



Multiscale Mixed FEM for Near-well Modeling

S. Krogstad*, L.J. Durlofsky

*SINTEF ICT, Applied Mathematics
(J. Aarnes, V. Kippe, K.-A. Lie)

SUPRI-B Industrial Affiliates Meeting, May 8-9, 2006

Outline

- Motivation
- Multiscale Mixed Finite Element Methods (MsMFEM)
- MsMFEM for near-well modeling
- Numerical experiments
- Conclusions / Further work

Motivation:



Near-well region
extremely important
Cannot fully resolve
all scales in typical
simulation
Multiscale methods
incorporate fine
scales in coarse scale
equations

Multiscale Methods for Reservoir Simulation

Multiscale Finite Element Method

T. Hou, X. H. Wu, 1997

Multiscale Mixed FEM

Z. Chen, T. Hou, 2003

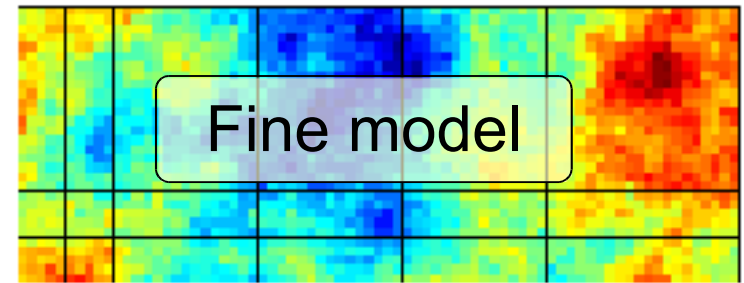
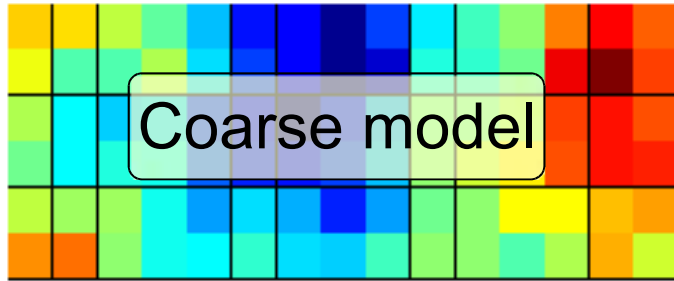
T. Arbogast et al., 2000

J. Aarnes et al., 2004 (group at SINTEF)

Multiscale Finite Volume Method

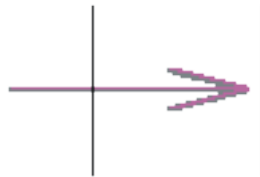
P. Jenny, S. H. Lee, H.A. Tchelepi, 2003

Standard / Multiscale Discretization

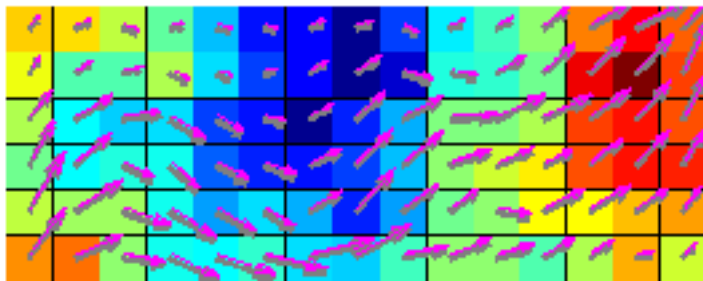


Standard

Local flow:

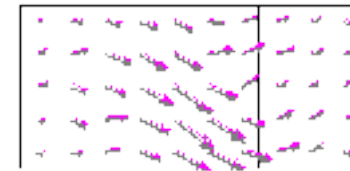


Solve **coarse** equations

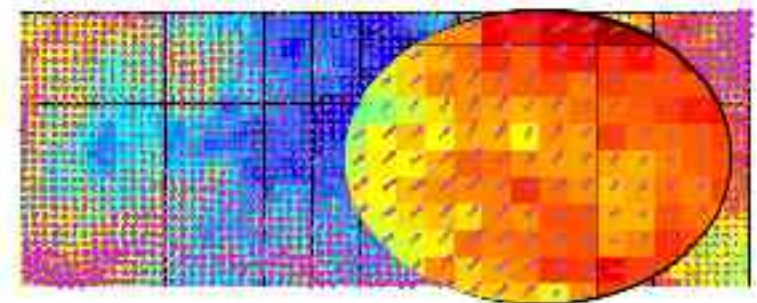


Multiscale

Local flow:



Solve **coarse** equations /
form fine scale flow



Mixed Finite Elements (MFEM)

Model equations:

$$v = -\lambda K \nabla p$$
$$\nabla \cdot v = q$$

Choose basis:

$$v = \sum \psi_i$$
$$p = \sum p_j \phi_j$$

Weak formulation:

$$\int v \cdot (\lambda K)^{-1} \hat{v} - \int p \nabla \cdot \hat{v} = 0$$
$$\int \hat{p} \nabla \cdot v = \int \hat{p} q$$

for all $(\hat{v}, \hat{p}) \in U \times V$.

Mixed discretization:

$$\begin{pmatrix} \mathbf{A} & \mathbf{B} \\ \mathbf{B}^T & \mathbf{0} \end{pmatrix} \begin{pmatrix} \mathbf{v} \\ -\mathbf{p} \end{pmatrix} = \begin{pmatrix} \mathbf{0} \\ \mathbf{q} \end{pmatrix}$$

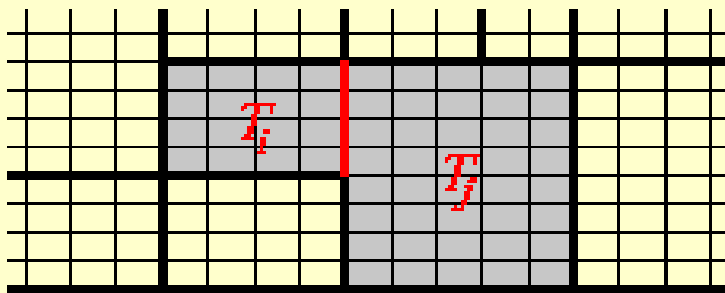
Multiscale MFEM (MsMFEM)

Flux basis function, ψ :

$$\psi = -K\nabla p_\psi$$

$$\nabla \cdot \psi = \begin{cases} w_i & \text{for } x \in T_i \\ -w_j & \text{for } x \in T_j \end{cases}$$

$$\psi \cdot n = 0 \text{ on } \partial(T_i \square T_j)$$



Initially compute basis functions

for n=1 **to** N

Solve coarse system based on current saturation

Form fine scale fluxes

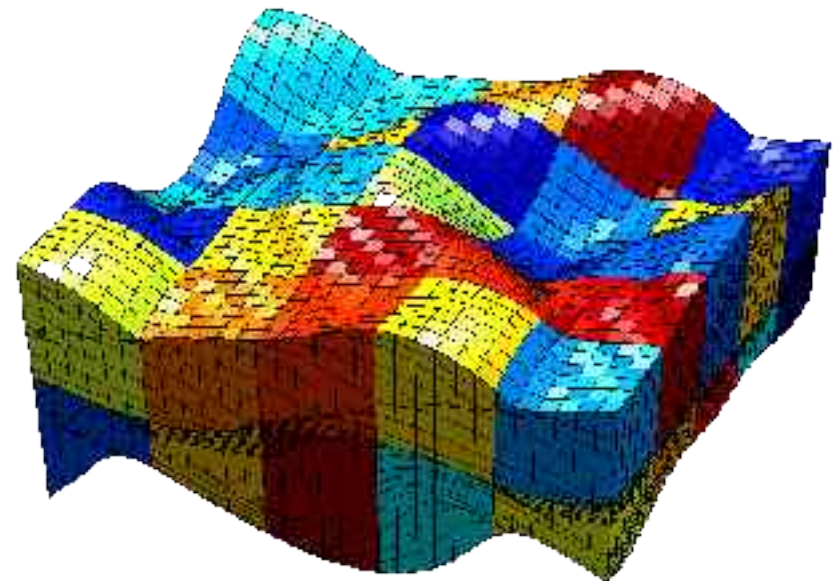
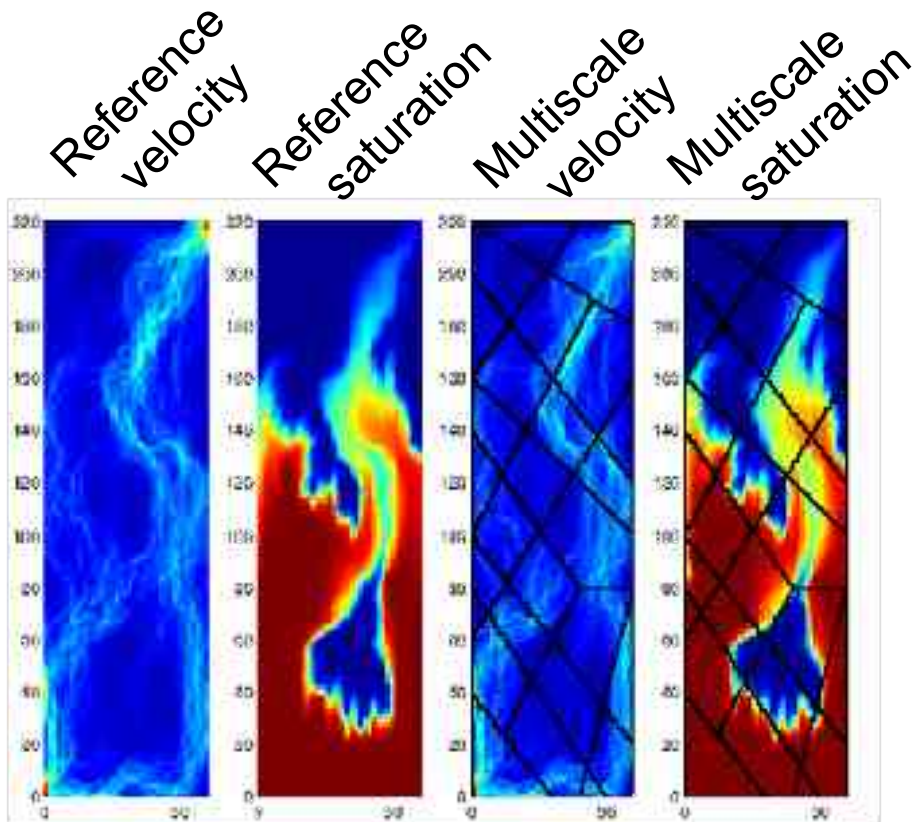
Advance fine scale saturation by Δt

end

Flexible Gridding

Coarse blocks: Any collection of fine grid cells

Fine cells: Both subdivision / MFEM and *mimetic* FDM have been implemented





Options for Improving Accuracy

Incorporate global information in the basis functions

Use overlap / border regions for the computation of basis functions

Occasionally update basis functions to account for mobility effects

MsMFEM for Near-well Modeling

Goal: Incorporate wellbore flow models into the MsMFEM framework

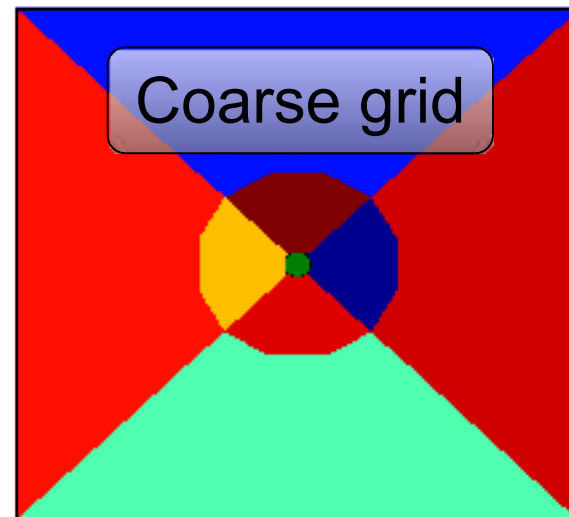
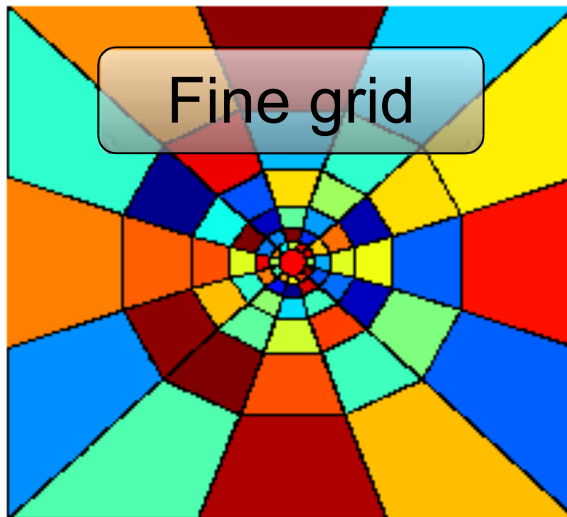
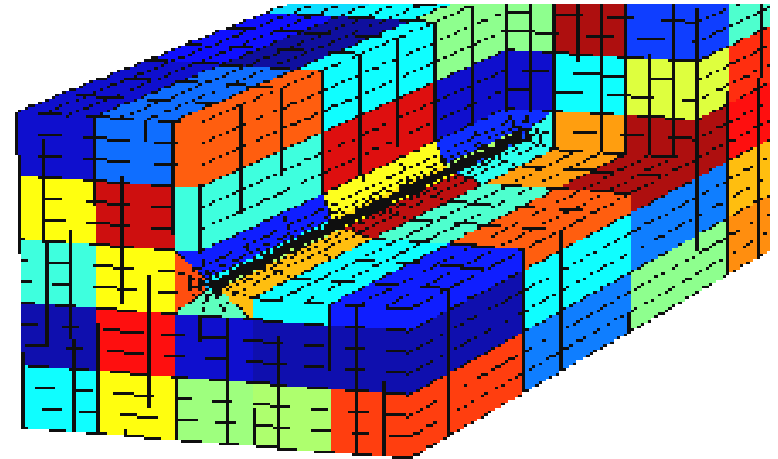
Obtain detailed flow in the near-well region while solving only a moderate sized system

Incorporate drift flux model for pressure drop in wellbore

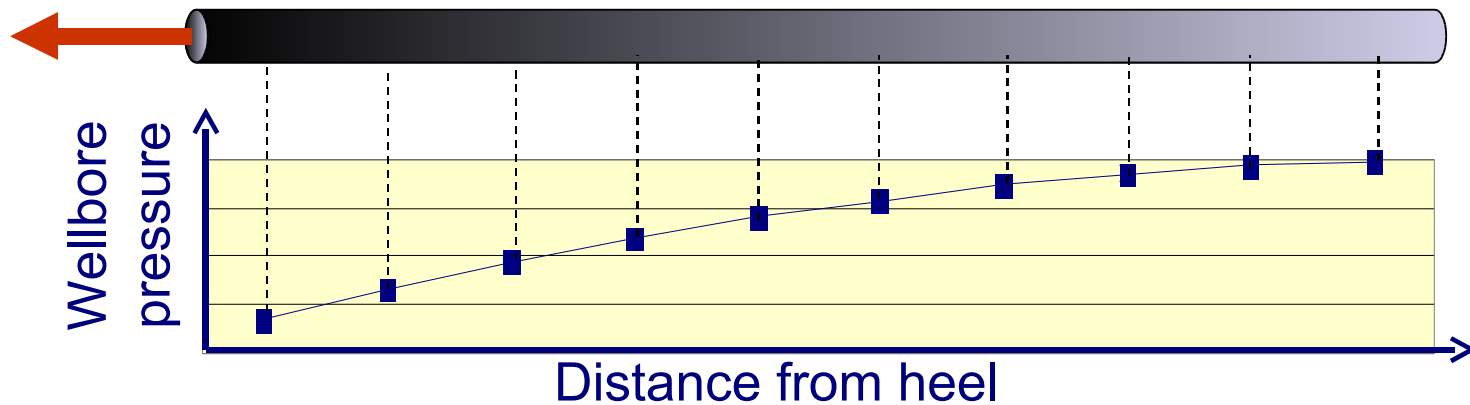
$$\Delta p = \Delta p_f + \Delta p_a + \Delta p_h$$
$$\frac{2L f_{tp} \rho_m v_m^2}{D} \quad \frac{2q_m \rho_m v_m}{A} \quad \rho_m g L \sin \theta$$

Well – Reservoir Linkage

- Fine grid to the annulus/ well segments included in the grid
- Well segments treated as coarse blocks / no well model is used



Wellbore Pressure Loss Treatment



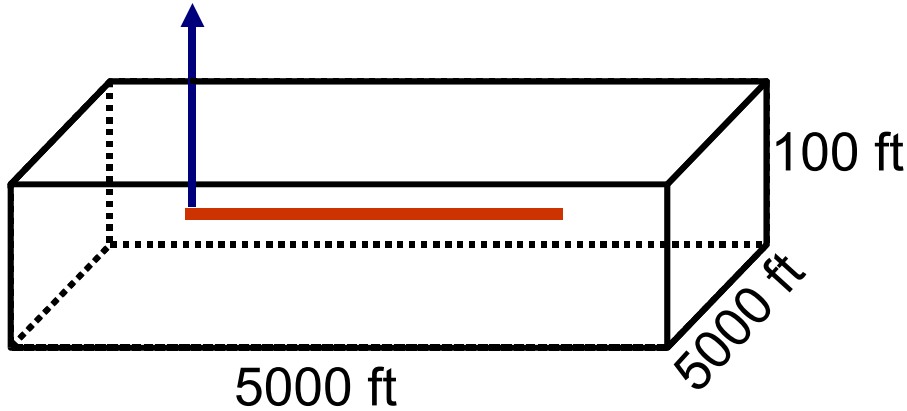
- Frictional pressure loss evaluated using previous and current time steps

$$\frac{\partial p_{n+1}}{\partial L} = -C_{n+1} v_{n+1}^2 \approx -C_n v_n v_{n+1}$$

- Successive substitution to obtain wellbore pressure at first time step

Numerical Experiments: Single-phase

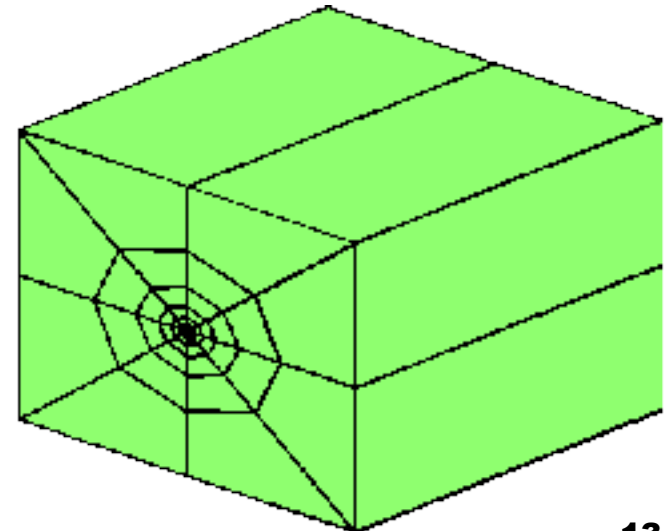
Homogeneous reservoir (validation) : model



Fine cells	18400
Coarse blocks	1900
Well segments	30

Isotropic permeability, <i>md</i>	200
Compressibility, <i>psi</i> ⁻¹	10 ⁻⁴
Wellbore radius, <i>inch</i>	2.0
Well length, <i>ft</i>	3000
Pipe roughness, <i>inch</i>	0.0012

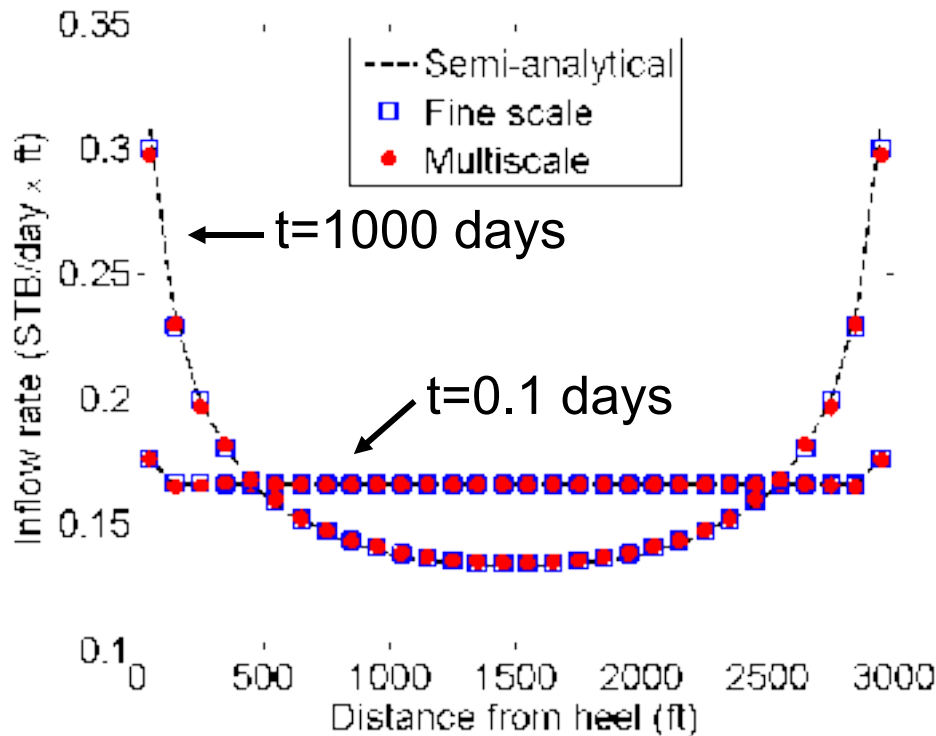
Coarse block



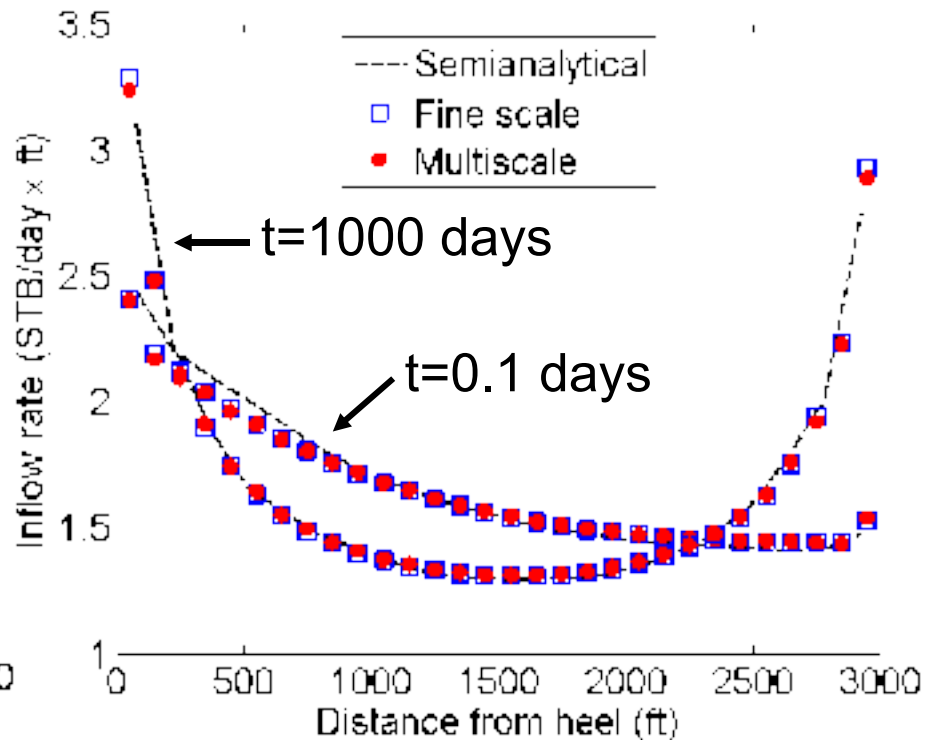
Numerical Experiments: Single-phase

Homogeneous reservoir (validation) : results

Production rate:
500 STB/day

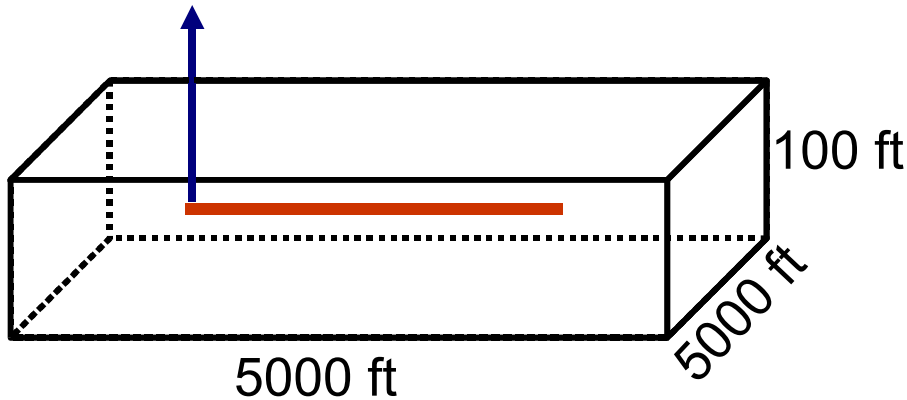


Production rate:
5000 STB/day



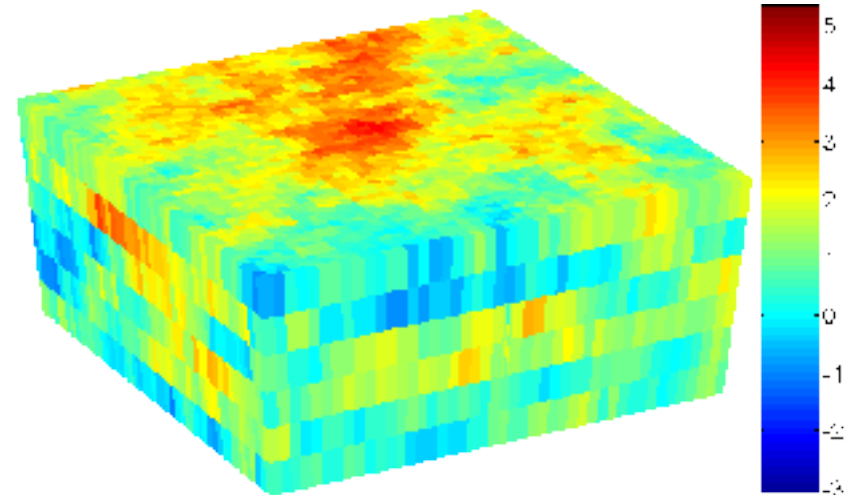
Numerical Experiments: Single-phase

Heterogeneous reservoir : model



Fine cells	18400
Coarse blocks	1900
Well segments	30

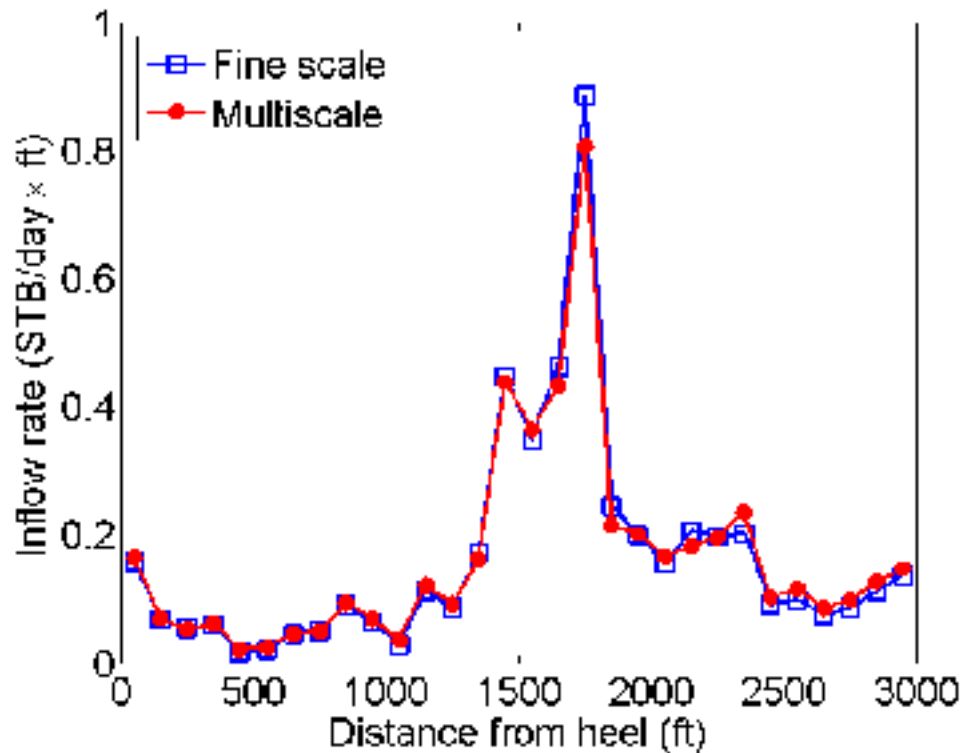
Isotropic permeability, <i>md</i>	10^{-3} - 10^5
Compressibility, <i>psi</i> ⁻¹	10^{-4}
Wellbore radius, <i>inch</i>	2.0
Well length, <i>ft</i>	3000
Pipe roughness, <i>inch</i>	0.0012



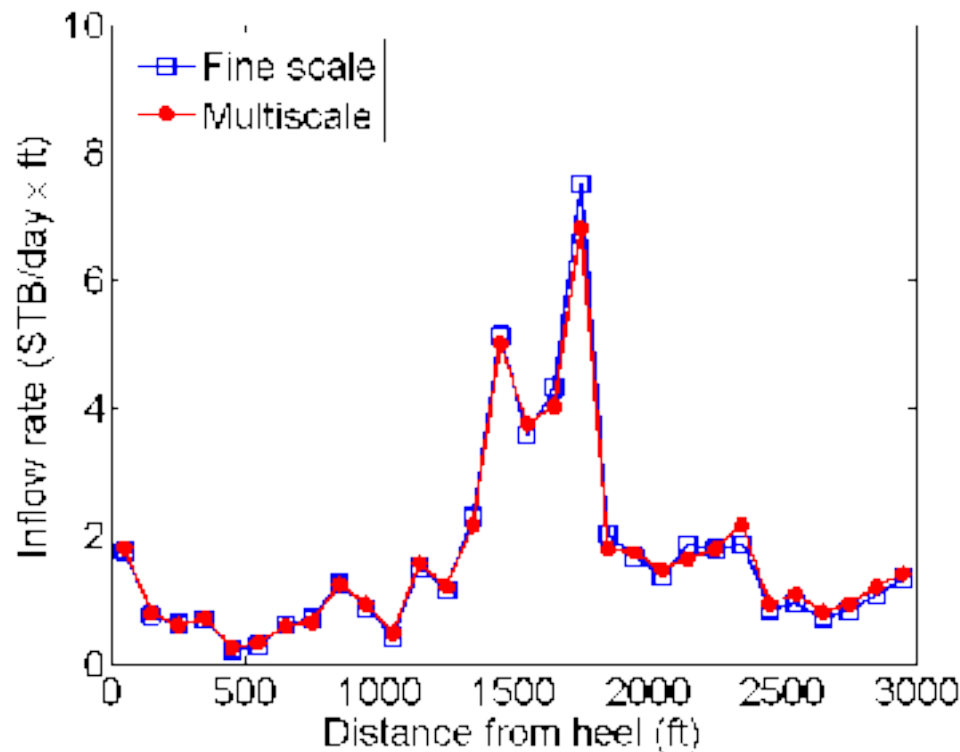
Numerical Experiments: Single-phase

Heterogeneous reservoir : Time = 1000 days

Production rate:
500 STB/day



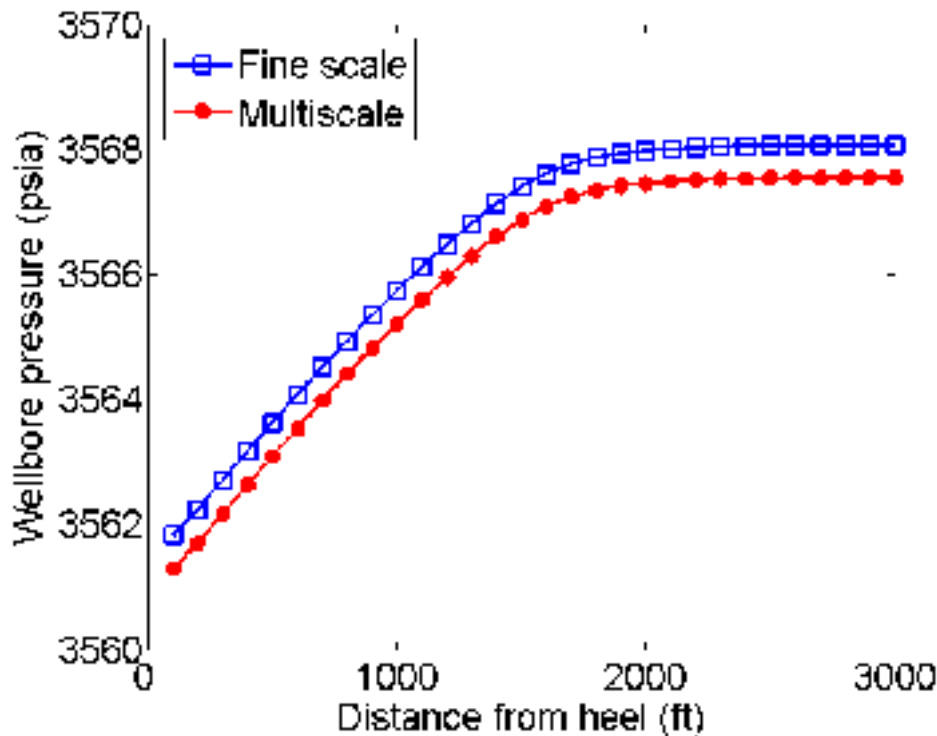
Production rate:
5000 STB/day



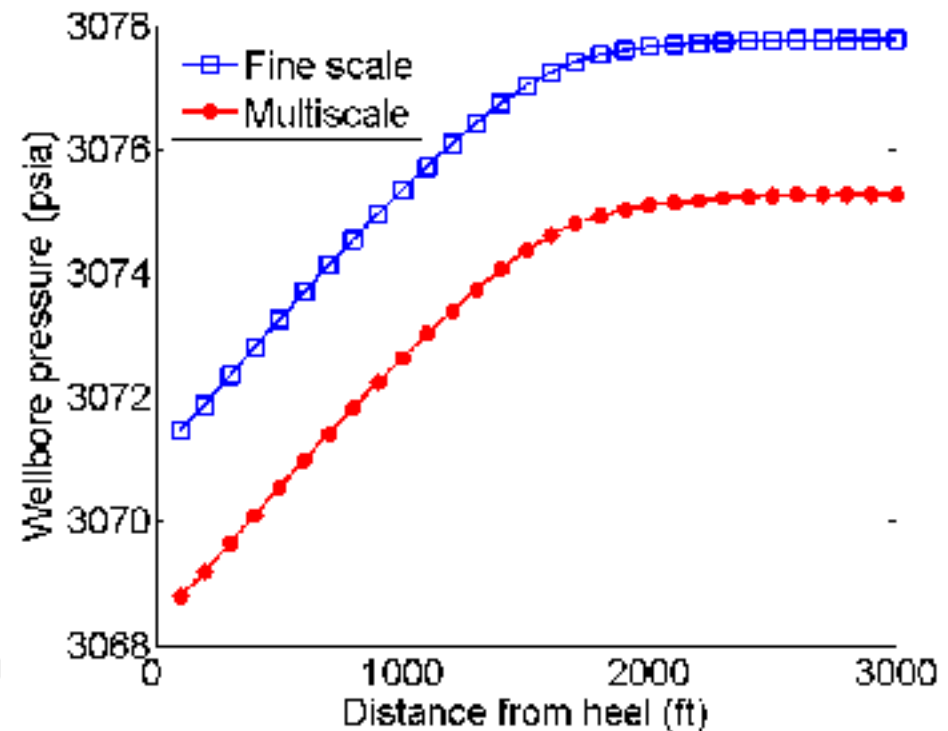
Numerical Experiments: Single-phase

Heterogeneous reservoir : 5000 STB/day

Time = 0.1 days



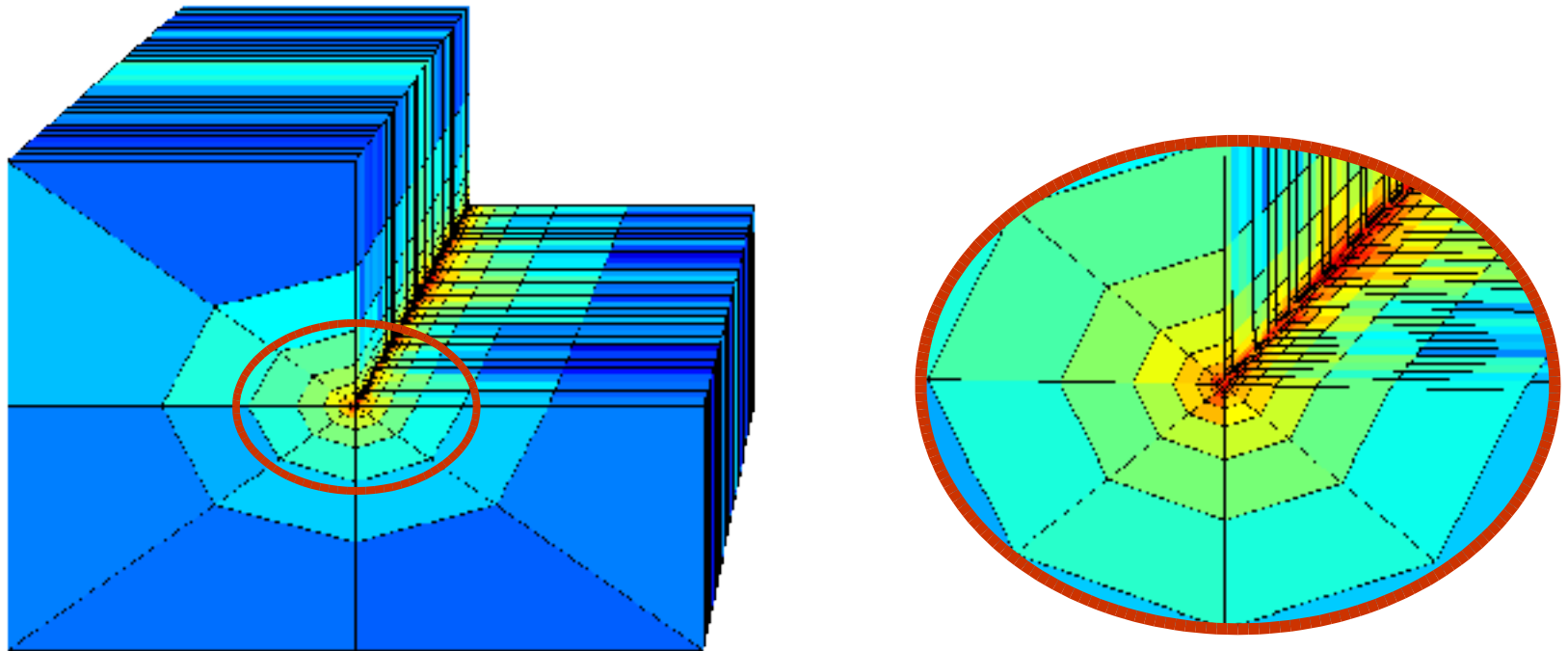
Time = 1000 days



Numerical Experiments: Single-phase

Heterogeneous reservoir : results

Velocity profile around well:



Conclusions / Further Work

Extended MsMFEM to include wellbore flow models

Presented numerical examples for single-phase flow

Further develop and test two-phase capability

Apply to complex wells