

## Thermodynamic Analysis of Reforming Processes

Shareq Mohd Nazir<sup>a\*</sup>, Schalk Cloete<sup>b</sup>, Shahriar Amini<sup>a,b</sup>, Olav Bolland<sup>a</sup>

- a. Department of Energy and Process Engineering, NTNU, Trondheim, Norway
- b. Sintef Material and Chemistry, Trondheim, Norway

Presenter's Email address: <a href="mailto:shareq.m.nazir@ntnu.no">shareq.m.nazir@ntnu.no</a>

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# NanoSim – EU FP7 Project

 A Multiscale Simulation-Based Design Platform for Cost-Effective CO<sub>2</sub> Capture Processes using Nano-Structured Materials (NanoSim)



- Connect models at different scales
- Reduce time spent on materials development
- To accelerate rationale development of CO<sub>2</sub> capture processes
- To demonstrate the technoeconomic competitiveness of CO<sub>2</sub> capture process based on Chemical Looping Reforming using Nano-Structured materials

# **Objective of the Current Work**

- Identify the thermodynamic potential of a Chemical Looping Reforming (CLR) process
- Exergy analysis of Chemical Looping Reforming (CLR) and conventional Partial Oxidation (POX) process
- Comparison of Exergy Destruction in CLR and POX at different operating conditions

# Chemical Looping Reforming (CLR)





- Where Me/MeO is the metal oxygen carrier system
- Side reactions occur to yield fractions of CO<sub>2</sub> and H<sub>2</sub>O

# **Chemical Looping Reforming**

- Pre-combustion CO<sub>2</sub> Capture
- Inherent Air Separation
- Process Intensification
- Operates at fairly low temperatures
- Gives higher H<sub>2</sub>/CO ratio when compared to conventional partial oxidation process

# **Thermodynamic Analysis - Exergy**

### Exergy

- Maximum useful work that can be derived from a system
- A method to account for irreversibilities in a system

$$E_D = \sum E_Q - W_{CV} + \sum E_i - \sum E_e$$

$$\mathsf{E}_{\mathsf{Q}} = \mathsf{Q} \; (1 - \mathsf{T}/\mathsf{T}_{\mathsf{o}})$$

Where

- Q Heat transfer across the system
- T Temperature of the system
- T<sub>o</sub> Ambient Temperature
- E<sub>Q</sub> heat transfer exergy
- W<sub>CV</sub> Work done by the system
- $E_i$ ,  $E_e$  Total exergy of the streams In and Out respectively
- E<sub>D</sub> Exergy destroyed in the system

# Methodology



# Methodology

### $ExD\% = (E_D/E_{CH4})^*100$

### Where

- E<sub>D</sub> Exergy destroyed in the system
- ExD% Percentage of exergy destroyed
- E<sub>CH4</sub> Chemical exergy of fuel (CH<sub>4</sub>)

Assumptions and Considerations:

- Air is considered a binary mixture of 21%  $O_2$  and 79 %  $N_2$  (mole fractions)
- Ni/NiO has been considered as the metal-metal oxide system
- Work input to Air Separation Unit (ASU) = 28.51 kJ/mol O2 (0.25 kWh/kg O<sub>2</sub>)
- Equilibrium data at different conditions have been taken from ASPEN Plus
- Reactions considered to proceed with minimization of Gibbs Free Energy principle
- Peng Robinson Equation of State has been considered
- Heat transfer across the system boundary occurs at constant temperature

### **Partial Oxidation**



#### Identifying best way to operate Partial Oxidation

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### **Chemical Looping Reforming**



#### Identifying best way to operate Chemical Looping Reforming

Partial Oxidation (POX) vs Chemial Looping Reforming (CLR)



Temperature of reactor exit streams at adiabatic conditions

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Partial Oxidation (POX) vs Chemial Looping Reforming (CLR)



Temperature of exit streams suited to water gas shift reaction

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### Partial Oxidation (POX) vs Chemial Looping Reforming (CLR)

CH<sub>4</sub> Conversion and H<sub>2</sub>/CO ratio



High Metal Circulation Rate in Chemical Looping Reforming at constant  $O_2$  input (0.75 mol  $O_2$  / 1 mol  $CH_4$ )



# Conclusions

- CLR seems to be a promising new method, with small thermodynamic losses and without the need for an air separation unit.
- Chemical Looping Reforming can be adiabatic no need for external supply of heat
- Exergy destruction in CLR is less than in POX, since the temperature of exit streams from POX is very high, and cooling them down to a suitable water gas shift temperature results in high exergy losses
- CLR reforms CH4 to a product gas with higher H<sub>2</sub>/CO ratio when compared to conventional POX

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## **Thank You**

