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# Technical modeling challenges for large idling wind turbines

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## Introductions



### Introduction

#### Let's start by asking ourselves

- What do we understand about the aerodynamics under idling cases
- Do we really need to model dynamic stall?
- How sensitive is dynamic stall calculations using engineering model in idling conditions?
- How the aerodynamic damping influences the loads?



### Introduction

#### The danger of deep stall.....



## Aerodynamics of Deep Stall

- Massively separated flow which includes all complex characteristics
- Vortical structures interact and change the instationary loads



Figure 11: Trailing vortices in the inboard region of the blade illustrated by Q-Criterion colored by Y-vorticity [1/s]. The inboard vortex system becomes stronger with increasing wind speed, showing distinct counter-rotating trailing vortices which induces downwash.

## Aerodynamics of Deep Stall

Massively separated flow which
includes all complex characteristics

- Vortical structures interact and change the instationary loads
- Unsteady excitation from angle of attack variation leads to a phenomenon called dynamic stall
- There are strong vortex interactions on the airfoil (blade) surface. Two main vortices are the leading edge vortex (LEV) and trailing edge vortex (TEV)



Ouro et al, 2018

## Some facts and issues

- The accuracy of wind turbine load predictions is influenced by correct modeling/capturing of 3D and unsteady effects.
- Dynamic stall (DS) remains one of the most difficult cases for wind turbine aerodynamics.
- The flow field during DS is complex and its mechanisms are insufficiently understood.
- Existing dynamic stall models hardly provide reliable predictions concerning the higher harmonic effects
- Many dynamic stall models are developed only for lift coefficient, only limited number of them consider drag and pitching moment
- In idling conditions, engineering models often underestimate the true aerodynamic damping → causing stronger instabilities than the real situations

# Research Methodology





## **Simulation Strategy**

#### Turbine and test cases

- IEA 15 MW turbine
- Rotor diameter = 242 m
- Idling DLC 6.3 case
  - $\circ \overline{U} = 40 \text{ m/s}$
  - $\phi \psi = [-20^{\circ}, 0^{\circ}, +20^{\circ}]$
  - o  $TI_X = 11\%$ ,  $TI_Y = 8.8\%$ ,  $TI_Z = 5.5\%$



## **Simulation Strategy**

#### Turbine and test cases

- Simulated using a development version of Bladed
- A new dynamic stall model "IAG Model"<sup>1</sup> has been recently implemented in Bladed
- Studies were performed by changing the dynamic stall modeling
- Simulations were carried out by adopting Bladed BEM and Bladed Vortexline (free wake + lifting line) modules

[1] Bangga, G., Lutz, T. and Arnold, M., 2020. An improved second-order dynamic stall model for wind turbine airfoils. *Wind Energy Science*, *5*(3), pp.1037-1058.



# **Results and Discussion**



# Effects of shed vortex inductions

- Computed wind turbine loads and blade tip torsion rotational deflection using Vortexline are affected by unsteady models
- The shed vortex effect introduces aerodynamic damping which helps stabilizing the results
- Shed vortex effects are pronounced when no dynamic stall model is adopted



# Effects of shed vortex inductions

- Computed wind turbine loads and blade tip torsion rotational deflection using Vortexline are affected by unsteady models
- The shed vortex effect introduces aerodynamic damping which helps stabilizing the results
- Shed vortex effects are pronounced when no dynamic stall model is adopted
- This causes variations of the induced velocities seen by the blade sections, even under idling conditions



### Dynamic stall modeling influence



BEM + No DS

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BEM + BL Model

#### BEM + IAG Model





## Yaw angle influence

- Increasing/decreasing yaw angle highlights the importance of dynamic stall modeling
- Without modeling the dynamic stall effects, hub resultant moment amplitudes become unreasonably large → due to missing aerodynamic damping
- IAG model predicts the smallest amplitudes, highlighting the characteristics of the higher aerodynamic damping for the studied test cases



# **Conclusions and Remarks**



## **Conclusions and Remarks**

- Idling instability predictions depend on the unsteady aerodynamic modeling especially the inclusion of the dynamic stall model.
- Calculations without dynamic stall model yield massive instabilities which are unlikely to be physically correct.
- The IAG dynamic stall model predicts more reasonable instability level which can be helpful for the loads analysis.
- Vortexline calculations incorporate induction dynamics even for idling conditions which allows the induced velocity especially in tangential direction to vary.
- The dynamics of the induced velocities partially extracts the energy of the flow and increases the aerodynamic damping. This effect is more pronounced when the shed vortex effect is included.

#### More details are given in the paper when it is published!

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## Thank you!

#### \*now time for snacks questions

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