

Power performance comparison of unmoored floating offshore wind turbines and energy ships

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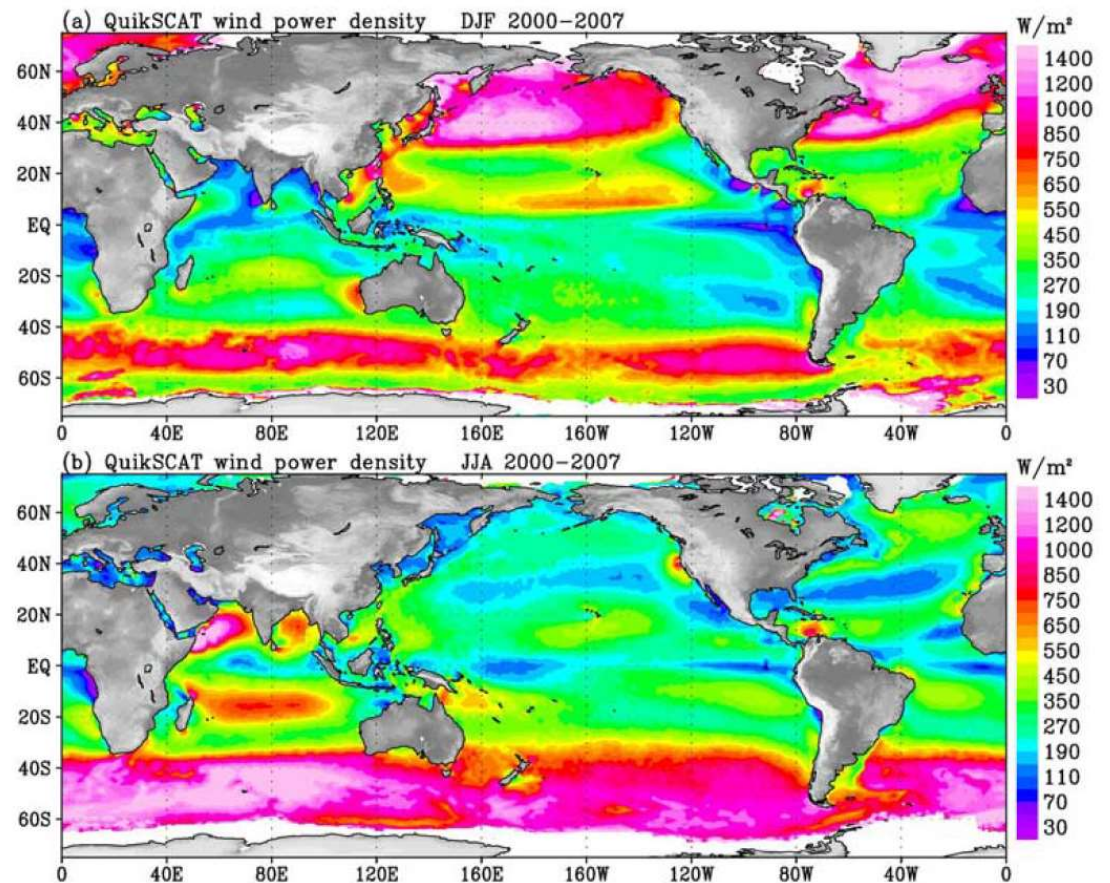
Overview

- Motivation and Background
- Research Questions
- Modelling Methodology
- Results and Discussion
- Conclusion

Motivation and Background

Far-offshore wind

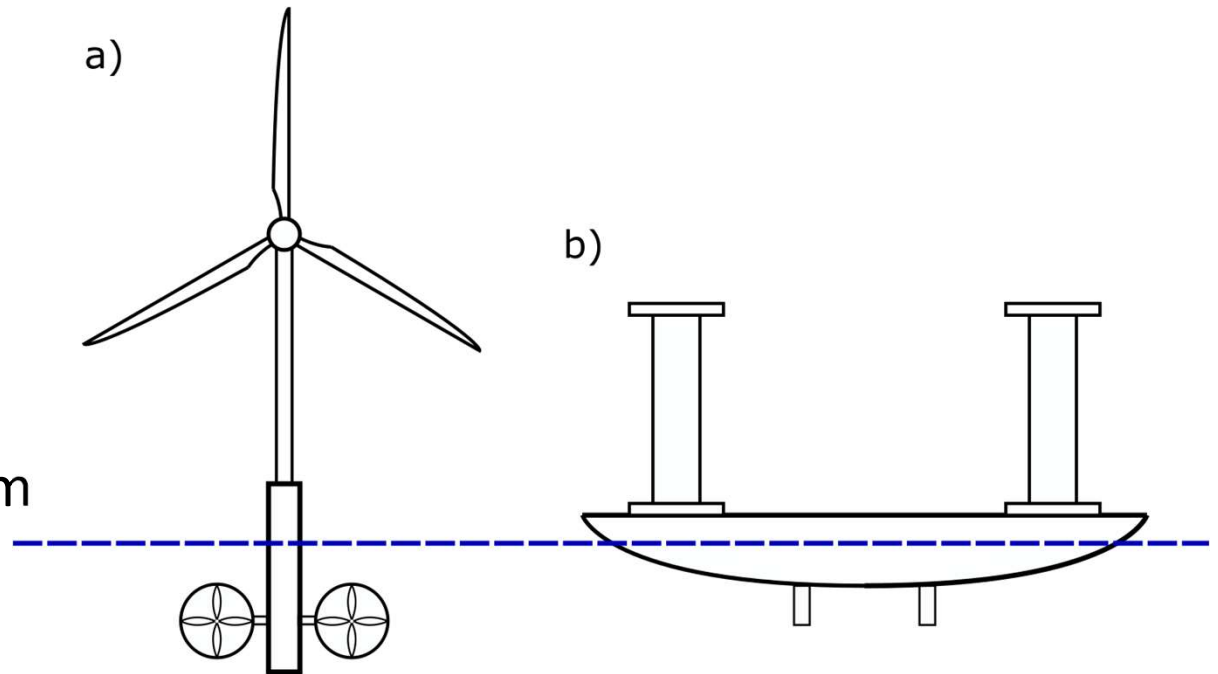
- Higher average wind speeds farther offshore
- Operating far-offshore means storing or using generated power
- Harsher met-ocean conditions
- Unknowns: O&M, Perception, legality



Global wind power density, [1] (Liu et al. 2008)

Technology concepts

- Two concepts:
 - a) Unmoored floating offshore wind turbine (UFOWT)
 - b) Energy ship
- Expressly designed for far-offshore operation
- Mobile, leads to problem of weather-routing
- Energy is used for synthesizing e-fuel or used directly (i.e DAC)



Research Questions

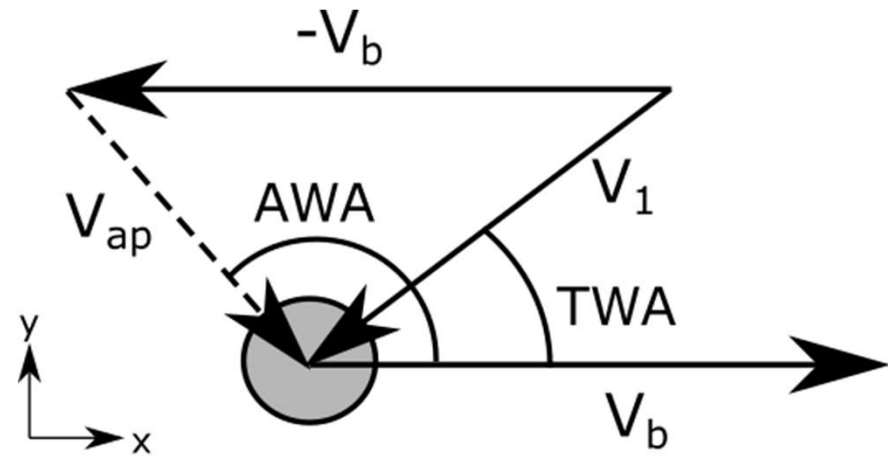
Questions

1. How does each concept (for a given design) perform at producing power under various environmental conditions?
2. How do the performance maps compare?

Modelling Methodology

Conventions

- V_1 - True wind velocity
- V_b – vessel/body velocity
- V_{ap} – Apparent wind velocity
- TWA – True wind angle
- AWA – Apparent wind angle



UFOWT (1)

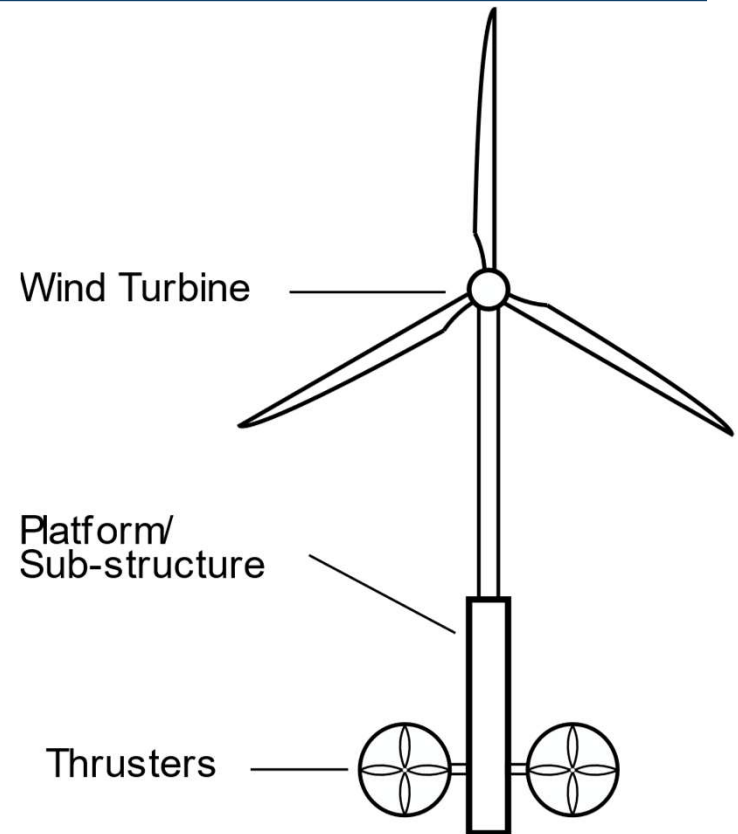
- 2D waterplane Steady-state model
($\sum \vec{F} = \vec{0}$)

- $\vec{F}_g = \left[\frac{1}{2} \rho_1 A_1 |V_{ap}|^2 C_{t1}(\beta, \lambda) - m_{rotor} g \sin(\theta_{tilt}) \right] [\cos(AWA) \hat{x}, \sin(AWA) \hat{y}]$
- $\vec{F}_p = -n_{wt} \rho_2 D_2^4 f^2 K_{t2}(J) [\cos(\theta) \hat{x}, \sin(\theta) \hat{y}]$
- $\vec{F}_{d2} = -\frac{1}{2} \rho_2 A_{d2} V_b |V_b| C_{d2} [1 \hat{x}, 0 \hat{y}]$

- Power

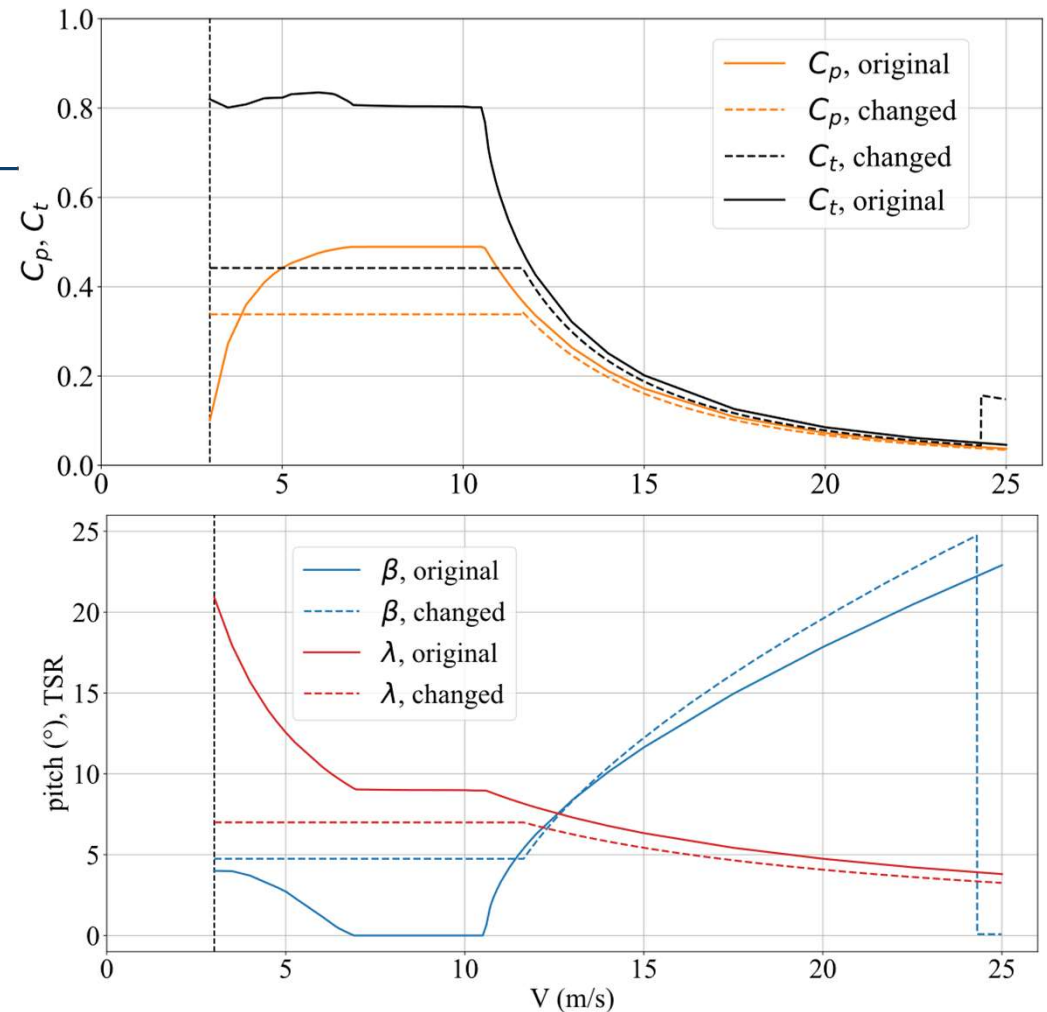
- $P_g = \frac{1}{2} \rho_1 A_1 V_{ap}^3 C_{p1}(\beta, \lambda)$
- $P_p = -2\pi n_{wt} \rho_2 D_2^5 f^3 K_{q2}(J)$
- $C_{p,net} = \frac{P_g + P_p}{P_1}$

- Note: No accounting for wave forces



UFOWT (2)

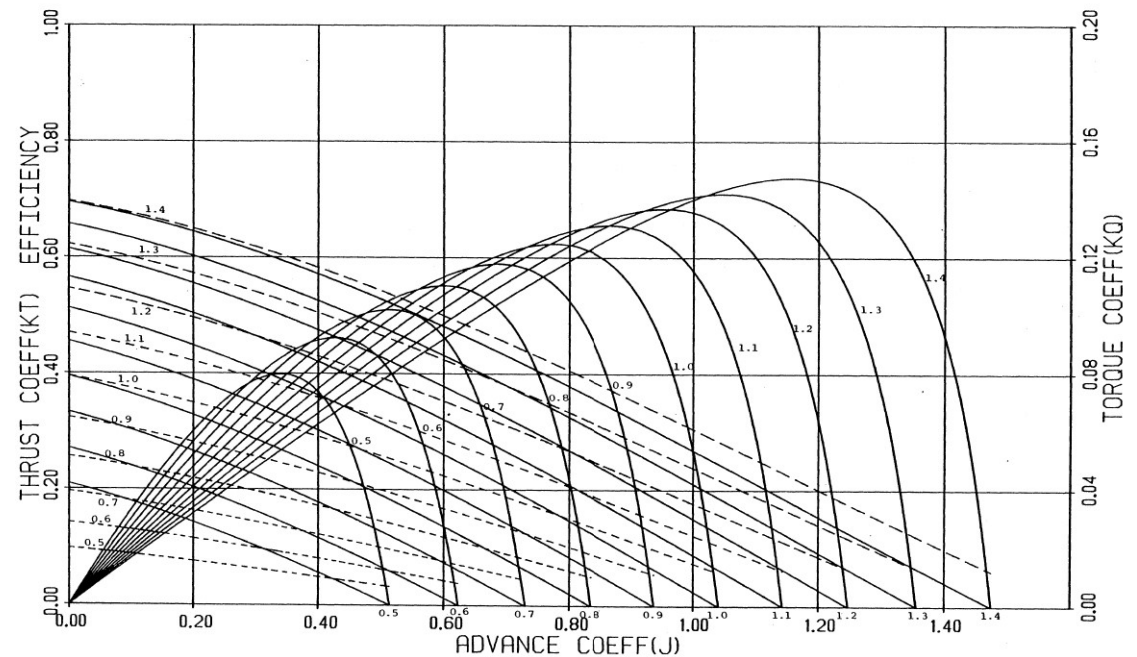
- Several control variables
 - β - Wind turbine blade pitch
 - λ - Wind turbine tip-speed ratio
 - θ - Thruster yaw angle
 - J - Thruster advance ratio
- Choose a new schedule (i.e $\beta(V_1)$) of (β, λ) to maximize $\frac{C_p}{C_t}$
- Solve for other variables analytically
- Design based on
 - IEA 15 MW reference turbine [2]
 - UMaine Voltorn platform [3]
 - Wageningen B-series, 7 bladed propeller [4]



Data from IEA 15 MW reference turbine [2] (Gaertner et al. 2020), denoted as "original"

UFOWT (3)

- Design based on
 - IEA 15 MW reference turbine [2]
 - Umaine Voltun platform [3]
 - Wageningen B-series, 7 bladed propeller [4]
- Design choices made for data availability, NOT optimality



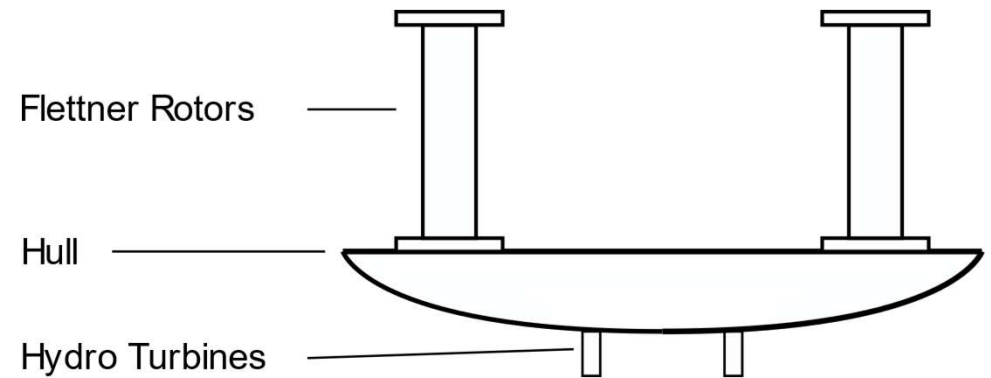
Energy Ship (1)

- Forces

- $\vec{F}_g = -2\rho_2 A_2 V_b |V_b| a(1-a)[1\hat{x}, 0\hat{y}]$
- $\vec{L} = \frac{1}{2}\rho_1 A_1 |V_{ap}^2| C_{lp}(\gamma)[\sin(AWA), \cos(AWA)]$
- $\vec{D} = \frac{1}{2}\rho_1 A_1 |V_{ap}^2| C_{dp}(\gamma)[- \cos(AWA), \sin(AWA)]$
- $\vec{F}_p = (\vec{L} + \vec{D})C_{t,int}$
- $\vec{F}_{d2} = -\frac{1}{2}\rho_2 A_{d2} V_b |V_b| C_{d2}(V_b)[1\hat{x}, 0\hat{y}]$

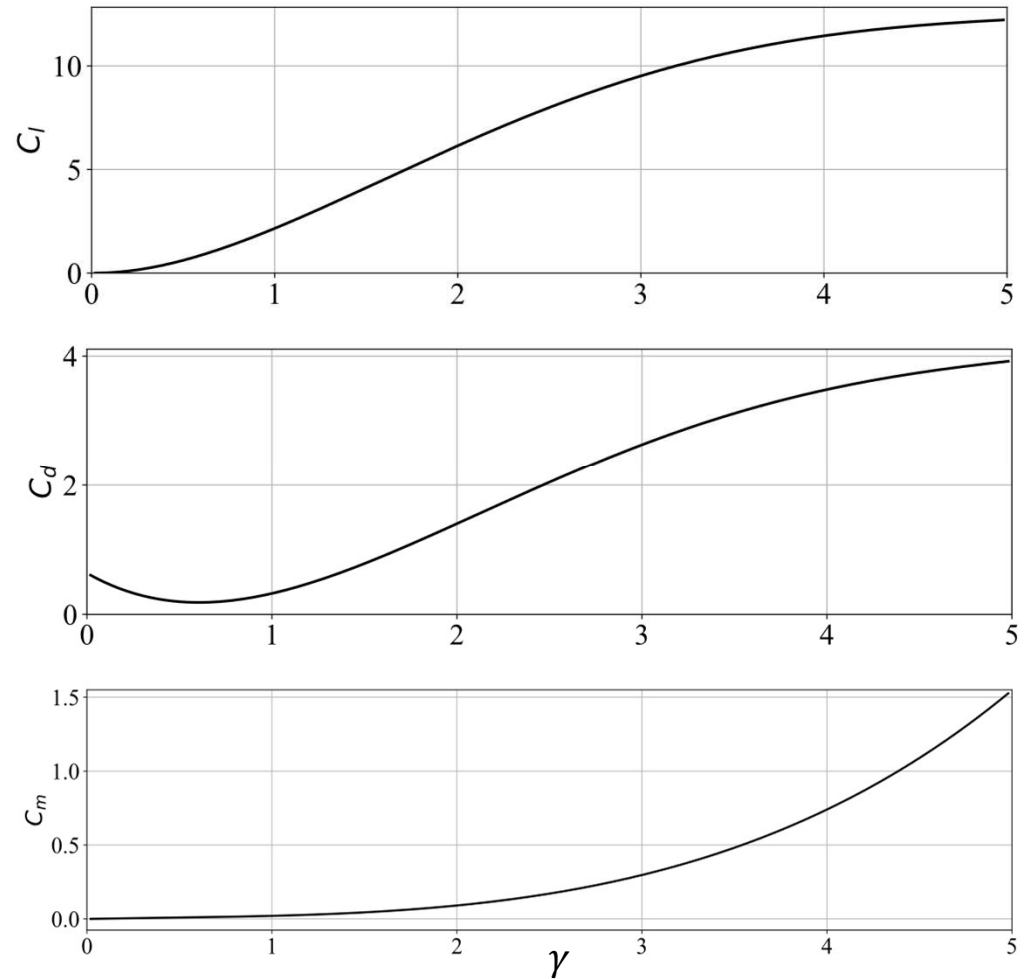
- Power

- $P_g = 2\rho_2 A_2 V_b^3 a(1-a)^2 \eta_g$
- $P_p = -\frac{1}{2}\rho_1 A_1 V_{ap}^3 C_m(\gamma)$
- $C_{p,net} = \frac{P_g + P_p}{P_1}$



Energy Ship (2)

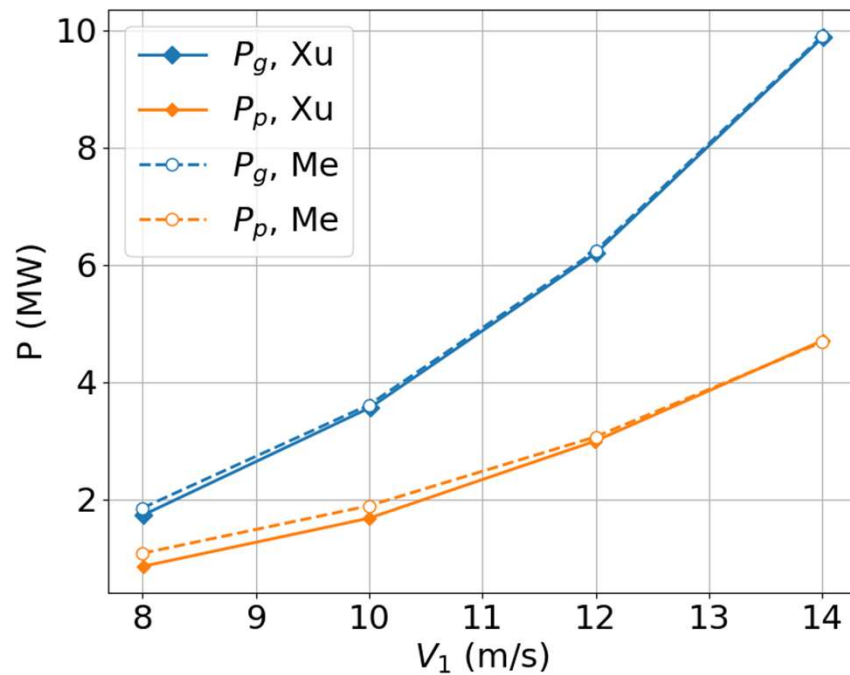
- Energy Ship Design based on FARWIND design [5]
 - 4x 35m tall Flettner rotors
 - 80m long catamaran hull
 - 2x 4m diameter water turbines
- Flettner rotor performance from empirical formulas [6]
- Use optimizer to choose control variables (γ , a , V_b)



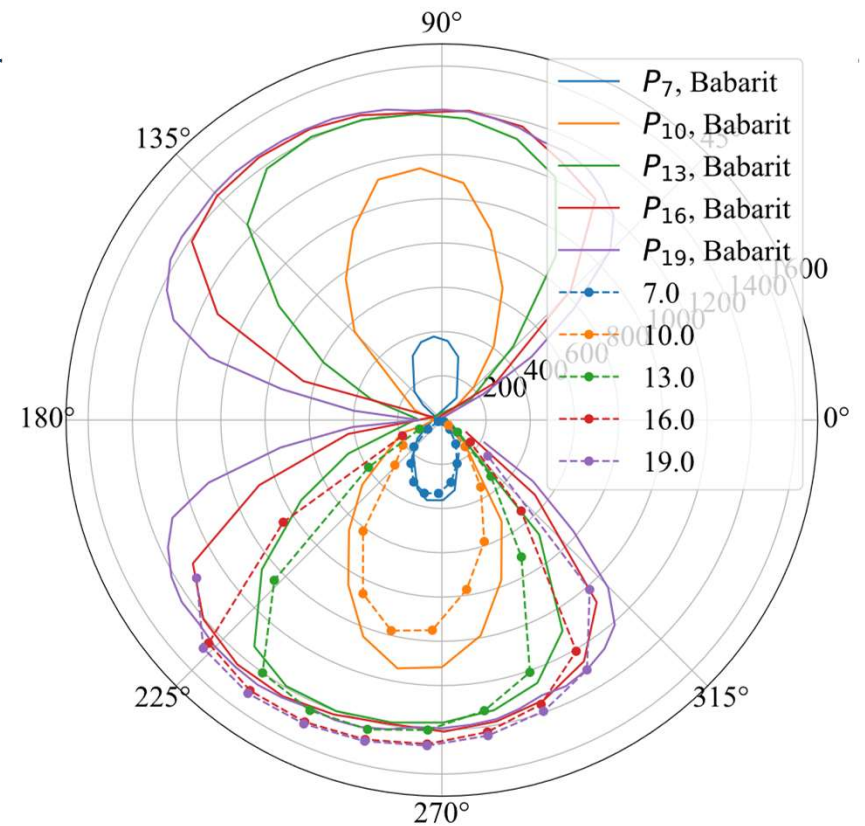
Flettner rotor performance curves [6]

Results and Discussion

Model Verification

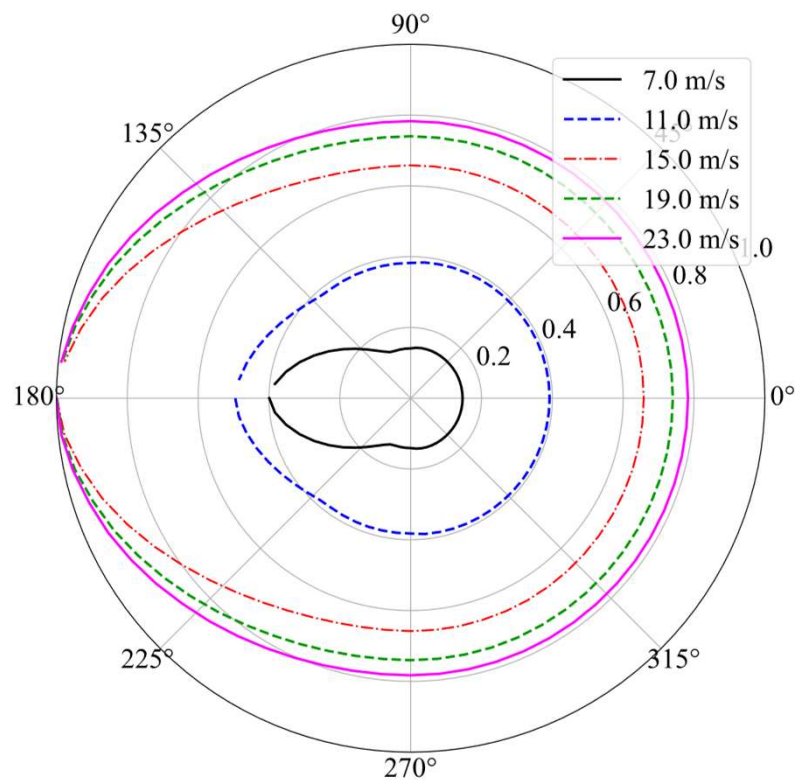


UFWOT Verification against [7] (Xu et al. 2021)

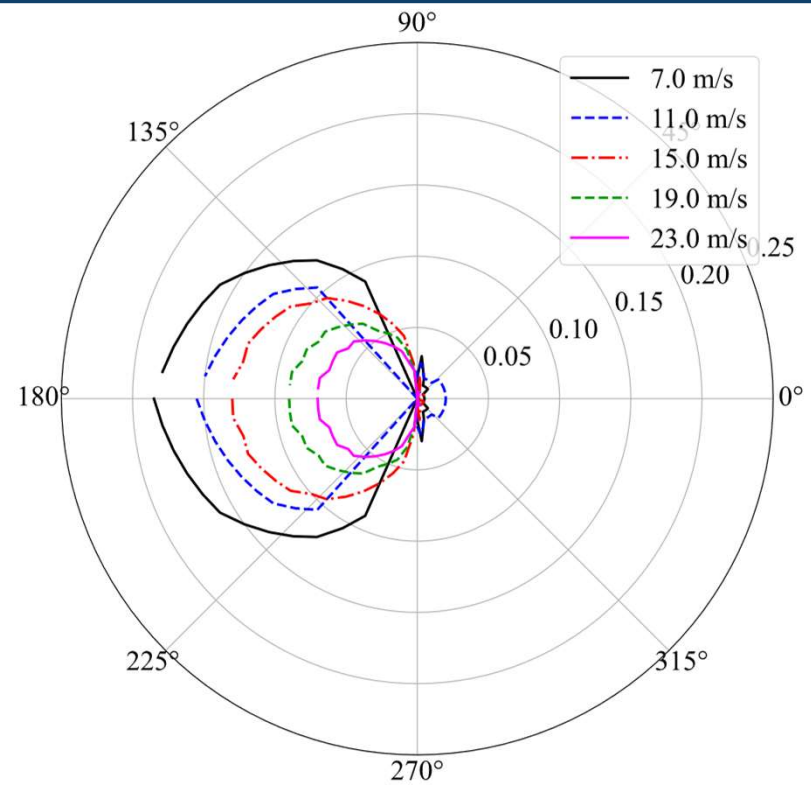


Energy Ship Verification against [5] (Babarit et al. 2021)

UFOWT Performance



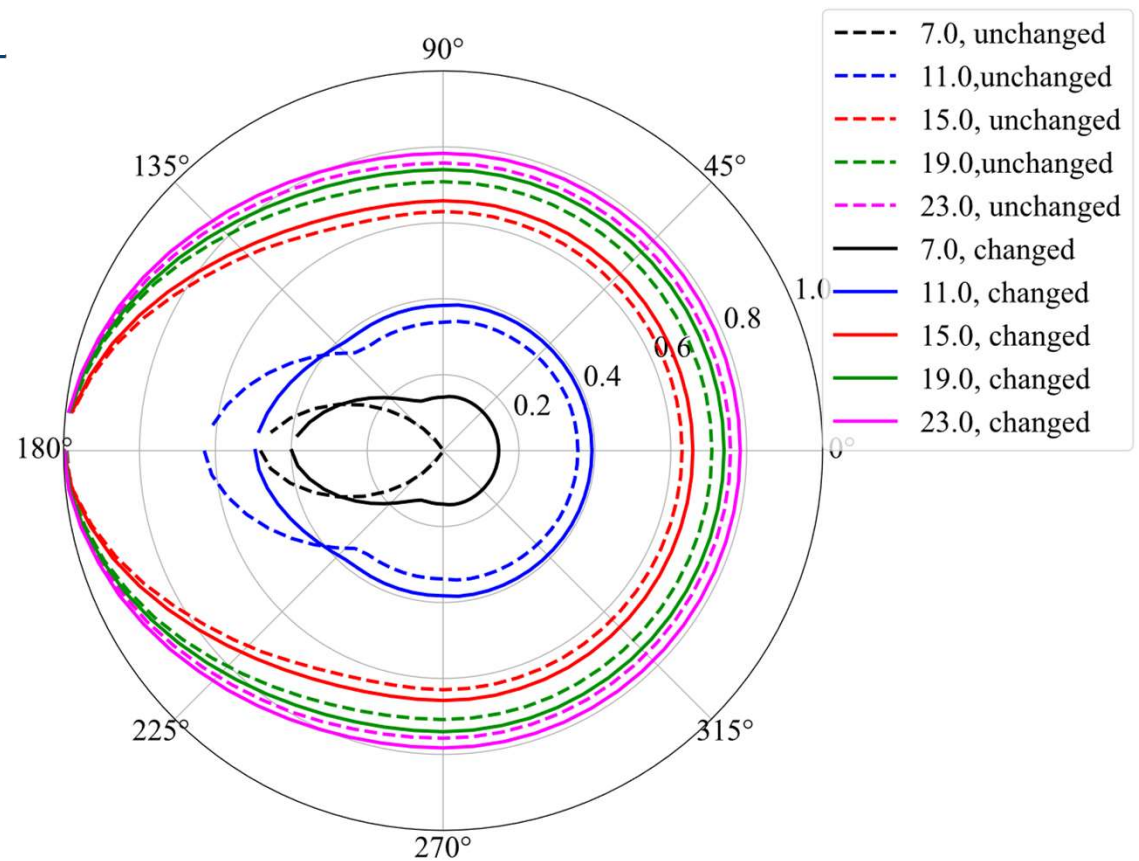
$C_{p,net}$ vs. TWA and V_1



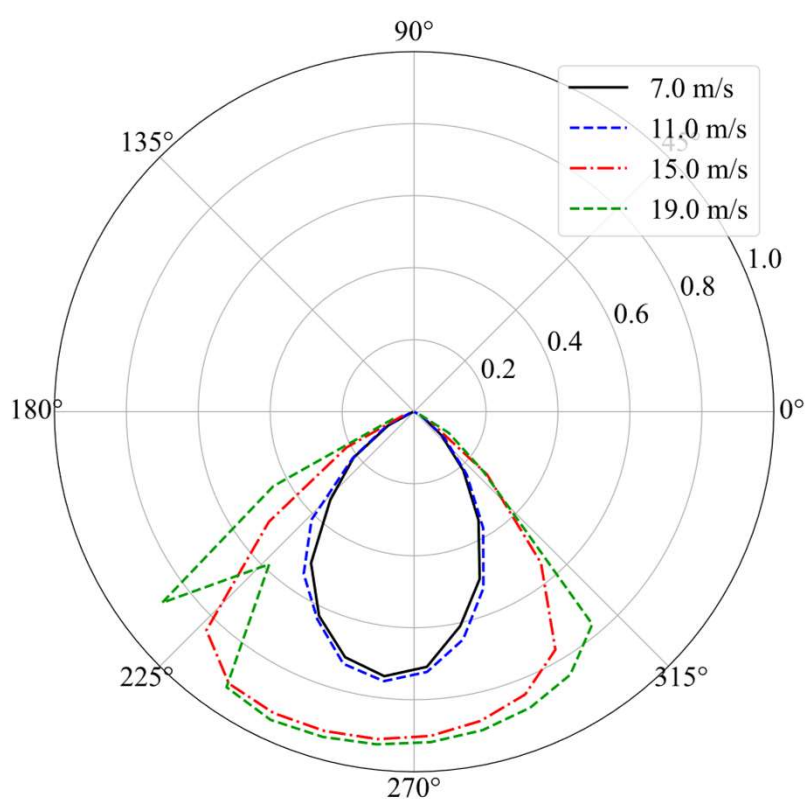
$V_{b,opt}$ (m/s) vs. TWA and V_1

UFOWT Control

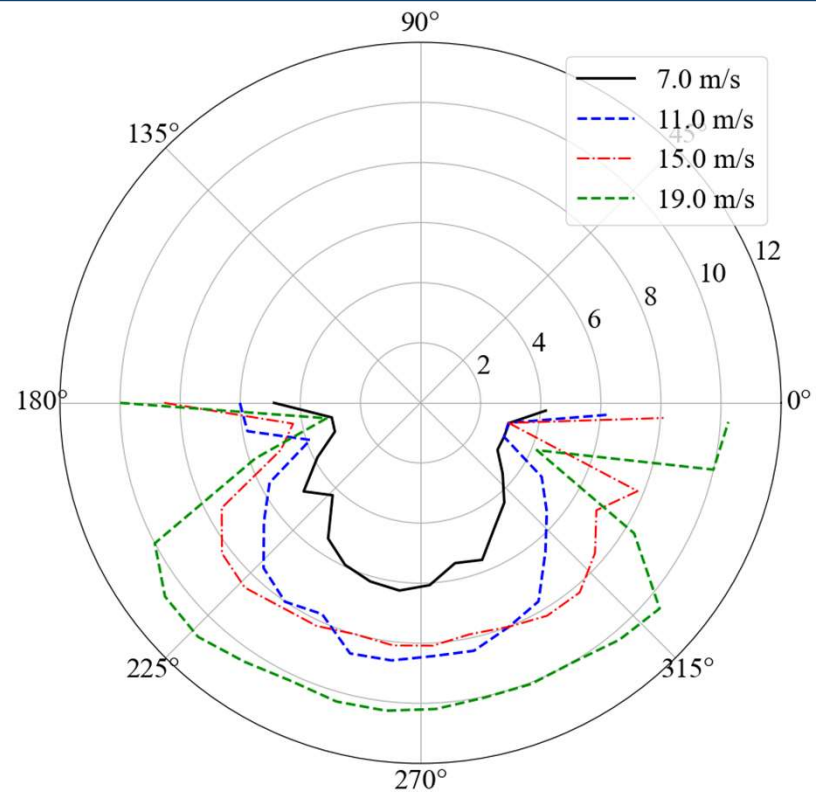
- Changing the C_p and the C_t map improves power performance for many cases
- However, better to use an optimization to find the best operating points



Energy Ship performance



$C_{p,net}$ vs. TWA and V_1

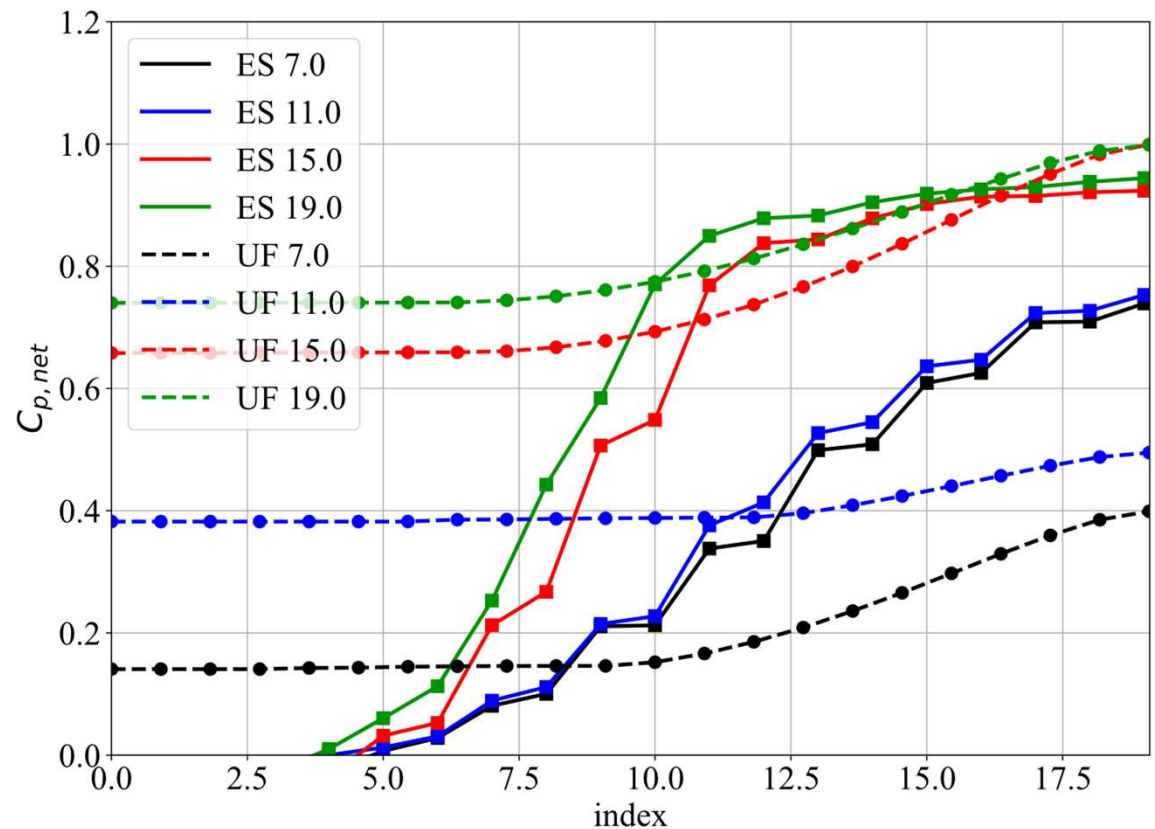


$V_{b,opt}$ vs. TWA and V_1

Note: performance is symmetric, one half plotted

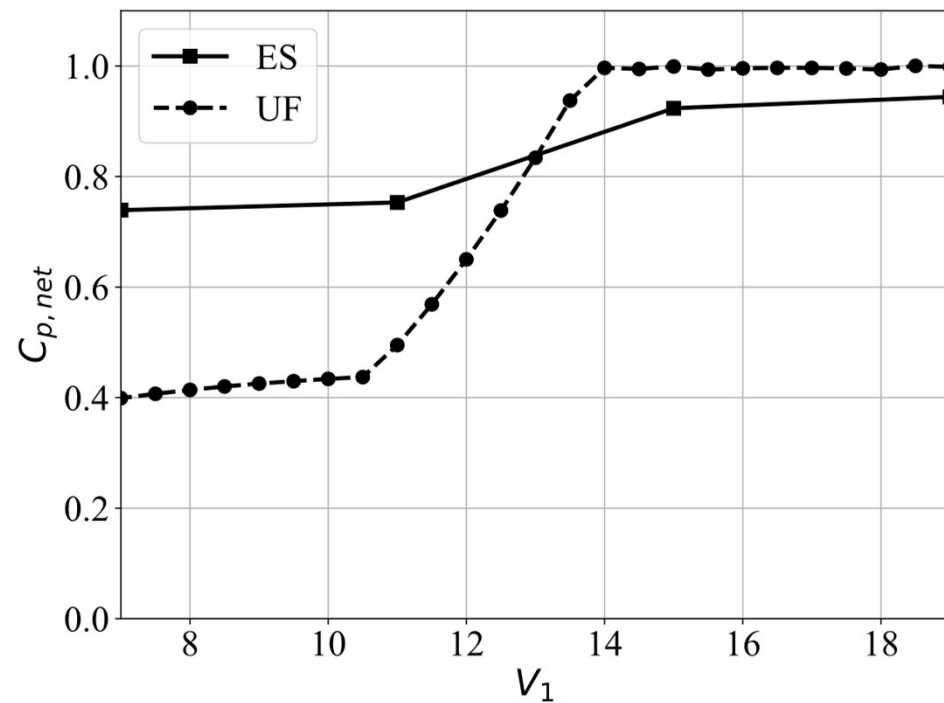
Comparison

- Power polars sorted for ascending $C_{p,net}$
- UFOWT performs better in best and worst cases
- Energy ship performs better in between



Comparison

- UFOWTs may perform better at very high wind speeds, but worse at low ones



Conclusion

Conclusions

- Developed models of two far-offshore wind energy systems
- These models can serve as the basis for further investigations
- More robust comparison is required, this requires design optimization and routing optimization
- Biggest differences are in optimal operating speeds. UFOWTs move slowly, energy ships move quickly

Future work

- Use the model for Design optimization and Optimization of control/operation
- Capital Cost estimates
- Routing → LCOE
- Account for other losses (i.e conversion efficiency, loading/unloading time, etc.)
- Dynamics
- Wind shear difference
- UFOWT hull design choices

References

- [1] W. T. Liu, W. Tang, and X. Xie, “Wind power distribution over the ocean,” *Geophys. Res. Lett.*, vol. 35, no. 13, 2008, doi: 10.1029/2008GL034172.
- [2] E. Gaertner *et al.*, “IEA Wind TCP Task 37: Definition of the IEA 15-Megawatt Offshore Reference Wind Turbine,” NREL, Technical Report NREL/TP-5000-75698, 2020. Accessed: Sep. 20, 2021. [Online]. Available: <https://www.nrel.gov/docs/fy20osti/75698.pdf>
- [3] C. Allen *et al.*, “Definition of the UMaine VoltturnUS-S Reference Platform Developed for the IEA Wind 15-Megawatt Offshore Reference Wind Turbine,” NREL/TP-5000-76773, 1660012, MainId:9434, Jul. 2020. doi: 10.2172/1660012.
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- [6] F. Tillig and J. W. Ringsberg, “Design, operation and analysis of wind-assisted cargo ships,” *Ocean Eng.*, vol. 211, p. 107603, Sep. 2020, doi: 10.1016/j.oceaneng.2020.107603.
- [7] S. Xu, M. Murai, X. Wang, and K. Takahashi, “A novel conceptual design of a dynamically positioned floating wind turbine,” *Ocean Eng.*, vol. 221, p. 108528, Feb. 2021, doi: 10.1016/j.oceaneng.2020.108528.

Questions

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Extra slides
