

Wind turbine rotors in surge motion:
Relevance of the returning wake effect for large-scale FOWT

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Motivation:

Are there unsteady contributions to the aerodynamic loads of FOWT?

If yes: Do we need to enhance our simulation models?

- Recent simulation study on surging rotors revealed
 - ➔ **strong unsteady contributions** at high motion frequencies
 - ➔ **returning wake effect** becomes relevant

Next step: Check practical relevance of returning wake effect and other unsteady phenomena for a large scale FOWT rotor

Preprint



Wind Energy Science

Wind turbine rotors in surge motion: New insights into unsteady aerodynamics of FOWT from experiments and simulations

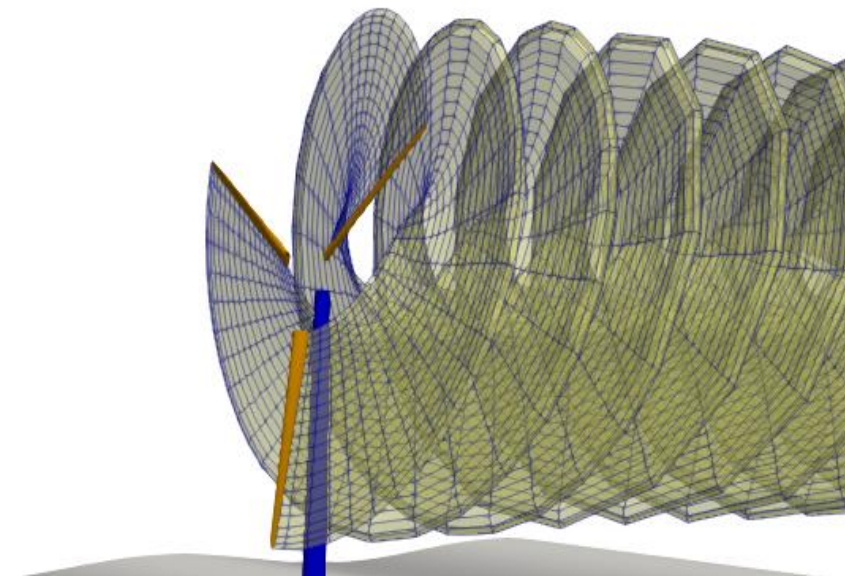
Christian W. Schulz, Stefan Netzband, Umut Özinan, Po Wen Cheng, and Moustafa Abdel-Maksoud

Abstract. An accurate prediction of the unsteady loads acting on floating offshore wind turbines (FOWT) under consideration of wave excitation is crucial for a resource-efficient turbine design. Despite a considerable number of simulation studies in this area,



Relevance of the returning wake effect for large-scale FOWT

- 1 Unsteady phenomena
 - Unsteady airfoil and dynamic wake effect
 - Returning wake effect
- 2 Simulation methods
- 3 Results: IEA 15MW in surge motion
 - Thrust force amplitude
 - Analysis of three unsteady regions
 - Appearance at wave frequency
- 4 Conclusion



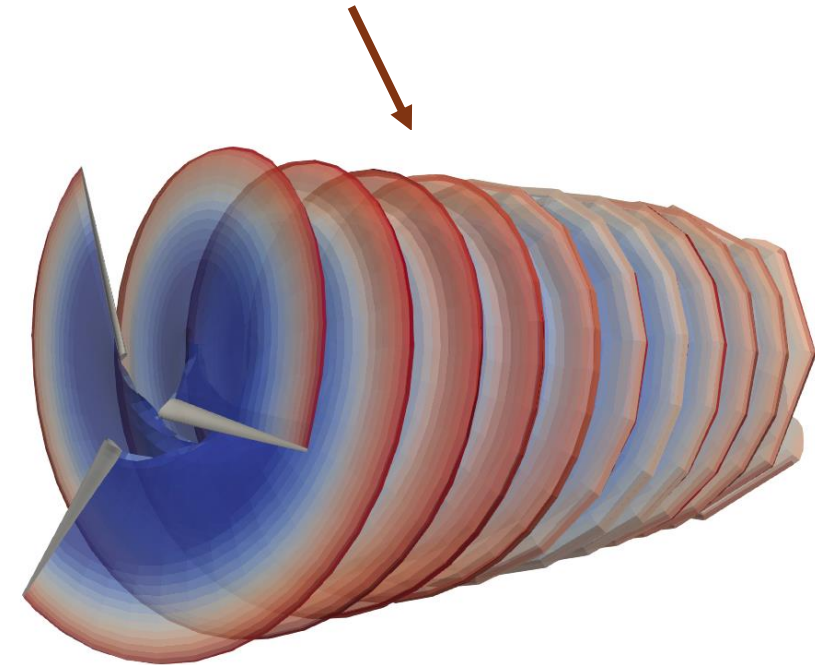
Relevant unsteady phenomena for surging wind turbines

Dynamic wake effect

- Also called dynamic inflow effect
- Changes of **the inflow situation in the past** act on **actual** induced velocity
- Only **gradual** changes of axial induced velocity
- **Low pass filter** effect
- Characterised by **rotor reduced frequency**

$$f_r = \frac{f D}{v_0}$$

Change of vortex strength and wake convection velocity



Equation: Schepers, 2012

Relevant unsteady phenomena for surging wind turbines

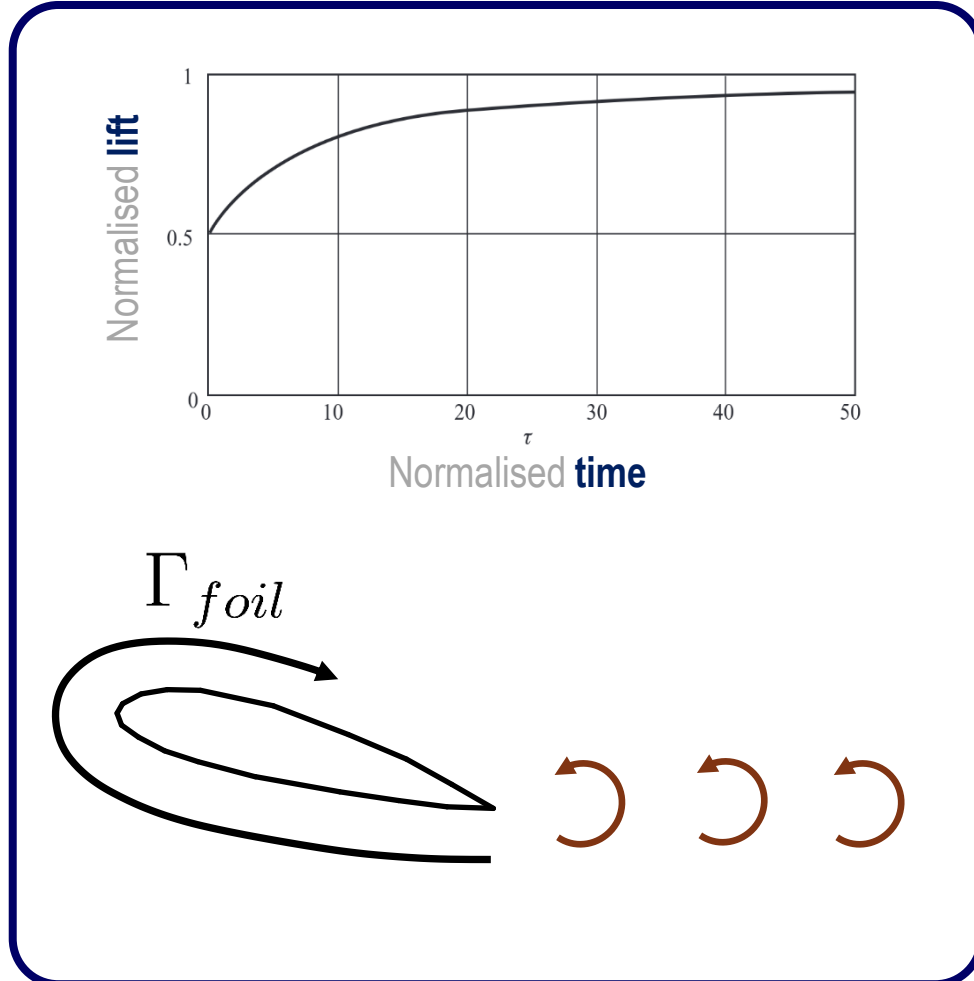


Figure: Burton et al., 2011

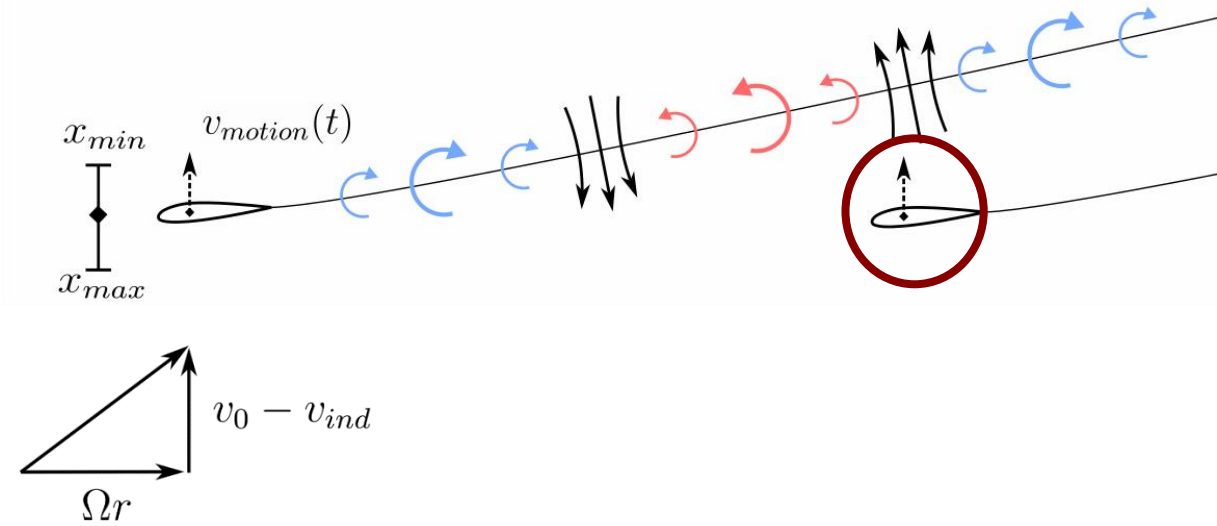
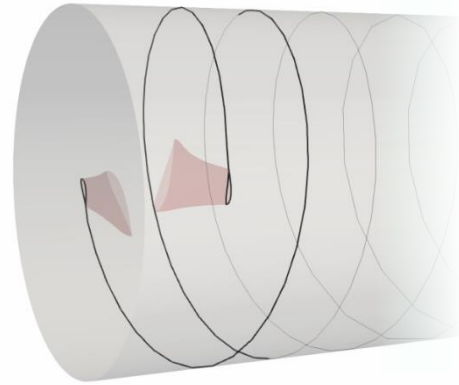
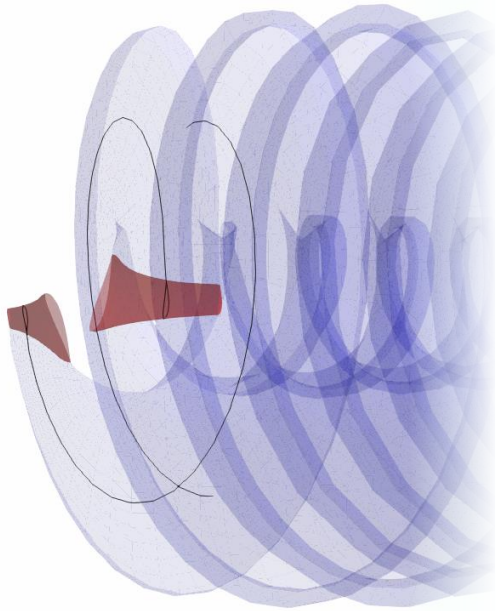
Unsteady airfoil effect (Theodorsen)

- **Attached flow**
 - **2D** thin airfoil theory
 - **Circulatory** / vortex shedding
 - Leads to **delayed response of lift** force (exponential)
- Characterised by **airfoil reduced frequency**

$$f_a = \frac{\pi f c(r)}{\sqrt{v_0^2 + (r\Omega)^2}}$$

- Dynamic stall: Minor relevance in this case

Relevant unsteady phenomena for surging wind turbines:
Returning wake effect



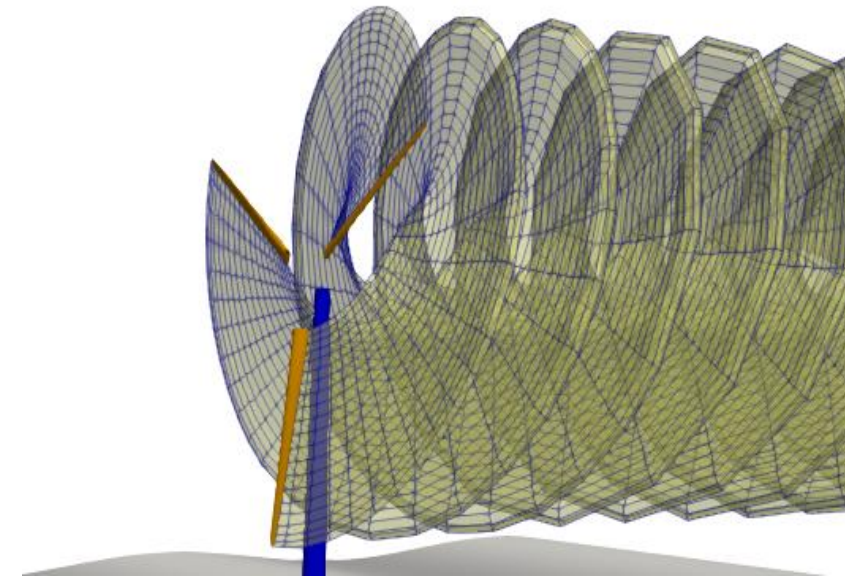
- Known from **helicopter aerodynamics**
- **Maximum** influence on loads when surge frequency equals **3P frequency**

- Characterised by

$$q_b = \frac{2\pi f}{n_b \Omega}$$

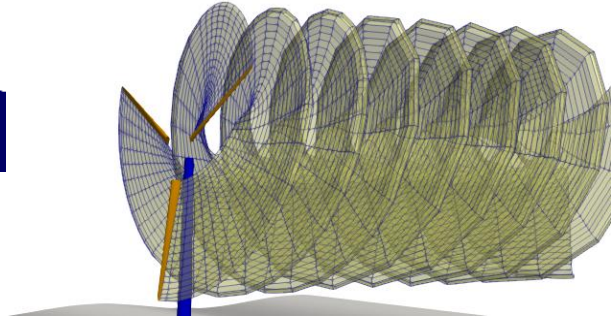
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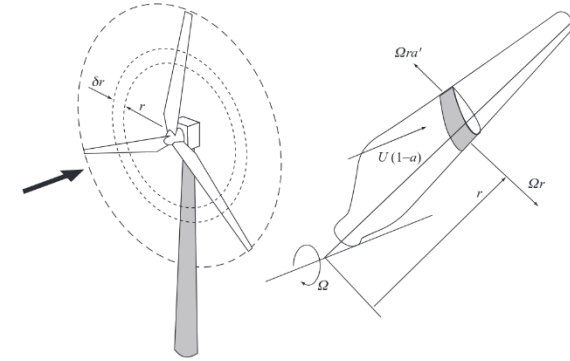
Simulation methods

panMARE



- Blade replaced by **vortex line**
- **3D, unsteady wake** representation
- Lift and drag forces from empirical coefficients
- **Unsteady effects** modelled:
 - Circulatory UA effect, dynamic inflow effect, **returning wake effect**

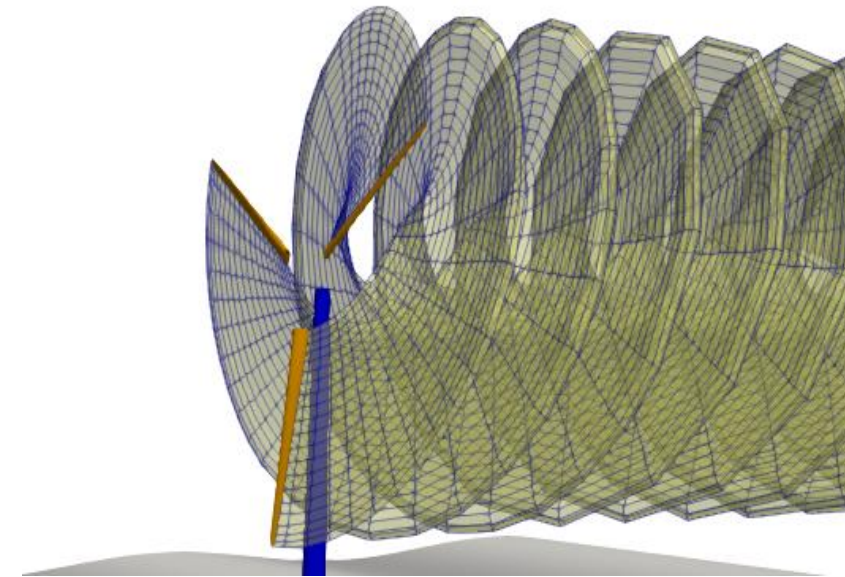
AeroDyn
OpenFAST



- **Blade Element Momentum Theory (BEM)**
- Unsteady corrections
 - **Dynamic inflow**
 - **Unsteady airfoil** correction (Leishman-Beddoes model)
 - Dynamic stall
- **No correction for returning wake effect**

Relevance of the returning wake effect for large-scale FOWT

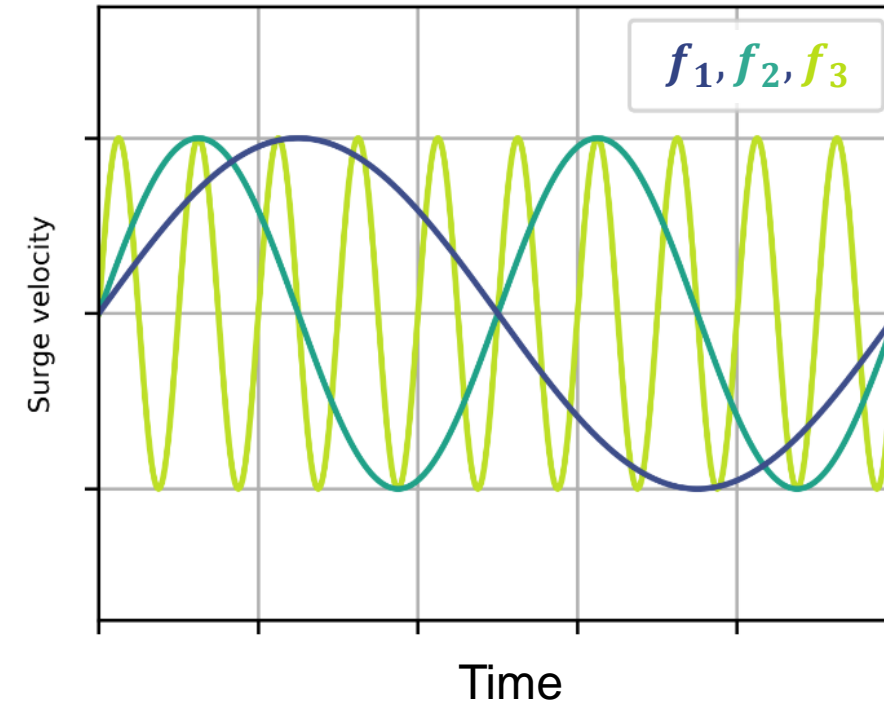
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Simulation scenarios for the identification of unsteadiness during surge motion

Definition of scenarios

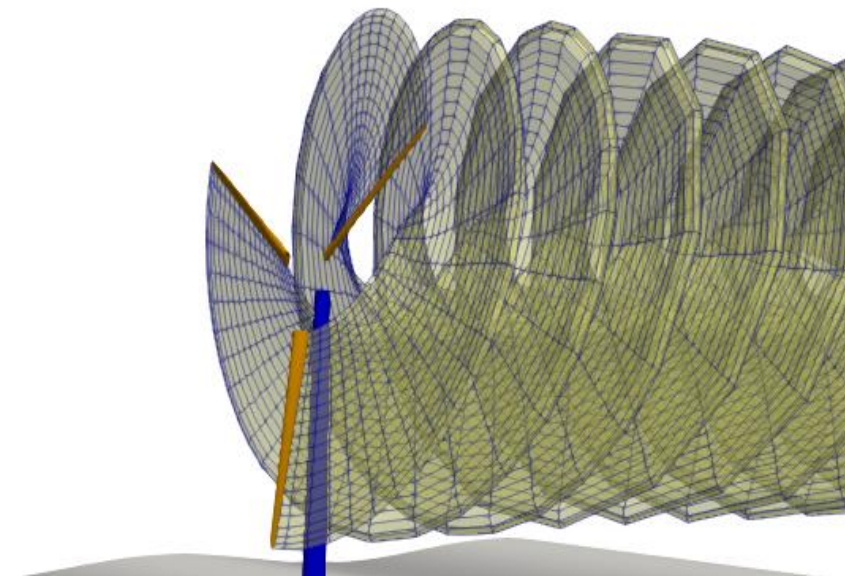
- Basic idea:
 - Load case set from **very low to very high motion periods**
 - **Same variation of TSR** for all cases
 - ➔ **Same result for all load cases** in case of **no unsteady contribution**
- Surge motion:
 - **Constant surge velocity amplitude**
 - Constant rotational speed and wind speed



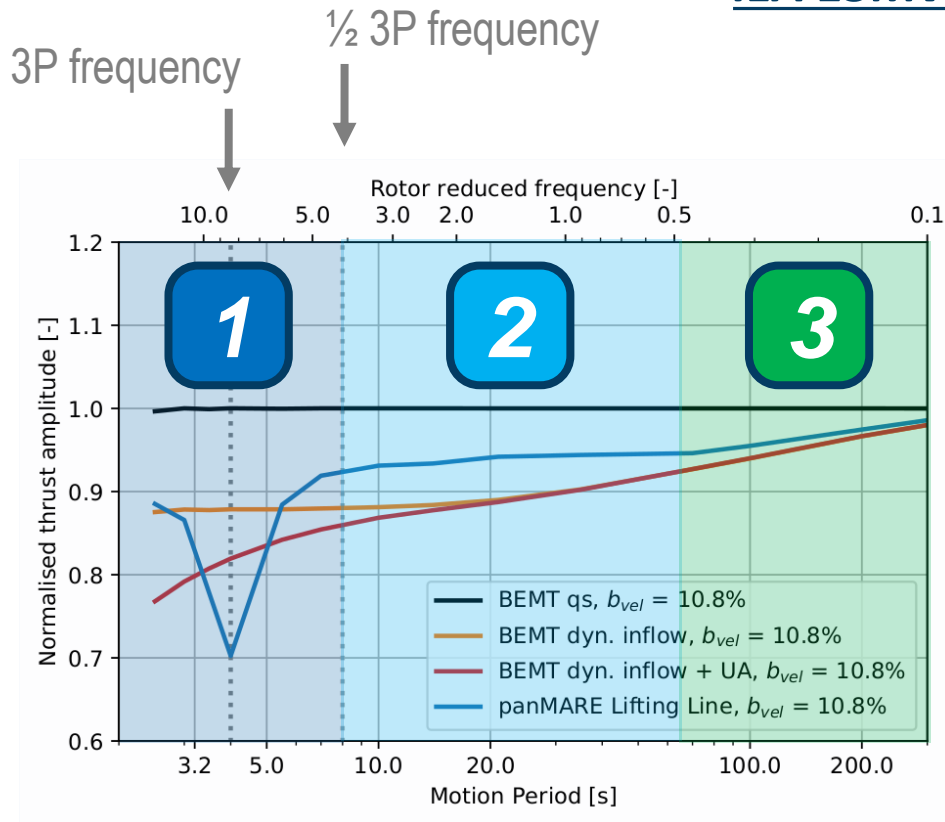
Surge motion velocity
Periods: approx. 3 up to 300 s

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IEA 15MW in surge motion: Rotor thrust amplitude



Fast

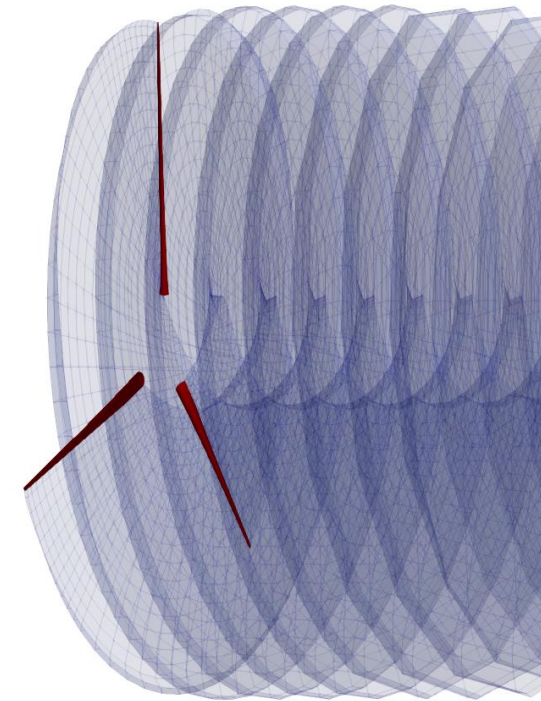


Slow

Rotor thrust amplitude

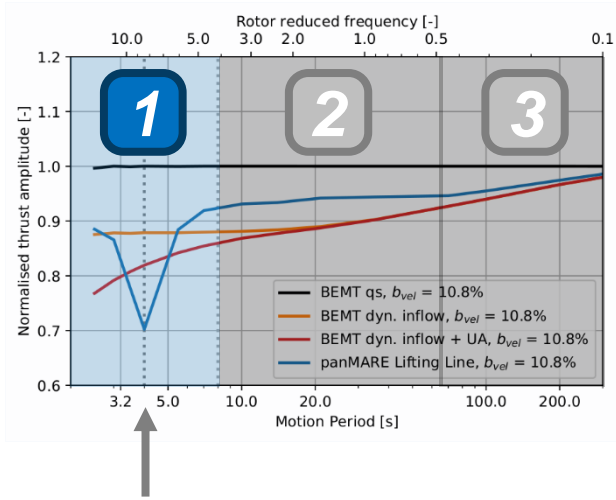
(@ 7 m/s uniform wind)

- Thrust normalised to case with highest period
- Plotted over motion period (log scale)
- OpenFAST BEMT simulations
 - Quasi-steady
 - Dynamic inflow correction
 - Dynamic inflow + unsteady airfoil corrections
- Quasi-steady model acts quasi-steady
- Significant unsteady contributions
- Analysis of unsteady regions



Simulation setup:

LL elements:	24
Wake panels:	14,400
Min. blade radius:	$r/R = 0.04$
Wake length:	4 D



3P frequency

IEA 15MW in surge motion: Unsteady region 1

Unsteady effects in region 1 (up to 8s)

- Minimum @ motion frequency = 3P
- Returning wake effect
- Not modelled in BEMT
- Findings from 2D simulations at $r/R = 0.64$

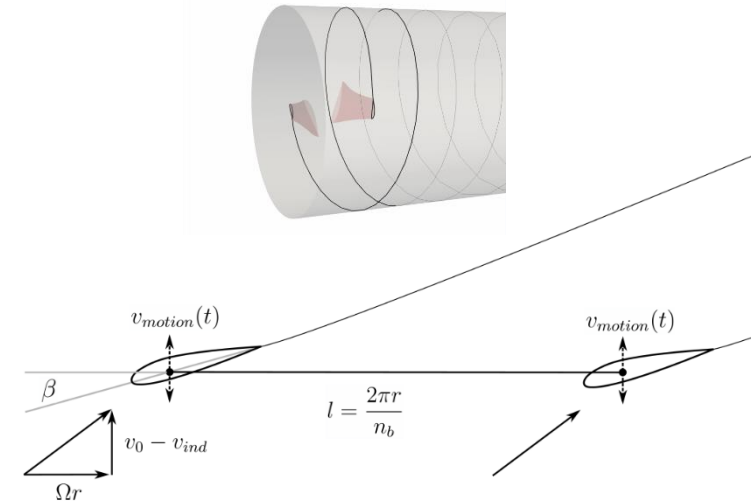
- Unsteady airfoil effect is prerequisite

$$f_a > 0.02$$

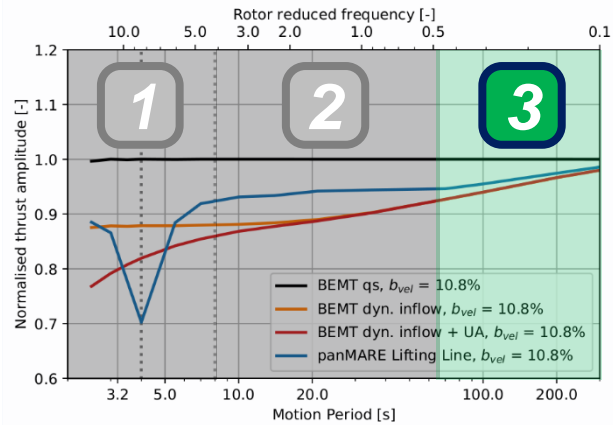
- Strong influence of returning wake effect when

$$q_b = \frac{2\pi f}{n_b \Omega} \quad q_b > 0.25 \dots 0.5$$

- Contribution of returning wake effect at periods lower than 20s



IEA 15MW in surge motion: Unsteady region 3

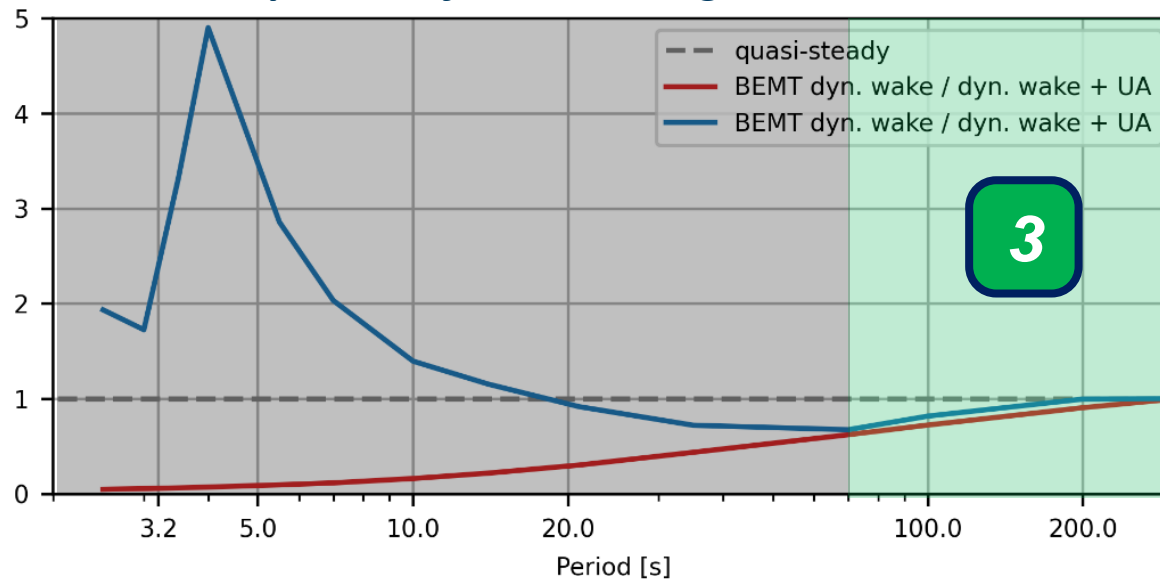


Unsteady effects in region 3 (70 to 300s)

- Both methods: **gradual decrease** of thrust amplitude
- Amplitude of axial induction
 - Normalised to quasi-steady case
 - Regions 1 and 2 **not comparable between LL and BEMT**
 - **Low pass filter** effect in both methods
 - Dominated by **dynamic wake effect**

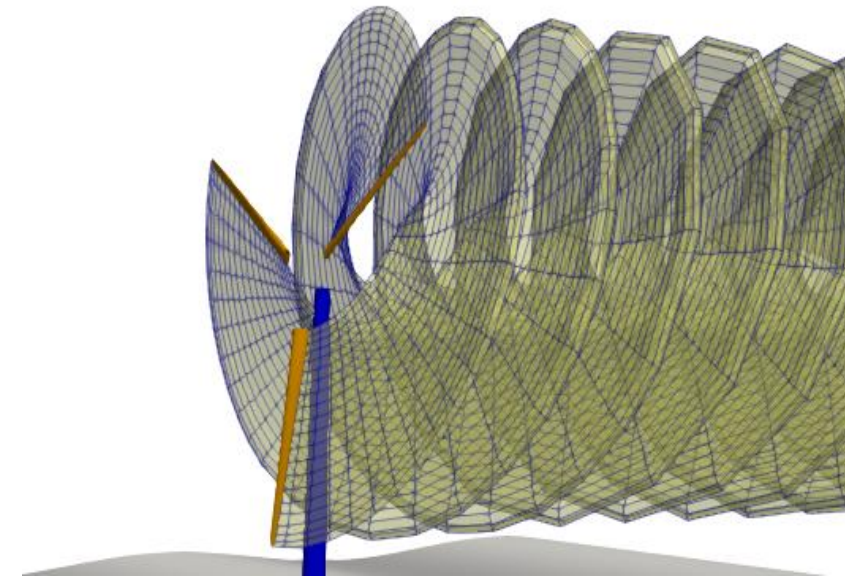
$$f_r > 0.1 \dots ?$$

Amplitude of rotor averaged axial induction



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Realistic wave periods

Gulf of Maine

		Tp (s)								
		1<Tp<2	2<Tp<3	3<Tp<4	4<Tp<5	5<Tp<6	6<Tp<7	7<Tp<9	9<Tp<11	Tp>11
Significant Wave Height [m]	<1	0,03%	4,69%	7,29%	7,02%	3,91%	5,91%	13,49%	6,27%	0,08%
	1< Hs <2		0,00%	0,92%	6,64%	6,85%	7,32%	7,90%	8,36%	0,16%
	2< Hs <3			0,00%	0,09%	0,55%	2,71%	2,91%	3,31%	0,15%
	3< Hs <4				0,00%	0,01%	0,12%	1,11%	1,04%	0,08%
	4< Hs <5						0,00%	0,19%	0,47%	0,04%
	5< Hs <6							0,02%	0,21%	0,01%
	6< Hs <7								0,08%	0,01%
	7< Hs <8								0,02%	0,01%
	Hs >8								0,00%	0,00%

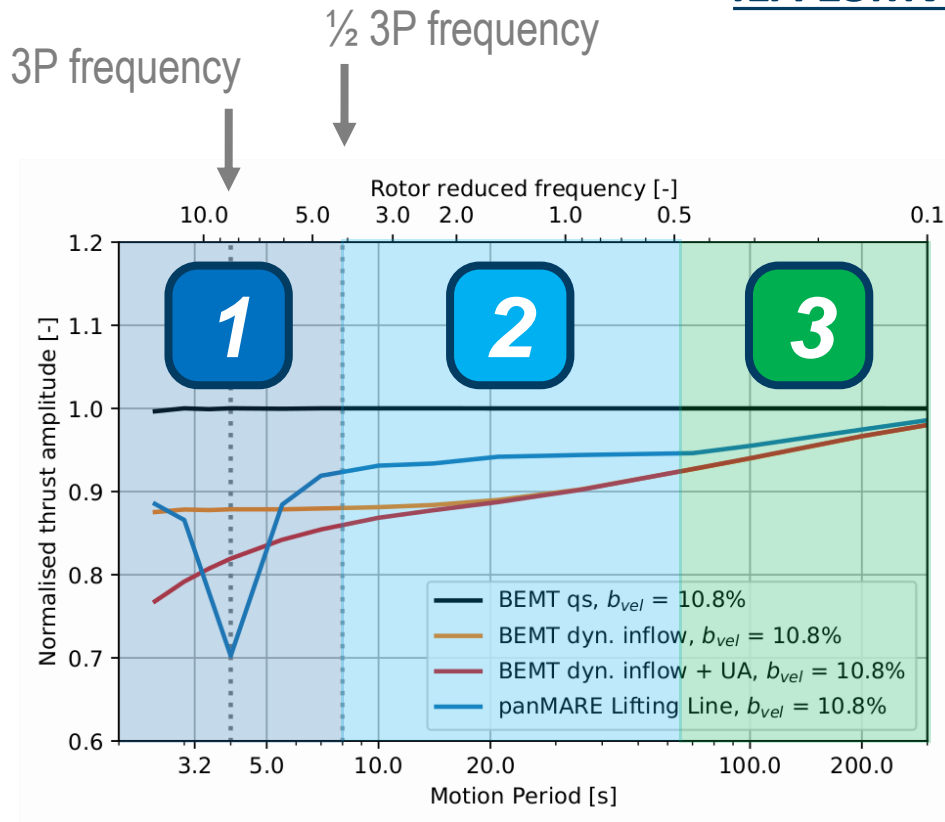
1*

Table 26: GoM significant wave height-peak period distribution

* for 7 m/s wind speed

Source: Lifes50+ Report, Deliverable 1.1 Oceanographic and meteorological conditions for the design

IEA 15MW in surge motion: Rotor thrust amplitude



Fast

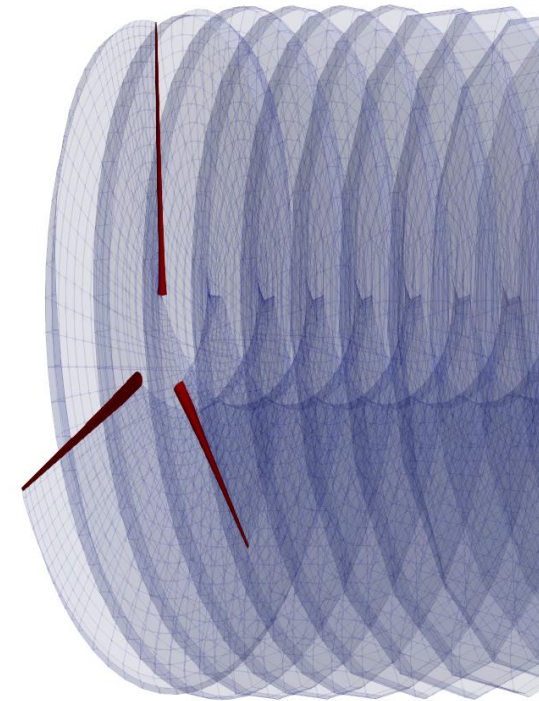


Slow

Rotor thrust amplitude

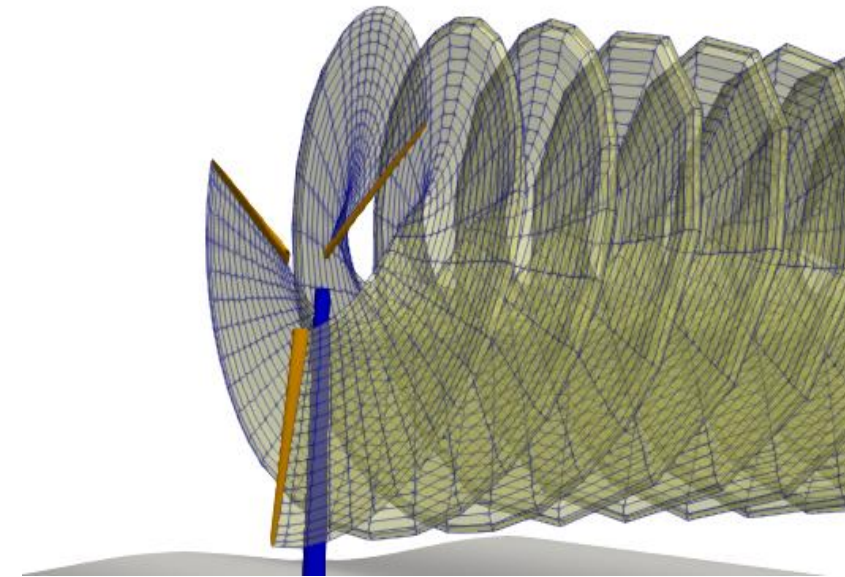
(@ 7 m/s uniform wind)

- **Returning wake effect is present at realistic wave periods!**
 - Especially at low wind speeds
 - Reduction of thrust amplitude of up to **25%**



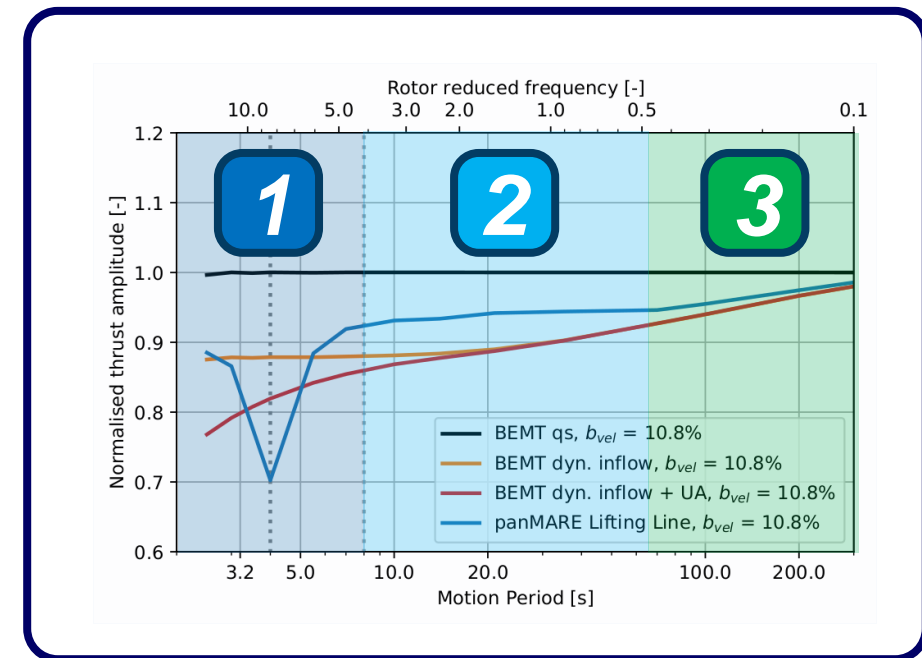
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Conclusions

- Unsteady contributions to rotor loads of the IEA 15 MW from
 - **Dynamic wake effect**
 - **Unsteady airfoil effect**
 - **Returning wake effect**
- Unsteady phenomena can be identified by interplay of
 - **Rotor reduced frequency**
 - **Airfoil reduced frequency**
 - **Ratio of motion and 3P frequency**
- Returning wake effect **occurs at realistic wave frequencies**
- **Simulation inaccuracies must be expected when using classical BEMT methods**

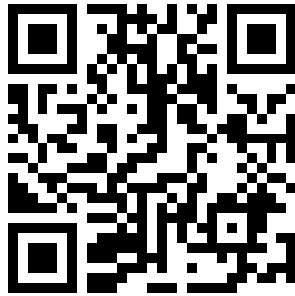


Related publications

Two related publications and
can be found at

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New publication follows in first half of 2024

Acknowledgements



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