Advanced bipolar plates without flow channels, for PEM electrolysers operating at high pressure

Hydrogen Session – Bipolar plates for PEM fuel cells and electrolyzers



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<u>Emile Tabu Ojong</u>¹, Eric Mayousse², Tom Smolinka¹, Nicolas Guillet²

 ¹Fraunhofer-Institut für Solare Energiesysteme ISE, Freiburg - Germany
 ²CEA – LITEN, Laboratoire d'Innovation pour les Technologies des Energies nouvelles et les Nanomatériaux, Grenoble - France

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Merits and challenges of high pressure PEM water electrolysis

Merits

- Splitting of water into its constituent elements by use of electricity
- Storage of excess power from renewable energy sources
- Highly efficient with zero carbon footprint
- Reduced system cost for operation at high pressure



\rightarrow Bipolar plate is the critical component for costs and life span improvements



The multifunctional bipolar plate

| Functions | Required properties | | |
|--|--|--|--|
| Conduction of electrical current from cell to cell | High electrical conductivity | | |
| Facilitation of heat management | Good thermal conductivity | | |
| Flow distribution of reactant water and | Highly impermeable to gases | | |
| product gases | Corrosion resistant on anode side | | |
| | Hydrogen embrittlement resistant on cathode side | | |
| | High electrochemical stability | | |
| Constitutes most part of the mass and | High mechanical stability | | |
| volume of electrolyser | Low material and production costs | | |
| | Availability | | |



Bipolar plates development at Fraunhofer ISE

- Conventional design
 - Machined Ti plates, 50 cm² active area
 - Expensive
- Gold coated design
 - Injection molded PPS
 - 9 cm² active area
 - Highly durable but expensive
- Low cost design
 - Injection molded plate with inner Ti pin
 - 78 cm²active area
 - Low thermal management and low power density
- Second generation low cost design
 - Thin unmachined Ti plate
 - Better thermal management
 - Problems with gas tightness







Major bipolar plate challenges

- Strong corrosive conditions on the anode side due to:
 - Anodic polarisation
 - Operation at elevated temperatures
 - Presence of oxygen
- Hydrogen embrittlement of metals on the cathode side
- High material costs and manufacturing techniques

R&D focus

- Screening of candidate materials based on corrosion and hydrogen embrittlement resistance
- Comprehensive cost analysis model on material and production techniques
- Novel design concepts













Benchmark materials and Cost break down model

Cost model and assumptions

- Material costs based on offers from suppliers that guarantee real market prices
- Manufacturing costs from in-house experience and information from subcontractors
- Cost model accounts for all steps in the production process
- Waste materials such as shavings are recycled and sold for a third of the original price
- Two stack design concepts (conventional and advanced) are considered

| Components | Specifications | | |
|---------------------------|---|--|--|
| Bipolar plates | Titanium | | |
| Cell frame | PPS GF40 | | |
| Anode catalyst | IrO ₂ | | |
| Anode loading | 2 mg/cm ² | | |
| Cathode catalyst | 40 wt. % Pt on carbon | | |
| Cathode loading | 1 mg/cm² | | |
| Membrane | Nafion 117 | | |
| Anode current collector | Sintered Ti, expanded Ti mesh, Ti felt | | |
| Cathode current collector | Carbon paper, sintered Ti, expanded Ti mesh, Ti felt | | |



Conventional Vs. Advanced design





BiP Manufacturing costs break down

- Machining of Titanium bipolar plates is quite expensive
- Only slight cost reduction with increasing production rate
- Cost target of 2500 € / Nm³h-1 cannot be met using machined bipolar plates





Corrosion screening of candidate bipolar plate materials

- Corrosion tests performed in a three electrodes electrochemical cell
- Hg/Hg₂SO₄ / K₂SO₄ (0,690 V vs. R.H.E) reference electrode
- 0,5M H₂SO₄ electrolyte
- pH 3,3
- Candidate materials tested
 - Grades of stainless steel
 - Tantalum coated stainless steel
 - Hastealloys
 - Various grades of Titanium







Stainless steel grades

| | Fe (Wt%) | Ni (Wt%) | Cr (Wt%) | Mo (Wt%) | Mn (Wt%) | | |
|---------|--|----------|----------|----------|----------|--|--|
| SS 316L | 0,68 | 0,11 | 0,17 | 0,02 | 0,02 | | |
| SS 904L | 0,49 | 0,26 | 0,21 | 0,02 | 0,01 | | |
| TCS | Low cost surface modification on 316L and 904L | | | | | | |



E (V vs. RHE)

E (V vs. RHE)

| | 316 L | 316LTS C | 904 L | 904LTS C | Ti Gr2 | DOE Objective |
|---|----------|-------------|----------|-------------|--------|---------------|
| Corrosion current at 2V vs. RHE (µA/cm²) | 96,1 | 88,2 | 42,4 | 31,8 | 10 | < 16 |





Tantalum coated stainless steel

- Tantalum coated by electrodeposition in ionic liquids
- A second sample of Ta coated SS316L was annealed at 500°C under air before testing



| | 316 L | 316L+Ta | 316L+Ta Annealed | Ti Gr2 | DOE Objective |
|---|----------|---------|---------------------|--------|---------------|
| Corrosion current at 2V vs. RHE (µA/cm ²) | 63,4 | 41,8 | 99,6 | 10 | < 16 |



Hastealloys

| | Fe (Wt%) | Ni (Wt%) | Cr (Wt%) | Mo (Wt%) | Mn (Wt%) |
|---------------|----------|----------|----------|----------|----------|
| Cronifer 1925 | 0,47 | 0,25 | 0,19 | 0,06 | 0,01 |
| Nicrofer 3127 | 0,32 | 0,31 | 0,27 | 0,06 | 0,02 |
| Nicrofer 5923 | 0,01 | 0,59 | 0,23 | 0,16 | - |



E (V vs. RHE)

E (V vs. RHE)

| | 1925 | 3127 | 5923 | Ti Gr2 | DOE Objective |
|---|------|------|------|--------|---------------|
| Corrosion current at 2V vs. RHE (µA/cm ²) | 63,4 | 41,8 | 99,6 | 10 | < 16 |



Titanium grades

| | C (Wt%) | Fe (Wt%) | H (Wt%) | N (Wt%) | O (Wt%) | Pd (Wt%) | Mo(Wt %) | Ni(Wt%) |
|----------|------------|-------------|------------|------------|------------|-------------|-------------|-------------|
| Grade 1 | 0,1 | 0,5 | 0,015 | 0,05 | 0,4 | - | - | - |
| Grade 2 | 0,1 | 0,3 | 0,015 | 0,05 | 0,35 | - | - | - |
| Grade 7 | 0,1 | 0,3 | 0,015 | 0,05 | 0,35 | 0,2 | - | - |
| Grade 12 | 0,1 | 0,3 | 0,015 | 0,05 | 0,35 | - | 0,3 | 0,8 |



E (V vs. RHE)

| | Grade 1 | Grade 2 | Grade 7 | Grade 12 | DOE Objective |
|--|---------|---------|---------|----------|---------------|
| Corrosion current at 2V vs. RHE (µA/cm²) | 15,4 | 10 | 14,1 | 6,3 | < 16 |



SEM and EDAX analysis for Ti Gr.2

As received



Polished







Trade-off

- Basically, all titanium grades meet the corrosion resistance target !
- Material cost become major trade-off criterion
- Availability also taken into consideration
- Concerns about the possibility of nickel leaching into electrolyser water and to the environment
- Likelihood of leaching not studied
- Titanium grade 2 is chosen as the preferred material for used as bipolar plate, due to corrosion resistance and relatively low cost
- Bipolar plates without machined channels

| Approximate material cost ratio* | | | | | | |
|----------------------------------|---------------|------------|--|--|--|--|
| | ASTM Grade | Cost ratio | | | | |
| Unalloyed Ti | 2 | 1,00 | | | | |
| Ti-0,3Mo-0,8Ni | 12 | 1,12 | | | | |
| Ti-0,15Pd | 7 | 1,90 | | | | |
| Ti-0,06Pd | 16 | 1,38 | | | | |
| Ti-0,1Ru | 26 | 1,15 | | | | |
| Ti-3AI-2,5V | 9 | 1,25 | | | | |
| Ti-3Al-2,5V-0,05Pd | 18 | 1,60 | | | | |
| Ti-3Al-2,5V-0,1Ru | 28 | 1,38 | | | | |
| Ti-6Al-4V | 5 | 1,22 | | | | |
| Ti-6AI-4V-0,05Pd | 24 | 1,57 | | | | |
| Ti-6Al-4V-0,1Ru | 29 | 1,34 | | | | |
| *Source: R.W \$ | Schutz et al. | 1996 | | | | |



Performance of conventional Vs. advanced design

- Laboratory test cells, both 25 cm² active area
- Sintered Ti Gr.2 discs as current collectors
- Fumatech EF-40 (230µm) MEA
- Increased electronic conduction
- Higher contact surface area





Outlook

In-situ tests with short stacks, 5 cells and then 10 cells

- 150 cm² cell active area
- 1,8 V nominal cell voltage
- 1 A/cm² current density
- Up to 30 bar operating pressure
- Characterisation after up to 1000 hours of operation
- Concerns about hydrogen embrittlement of titanium
- Questions about titanium self ignition
- Further investigation on other coating configurations and surface modifications



Thank you for your attention !!



M.Sc. Emile Tabu Ojong Fraunhofer – Institute for Solar Energy sytsems Heidenhofstr. 2; 79110 – Freiburg; Germany Ph: +49 761 4588 5335 emile.tabu.ojong@ise.fraunhofer.de www.ise.fraunhofer.de

