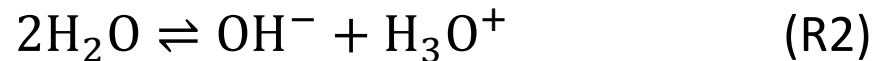
*protonation reactions are the only step where the two absorbents may interfere*

$$f_{MDEA} = \frac{\frac{K_{eq,4} C_{MDEA}}{K_{eq,7} C_{PZ}}}{1 + \frac{K_{eq,4} C_{MDEA}}{K_{eq,7} C_{PZ}}}$$

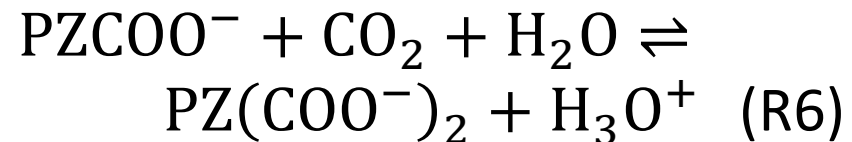
R4 will prevail over R7 with the result of freeing PZ, which become available for more CO<sub>2</sub> absorption



# SIMPLIFIED MDEA + PZ + CO<sub>2</sub> CHEMISTRY



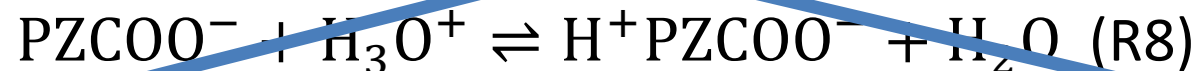
*Carbamate and dicarbamate formation:*



*Protonation:*



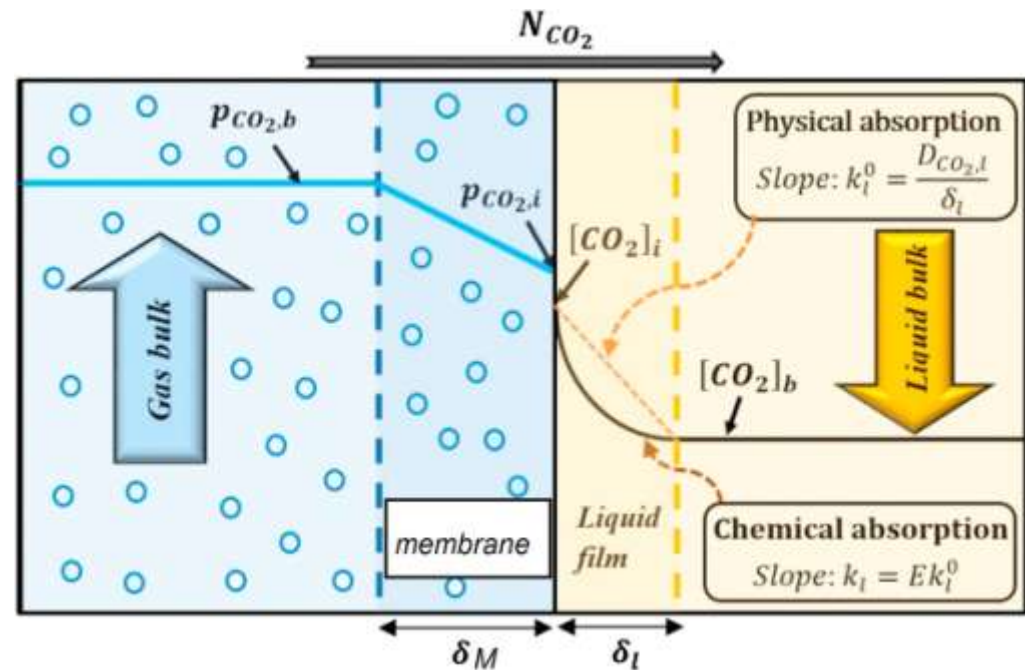
*Protonations:*



# bit of modelling...

*we use the classical  
film theory*

$$J_{CO_2} = \frac{p_{CO_2}}{\frac{1}{k_M} + \frac{H}{Ek_L}}$$



# bit of modelling...

## *in order to estimate E*

$$D_j \frac{\partial^2 C_j}{\partial x^2} + \sum_i r_{ij} = 0$$

(with the pseudo-steady-state-hypothesis a reasonable assumption)

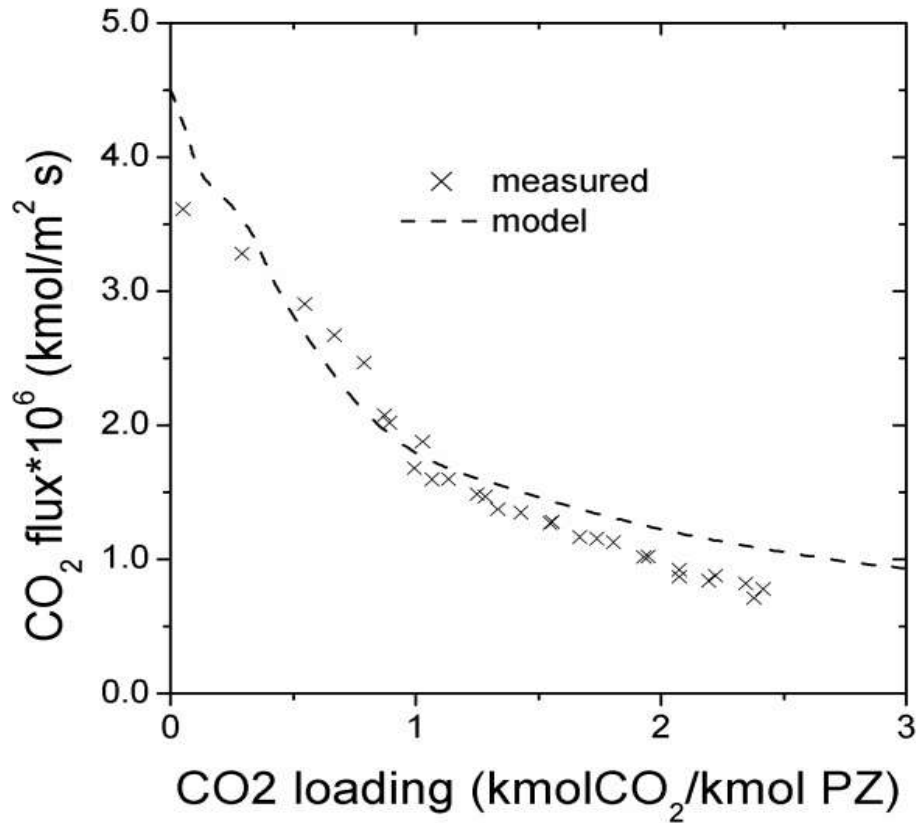
At  $x=0$  (membrane-liquid interface)

$\frac{\partial C_j}{\partial x} = 0$  for every component  $j$  excluding  $\text{CO}_2$  for which

$$C_{\text{CO}_2} = \frac{p_{\text{CO}_2, M}}{H}$$

At  $x=\delta$  (liquid film-liquid bulk interface)  $C_j = C_{j, b}$  valid for any components.

# bit of modelling...



*(all necessary data from literature, no fitting parameters)*

# CONCLUSIONS

- Observed behavior of the MDEA+PZ absorbing mixtures can be explained without the need to introduce «exotic» steps
- «Shuttle» mechanism can also be discarded
- Rather than  $\alpha$ -MDEA, MDEA+PZ mixtures should be named  $e$ -PZ

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