

A Discontinuous Galerkin Method for Computing Flow in Porous Media

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Stuttgart, November 24 2005

Outline

- 1 The Time-Of-Flight Equation
- 2 The Discontinuous Galerkin Method
 - The Discontinuous Galerkin Space Discretisation
 - Reordering
 - Numerical Results
- 3 Tracer Flow
 - Stationary Distribution of Tracers
 - Numerical results
- 4 Multiphase Flow
 - Implicit DG Solution
 - Numerical Results

Motivation

Aim: Construct a fast method to compute flow in porous media
Method: Discontinuous Galerkin Method (DGM)

- reservoir flow
- groundwater flow

The Time-Of-Flight Equation

- Fluids flow with velocity \mathbf{v} obtained from Darcy's law,

$$\mathbf{v} = -\frac{\mathbf{K}}{\mu} \nabla p$$

- The time-of-flight of a particle along a streamline, Ψ :

$$T(x) = \int_{\Psi} \frac{ds}{|\mathbf{v}(\mathbf{x}(s))|}$$

- The time-of-flight is the solution of a boundary value problem:

$$\mathbf{v}(\mathbf{x}) \cdot \nabla T = 1, \quad T = 0 \text{ on } \Gamma^+$$

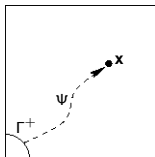
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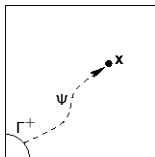
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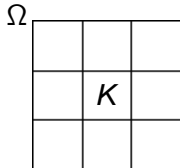
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Solution Space

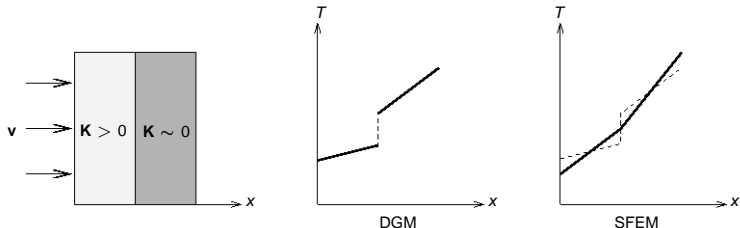
- Space for approximate solution T_h :

$$V_h^{(n)} = \{\varphi : \varphi|_K \in \mathbb{Q}^{(n-1)}\},$$

where $\mathbb{Q}^n = \text{span}\{x^p y^q : 0 \leq p, q \leq n\}$



- No continuity across inter-element boundaries



Variational Formulation

For all elements K , and for all $\varphi \in C_\infty(K)$:

$$\mathbf{v} \cdot \nabla T = 1$$

Variational Formulation

For all elements K , and for all $\varphi \in C_\infty(K)$:

$$\mathbf{v} \cdot \nabla T\varphi = 1\varphi$$

Variational Formulation

For all elements K , and for all $\varphi \in C_\infty(K)$:

$$\int_K \mathbf{v} \cdot \nabla T \varphi \, dx dy = \int_K \varphi \, dx dy$$

Variational Formulation

For all elements K , and for all $\varphi \in C_\infty(K)$:

$$\int_{\partial K} T \varphi \mathbf{v} \cdot \mathbf{n}_K ds - \int_K T \mathbf{v} \cdot \nabla \varphi \, dx dy = \int_K \varphi \, dx dy$$

Variational Formulation

For all elements K , and for all $\varphi_h \in V_h$:

$$\int_{\partial K} T_h \varphi_h \mathbf{v} \cdot \mathbf{n}_K ds - \int_K T_h \mathbf{v} \cdot \nabla \varphi_h dx dy = \int_K \varphi_h dx dy$$

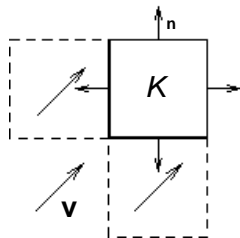
Variational Formulation

For all elements K , and for all $\varphi_h \in V_h$:

$$\int_{\partial K} \hat{f}(T_h, T_h^{\text{ext}}, \mathbf{v} \cdot \mathbf{n}_K) \varphi_h ds - \int_K T_h \mathbf{v} \cdot \nabla \varphi_h dx dy = \int_K \varphi_h dx dy$$

Numerical Flux Function

- The numerical flux function depends only on the values of T_h at the discontinuities




The numerical flux function:

$$\hat{f}(T_h, T_h^{ext}, \mathbf{v} \cdot \mathbf{n}_K) = T_h \max(\mathbf{v} \cdot \mathbf{n}_K, 0) + T_h^{ext} \min(\mathbf{v} \cdot \mathbf{n}_K, 0)$$

Solution Procedure

$$\int_{\partial K} \hat{f}(T_h, T_h^{\text{ext}}, \mathbf{v} \cdot \mathbf{n}_K) \varphi_h ds - \int_K T_h \mathbf{v} \cdot \nabla \varphi_h dx dy = \int_K \varphi_h dx dy$$


$$F_K(T) - R_K T_K = B_K$$

Solution Procedure

- The upwind flux can be written

$$F_K(T) = F_K^+ T_K + F_K^- T_{\Omega \setminus K},$$

where F_K^+ approximates the flux out of each element and F_K^- the flux entering from neighbour elements

- The system may then be written as

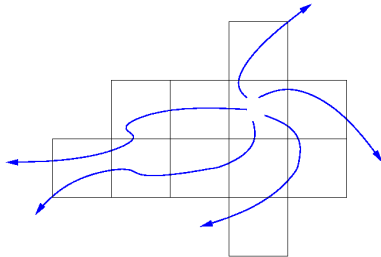
$$F_K^+ T_K - R_K T_K = B_K - F_K^- T_{\Omega \setminus K}$$

Reordering

- An elementwise solution is possible by exploiting the causality of the equation
- This sequence can be computed before solving the resulting system (using a depth-first search)
- Reduction in runtime:

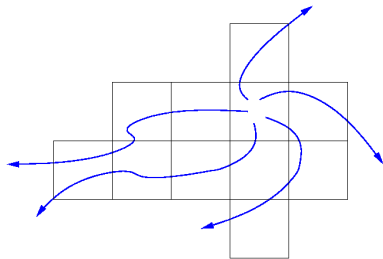
$Nm \times Nm$ system \longrightarrow N systems of size $m \times m$

Elementwise solution

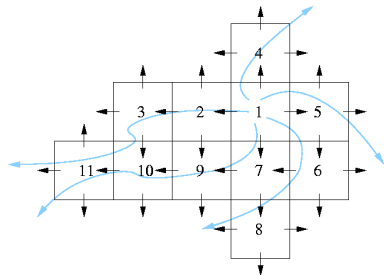


A few grid cells and
streamlines...

Elementwise solution



A few grid cells and
streamlines...



and the corresponding fluxes
and a possible sequence of
operations

L_2 -errors and convergence rates

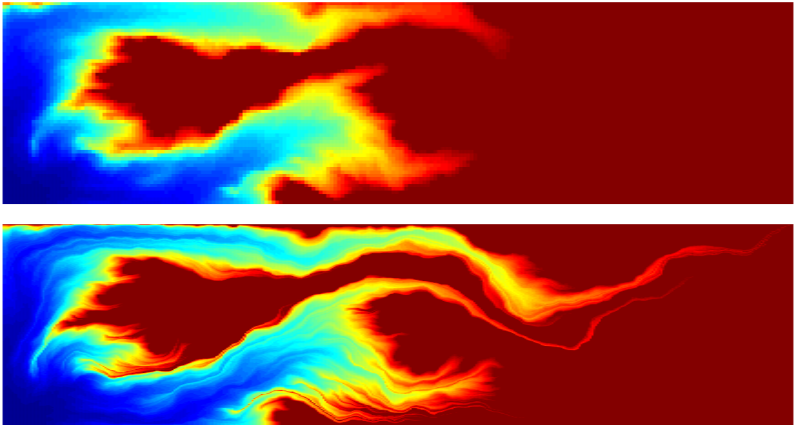
Ex: Linear rotation, $\mathbf{v} = (y, -x)$:

Table: L_2 -errors and the convergence rates in a smooth domain.

N	1. order		2. order		3. order		4. order	
10	3.36e-03		3.13e-05		1.74e-07		2.77e-09	
20	1.52e-03	1.15	7.42e-06	2.08	2.24e-08	2.96	1.45e-10	4.25
40	8.01e-04	0.92	1.95e-06	1.93	2.90e-09	2.95	9.58e-12	3.92
80	4.14e-04	0.95	5.02e-07	1.96	3.69e-10	2.97	6.22e-13	3.94
160	2.05e-04	1.01	1.25e-07	2.01	4.60e-11	3.01	3.84e-14	4.02
320	1.02e-04	1.01	3.10e-08	2.01	5.73e-12	3.00	2.39e-15	4.01

Top Layer in SPE 10

$$n = 1$$

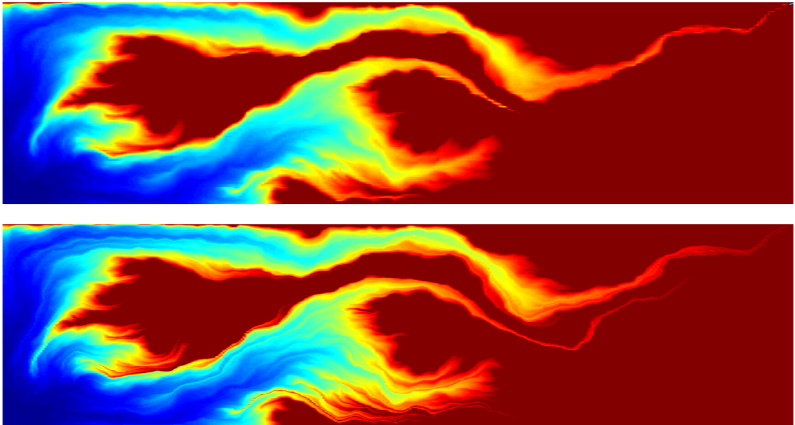


Comparison of DGM with a reference solution



Top Layer in SPE 10

$$n = 2$$

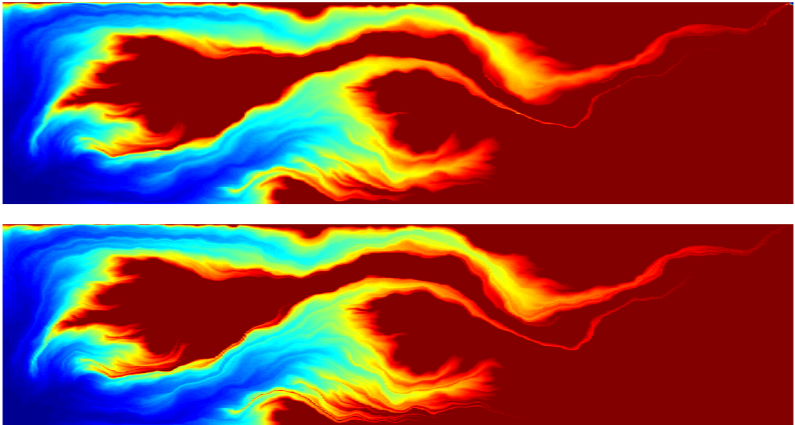


Comparison of DGM with a reference solution



Top Layer in SPE 10

$$n = 3$$

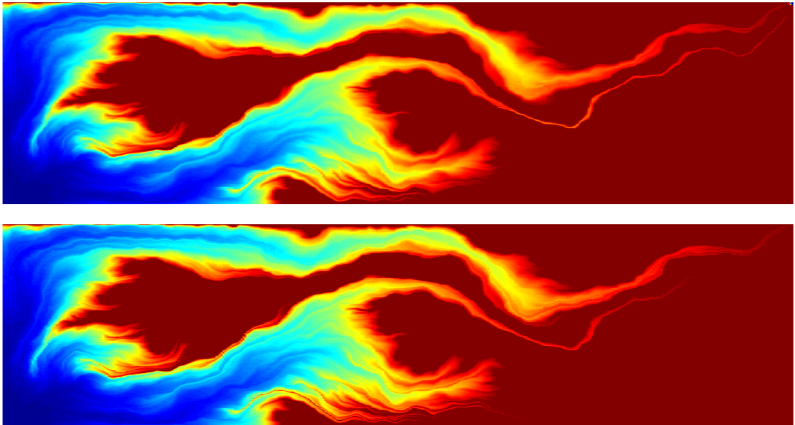


Comparison of DGM with a reference solution



Top Layer in SPE 10

$$n = 4$$

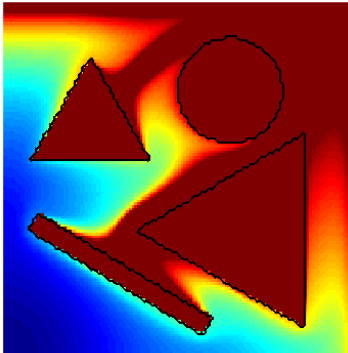


Comparison of DGM with a reference solution

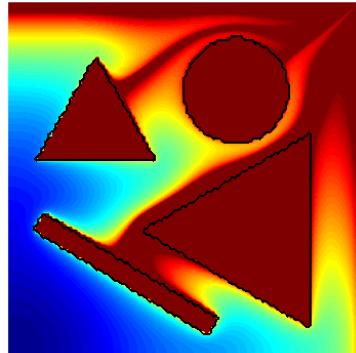


Flow Around Strong Discontinuities

$$n = 1$$



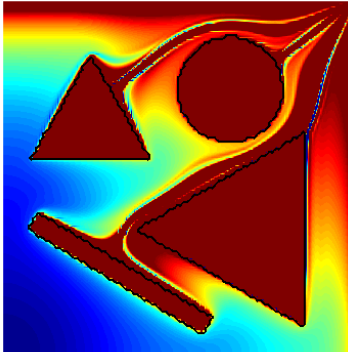
TOF using DGM



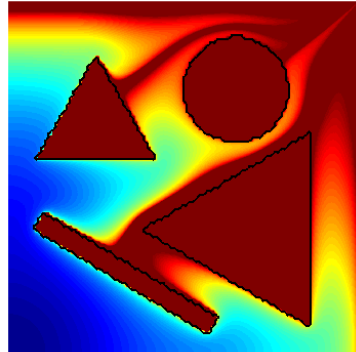
Reference solution

Flow Around Strong Discontinuities

$$n = 2$$



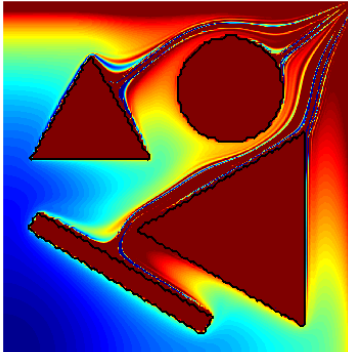
TOF using DGM



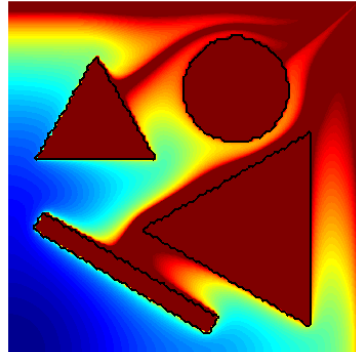
Reference solution

Flow Around Strong Discontinuities

$$n = 3$$



TOF using DGM



Reference solution

Tracer Flow

Linear transport equation:

$$\partial_t \mathbf{c} + \nabla \cdot (\mathbf{v}\mathbf{c}) = 0$$

Tracer Flow

Stationary distribution of tracers:

$$\nabla \cdot (\mathbf{vc}) = 0$$

Tracer Flow

Stationary distribution of tracers:

$$c \nabla \cdot \mathbf{v} + \mathbf{v} \cdot \nabla c = 0$$

Tracer Flow

Stationary distribution of tracers:

$$\mathbf{v} \cdot \nabla c = 0$$

Tracer Flow

Stationary distribution of tracers:

$$\mathbf{v} \cdot \nabla c = 0$$

Time-of-flight equation:

$$\mathbf{v} \cdot \nabla T = 1$$

Tracer Flow

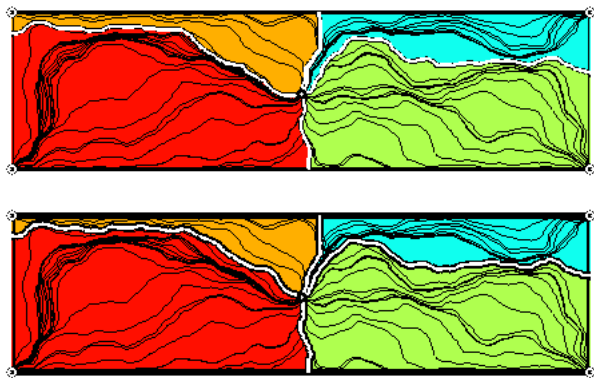
Stationary distribution of tracers:

$$\mathbf{v} \cdot \nabla c = 0$$

The linear equations for element K are

$$F_K^+ C_{i,K} - R_K C_{i,K} = -F_K^- C_{i,\Omega \setminus K}, \quad i = 1, \dots, n$$

Top layer in SPE 10



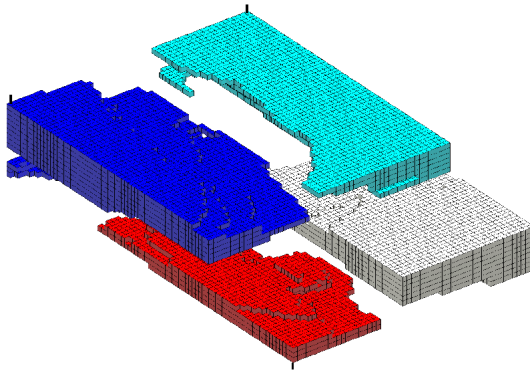
Comparison of the approximate tracer distribution using 1. and 5. order DGM

Top layer in SPE 10



Order 1 - Piecewise constant polynomials

3D: 15 layers of SPE 10



Implicit DG Solution

- Consider flow of two or more phases

$$S_t + \nabla \cdot (\mathbf{v}F(S)) = 0$$

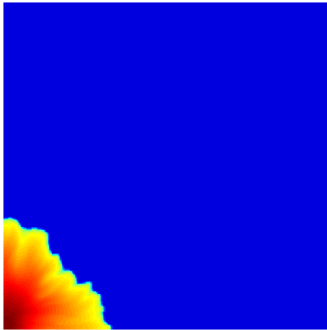
where F has positive characteristics

- Using product rule and semi-discretization

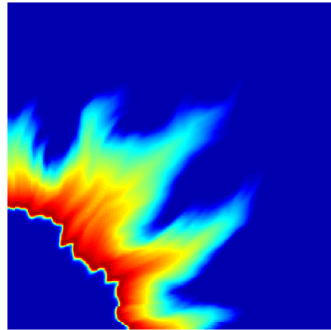
$$S^{n+1} + \Delta t \mathbf{v} \cdot \nabla F(S^{n+1}) = S^n - \Delta t F(S^n) \nabla \cdot \mathbf{v}$$

- Discretization by DGM
- Reordering as for $\mathbf{v} \cdot \nabla T = 1 \longrightarrow$ elementwise solution of N *nonlinear* $m \times m$ systems
- For large models: reordered dG + domain decomposition

WAG Injection (3-Phase Flow)



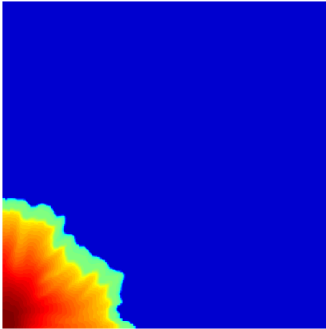
Water ($t = 0.075$)



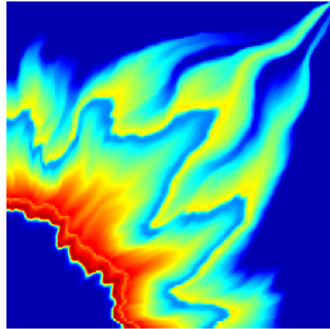
Gas ($t = 0.075$)

2nd order dG method with minmod postprocessing

WAG Injection (3-Phase Flow)



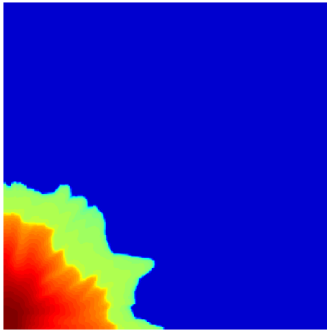
Water ($t = 0.125$)



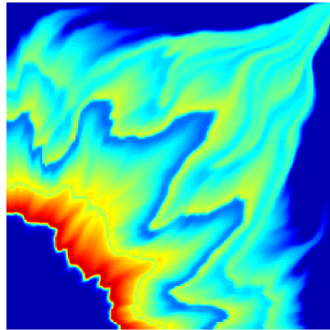
Gas ($t = 0.125$)

2nd order dG method with minmod postprocessing

WAG Injection (3-Phase Flow)



Water ($t = 0.175$)



Gas ($t = 0.175$)

2nd order dG method with minmod postprocessing

Summary

Summary

- Higher-order discontinuous Galerkin methods are implemented
- Fast elementwise solution strategy
- Runtime of the methods are $\mathcal{O}(N)$ for N unknowns
- Effective approximation of stationary tracer distribution
- Promising results for multiphase flow