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Post Combustion CO₂ Capture via Chemical Absorption with Amino Acid Salts Solutions

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INTRODUCTION

Background

- The present work has been carried out in the framework of a collaboration between LEAP (Laboratory of Energy and Environment Piacenza)-Politecnico di Milano and Sotacarbo Research Center
- The activity is partially funded by the Regional Government of Sardinia (FSC 2014-2020) within the “Centre of Excellence on Clean Energy” project (CUP D83C17000370002)

Objective

- Research project on alternative solvents for chemical absorption applied to CO₂ for post-combustion capture applications
- Alternative solvents to be investigated → Amino Acids (green solvents)
- CCS technology applied to Natural Gas Combined Cycle (NGCC) flue-gas
- Reference solvent → 5M MEA solution (30% w/w as from EBTF-CAESAR Project)

INTRODUCTION

Benefits of Amino Acid Salts and their Potential Impact (Literature Information)

↑ CO₂ Loading
and Absorption
Rate

↑ Cyclic
Capacity

↓ Thermal
Oxidative
Degradation

↓ Corrosion

↓ Volatility,
↑ Environmental
Compatibility

Less circulating
solute

Lower circulation
rate

Higher solvent life

Longer equipment
and accessory life

Lower vapour losses

Lower equipment
size (absorber)

Lower energy
required (e.g.: pumps)

Reduced make-up and
operating costs

Lower equipment
cost

Lower solvent
make-up

Lower CAPEX

Cost reduction
(CAPEX and OPEX)

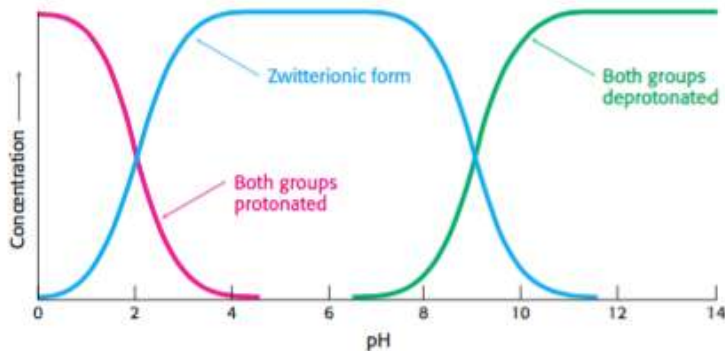
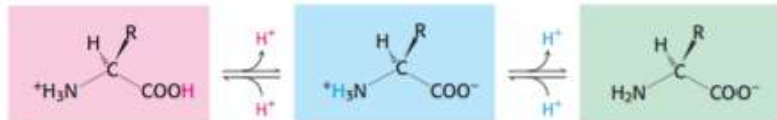
Enhanced capacity -
solvent precipitation
(at high loadings)

Reduced health and
environmental effects

To be verified

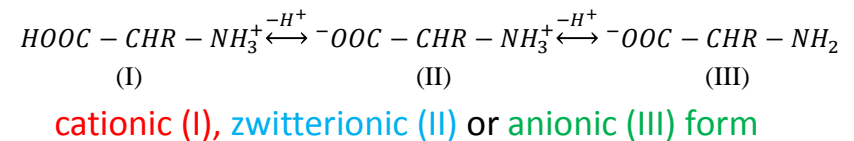
INTRODUCTION

THE STRUCTURE OF AMINO ACIDS

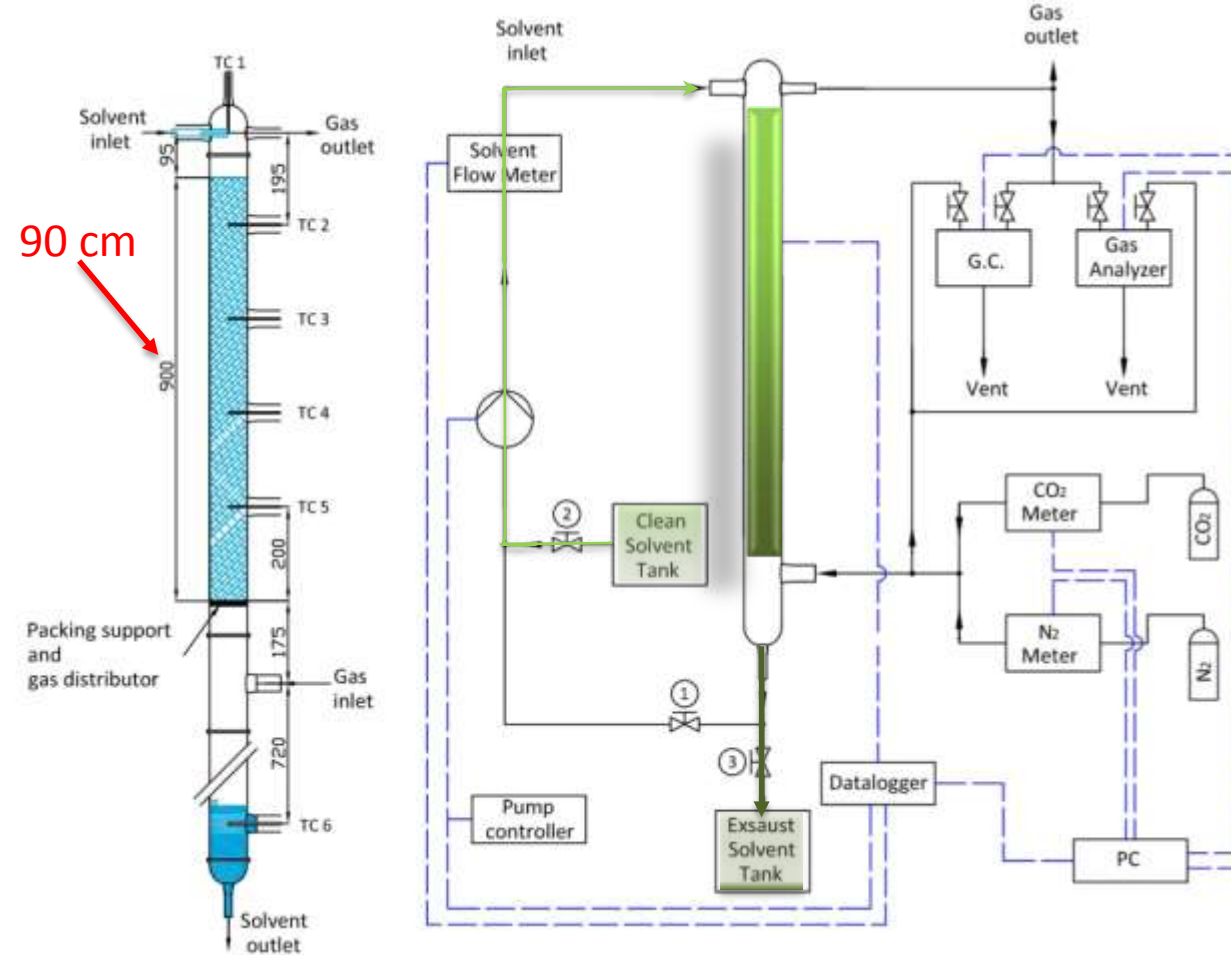


- Central carbon atom bonded to carboxyl group, amino group, hydrogen atom, side chain (R)
- R → only difference among the 20 most common amino acids
- R → affects molecular structure, size and electric charge, impacts on water solubility
- In water solutions, the following equilibrium is established (pH environment):

$$\begin{array}{ccccc}
 \text{HOOC} - \text{CHR} - \text{NH}_3^+ & \xrightleftharpoons{-\text{H}^+} & ^-\text{OOC} - \text{CHR} - \text{NH}_3^+ & \xrightleftharpoons{-\text{H}^+} & ^-\text{OOC} - \text{CHR} - \text{NH}_2 \\
 \text{(I)} & & \text{(II)} & & \text{(III)} \\
 \text{cationic (I),} & \text{zwitterionic (II) or} & \text{anionic (III) form} & &
 \end{array}$$
- Form III: CO₂ reactive, zwitterionic mechanism → + strong base, basic pH



MATERIALS and METHODS



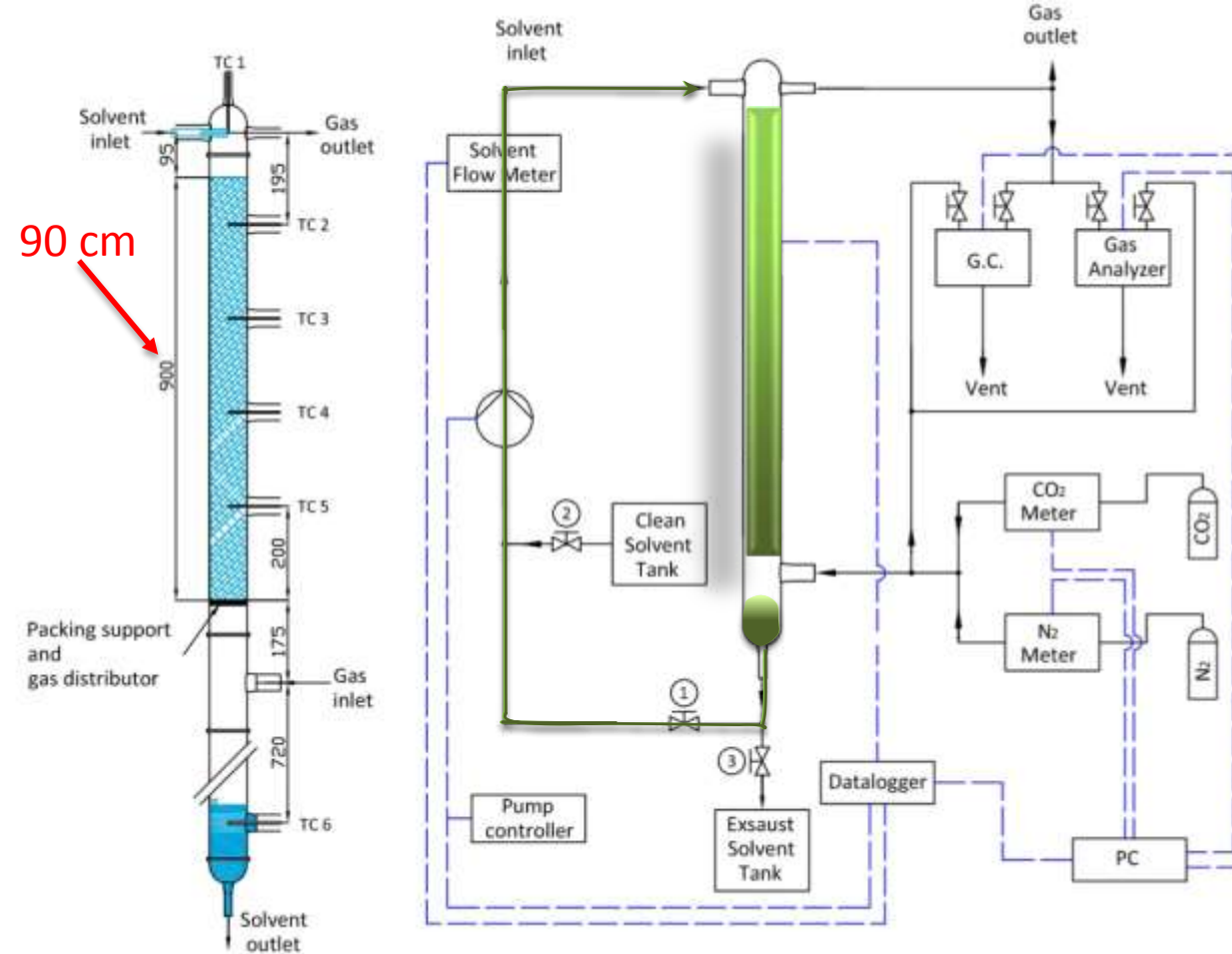
Equipment

- Glass column (adiabatic)
- 90 cm packed bed (metallic Raschig rings)
- Online analyser and micro GC for CO₂ gas concentration
- Mass flowmeter (gas side) and volumetric flowmeter (liquid side)

Open Cycle

- Counter current absorption of 4% CO₂ rich gas (open cycle) with tested solution at given concentration
- **Rich loading** over 90 cm absorption
- **Removal** calculation over 90 cm absorption

MATERIALS and METHODS



Equipment

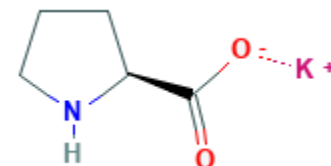
- Glass column (adiabatic)
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Closed Cycle

- Counter current absorption of 4% CO₂ rich gas (open cycle) with tested solution at given concentration
- Test duration → until **saturation**
- **Loading curves**, maximum loading, **capacity**
- Identification of an **Open Cycle Equivalent time lapse** and related figures of merit (e.g.: removal, partial capacity)

RESULTS

Solvent Selection: Potassium Prolinate vs. MEA

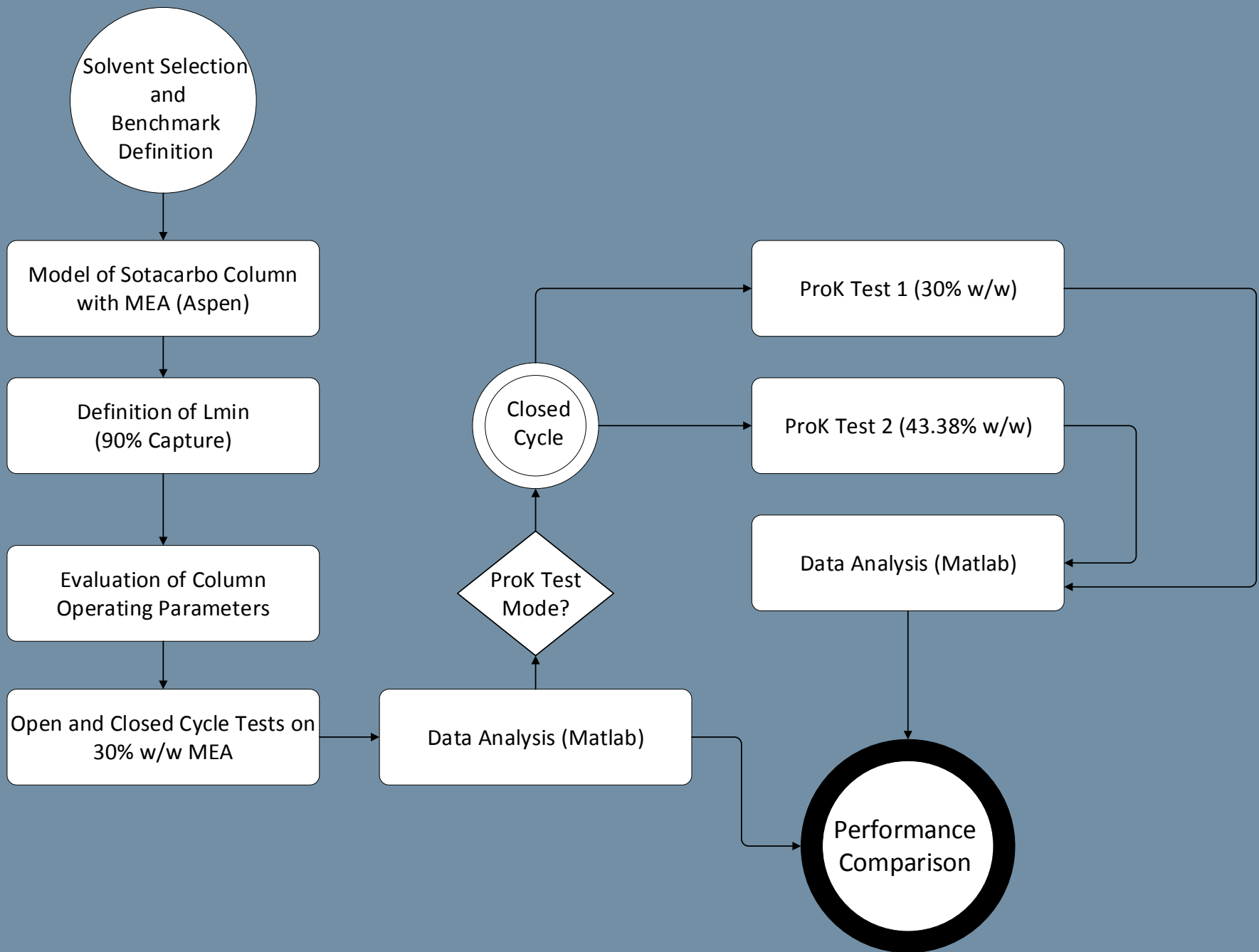


FOCUS ON: non-precipitating solvents

	C	T	Density	Viscosity	H _{CO2}	p _{CO2}	N _{CO2}	kov	D	pKa	Reference
	[M]	[K]	[kg/m ³]	[mPa*s]	[kPa*m ³ /kmol]	[kPa]	10 ⁻³ [mol/m ² s]	[s ⁻¹]	[10 ⁻⁹ m ² /s]	[-]	
ProK	0.97	303	1058.6	1.27	4384	2.92	4.00	26632	1.08	10.64	(Hamborg et al., 2008; Paul and Thomsen, 2012)
	2.00	303	1118.8	2.00	5806	3.09	4.58	71940	0.988		
	3.03	303	1167.8	3.46	7854	3.19	4.05	130855	0.819		
MEA	5.00	298	1010.6	2.48	3320	4.00	1 (@ 3M, 40°C)	90800	1.65	9.5	(Amundsen et al., 2009; Bui et al., 2014; Feron, 2016; Freguia, 2002; Hall, 1957; Luo et al., 2015)

- Higher AA viscosity and Henry constant
- Higher AA kinetic constant and N-CO₂
- Lower AA diffusivity

→ Solvent screening to include energy performance (e.g.: heat of regeneration)

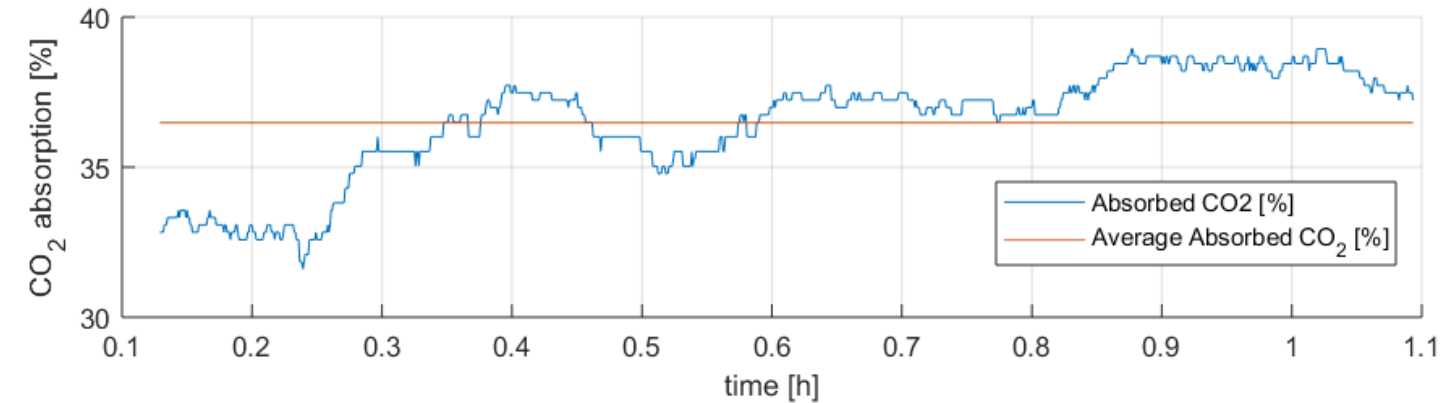


RESULTS

		OPEN CYCLE	CLOSED CYCLE			UNIT
		MEA	MEA	ProK-test 1	ProK-test 2	
Gas flow rate		111.71	111.86	111.79	111.81	mol/h
- molar	CO ₂	4.63	4.78	4.71	4.72	mol/h
	N ₂	107.08	107.08	107.08	107.08	mol/h
- volumetric	CO ₂	0.1	0.1	0.1	0.1	Nm ³ /h
	N ₂	2.4	2.4	2.4	2.4	Nm ³ /h
Liquid flow rate		3.5	3.5	3.4	3.8	l/h
- mass		3.5	3.5	3.8	4.4	kg/h
- mol		155	155	155	155	mol/h
Solvent concentration		30%	30%	30%	43.38%	w/w
- molar		5.0	5.0	2.2	3.2	mol/L
T _{gas} in		9	12.5	9.4	8.2	°C
T _{liquid} in		22	18	18	19	°C
L/G		1.39	1.39	1.39	1.39	mol/mol

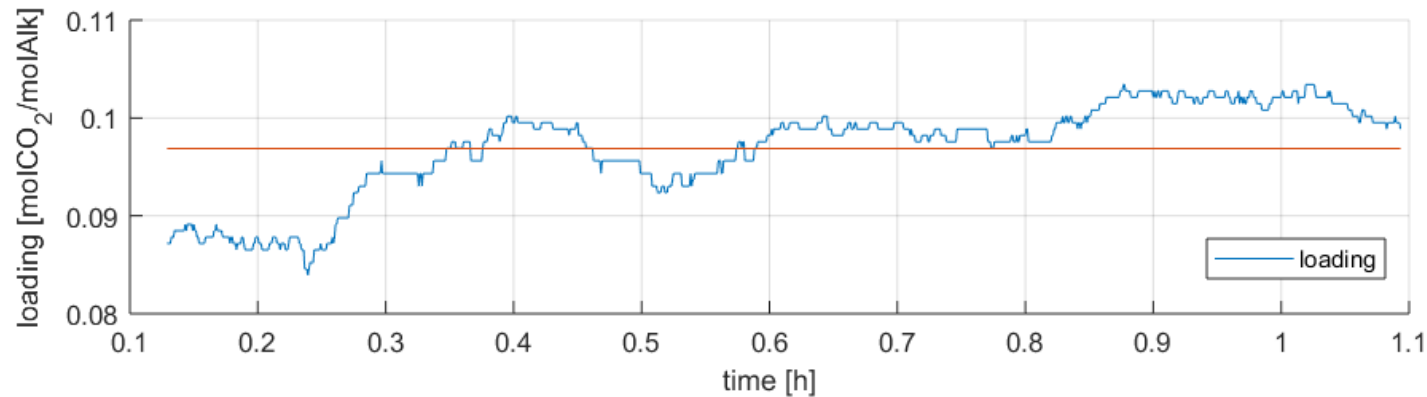
RESULTS

MEA Open Cycle Test (from Data Analysis)



Absorption

36.5%
CO₂ absorption (av.)

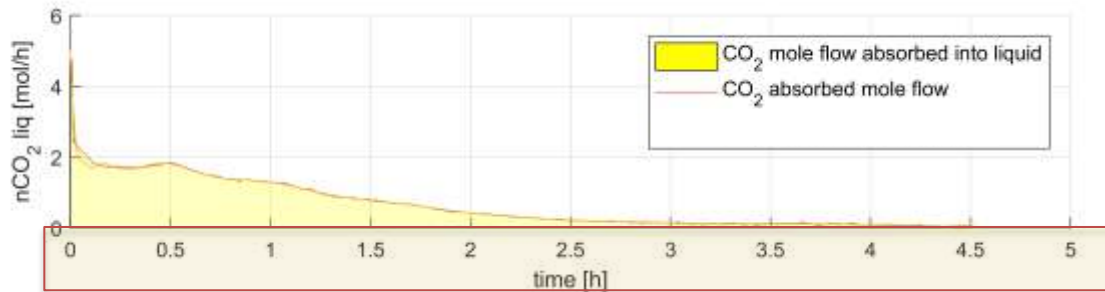


Loading

~0.1 molCO₂/molALk

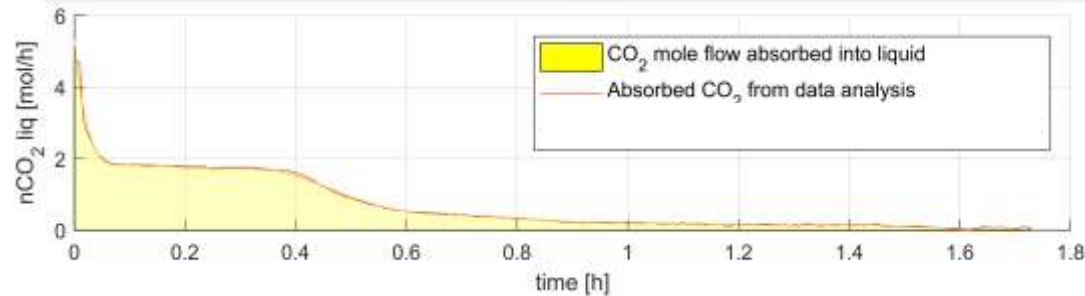
RESULTS

MEA vs. ProK Closed Cycle Test (from Data Analysis)

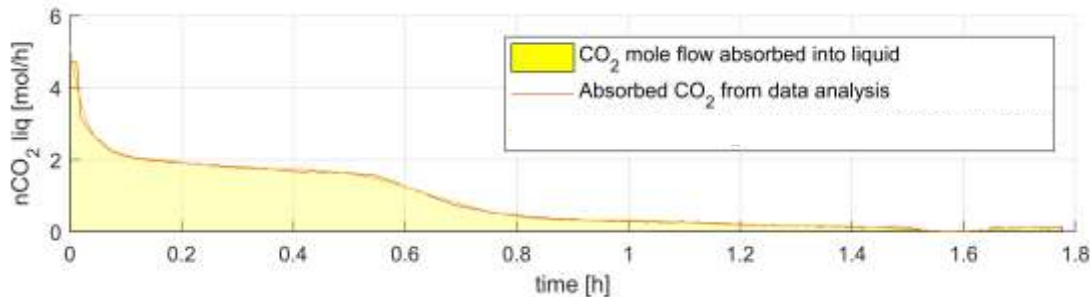


Absorbed flow rate-30% w/w MEA solution

Longer test duration



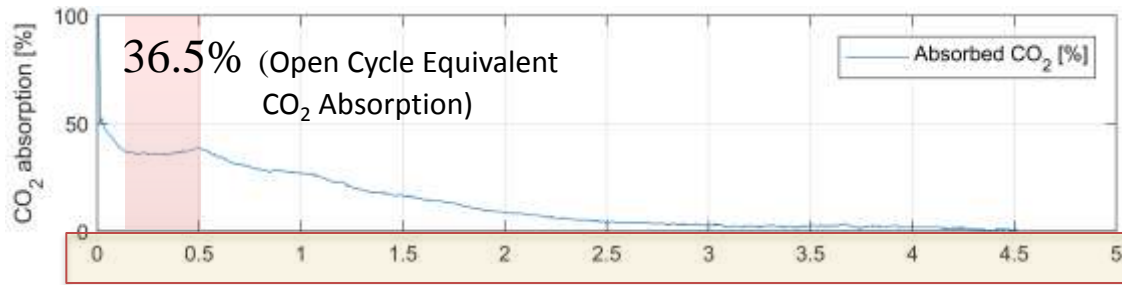
Absorbed flow rate-30% w/w ProK solution



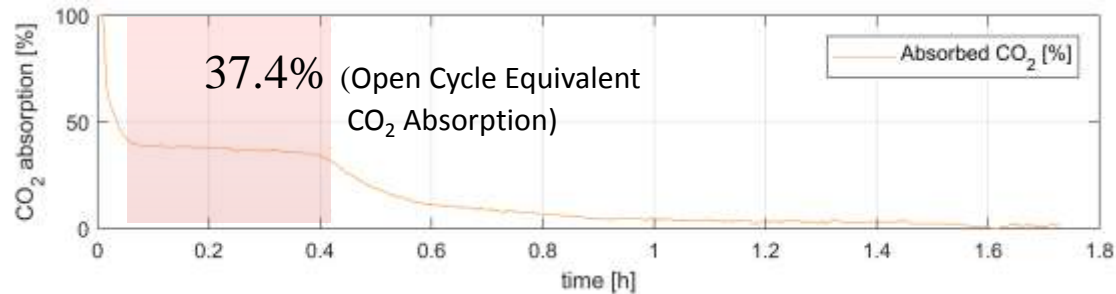
Absorbed flow rate-43.38% w/w ProK solution

RESULTS

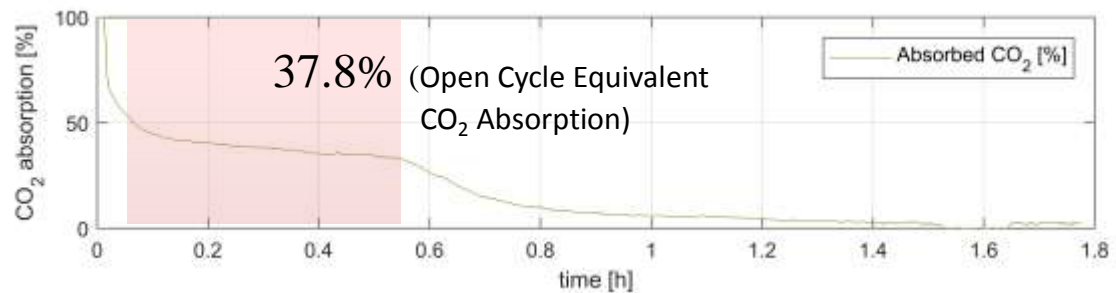
MEA vs. ProK Closed Cycle Test (from Data Analysis)



Absorption
30% w/w MEA solution

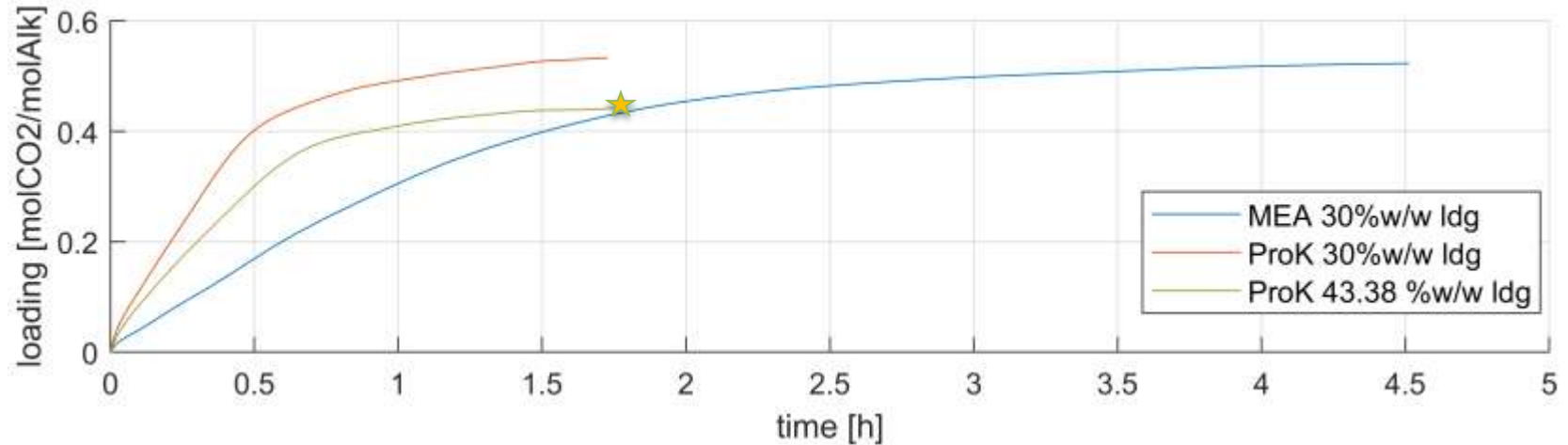


Absorption
30% w/w ProK solution



Absorption
43.38% w/w ProK solution

DISCUSSION



★ Precipitation detected

- From data analysis
- Faster loading increase detected during ProK tests
- Lower maximum loading achieved by 43.38%w/w ProK (**0.44 molCO₂/molAlk**)
- Comparable maximum loading of ProK and MEA 30%w/w (respectively **0.53 vs. 0.52 molCO₂/molAlk**)

DISCUSSION



	MEA-Closed Cycle	ProK-Test 1	ProK-Test 2	
			43.38%	
	30% w/w	30% w/w	w/w	Unit
Circulating solute $-n_{Alk}$ (MEA/ProK)	5.42	2.23	3.38	mol
Circulating solvent (water+solute)	1.103	1.138	1.193	kg
Mole of CO ₂ absorbed	2.83	1.19	1.50	mol
Calculated Loading (end of test)	0.52	0.53	0.44	molCO ₂ /molAlk
Calculated Capacity	2.57	1.04	1.25	molCO ₂ /kg solvent
Time period of Open Cycle Equivalent	0-0.48	0-0.39	0-0.54	h
Mole of CO ₂ absorbed Open Cycle Equivalent	0.88	0.76	1.09	mol
Partial capacity (end of Open Cycle Equivalent)	0.80	0.67	0.91	molCO ₂ /kg solvent
Average absorption (Open Cycle Equivalent)	36.5	37.4	37.8	%

CONCLUSION

Final Considerations

- ProK solutions (30% and 43.38%w/w) have been tested at **bench-scale** to investigate CO₂ absorption from synthetic NGCC flue gas;
- **Faster loading increase** of ProK vs. MEA
- **Similar maximum loading** of MEA vs. ProK 30%w/w;
- Calculated **capacity** at the end of the **MEA** closed cycle test is the **highest** one among the three assessed (2.57 molCO₂/kg_{solvent});
- Open cycle equivalent time-lapse → 43.38% w/w ProK shows higher partial capacity compared to MEA (0.91 vs. 0.80 molCO₂/kg Solvent)
- Open cycle equivalent time-lapse → comparable CO₂ removal among the 3 cases

Future Work

- Investigation of other AA for NGCC flue gas decarbonisation
- Modelling and experimental campaigns to estimate the **AA regeneration duty**
- Definition of thermodynamic models and **techno-economic assessment** for a comprehensive evaluation of AA performance



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Thank You for Your Attention

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INTRODUCTION

Motivation

- Amines → Primary, secondary and tertiary
- Unhindered (primary or secondary) amines form a fairly stable carbamate → high energy requirement for solvent regeneration
- Hindered (tertiary) amines form an unstable carbamate and have a higher theoretical capacity
- Tertiary amines regeneration is less energy-demanding than unhindered amines
- Low rates of absorption make tertiary amines difficult to be used for CO₂ gas removal
- MEA considered a benchmark in the field of CO₂ capture via chemical absorption → economical technology
- MEA + CO₂ → high reaction rate and capacity, low molecular weight and cost, high heat of regeneration (~3.5-3.9 GJ/ton CO₂);
- MEA is affected by vaporization losses due to high vapor pressure, it is corrosive and it forms degeneration products (oxidative and thermal degradation), toxicity issues

