

Design optimization of spar floating wind turbines considering different control strategies

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Larsen and Hanson (2007)

Motivation

- Controller design is challenging for FWTs
- Several control strategies suggested
 - Trade-offs between structural loads, rotor speed tracking, and blade-pitch actuator use
 - Non-trivial to find optimal control parameters
- Interactions between controller and structure
 - Should be designed together for fair comparison between solutions
- Simultaneous design optimization with realistic design limits

Linearized FWT model

- Linearized model
 - aero-hydro-servo-elastic
 - frequency-domain
 - stochastic wind/wave input

$$\mathbf{x} = \mathbf{x}_0 + \Delta \mathbf{x}, \quad \mathbf{u} = \mathbf{u}_0 + \Delta \mathbf{u}$$

$$\Delta \dot{\mathbf{x}} = \mathbf{A} \Delta \mathbf{x} + \mathbf{B} \Delta \mathbf{u}$$

- External loads
 - wave excitation
 - thrust
 - tilting moment
 - torque
- Control inputs
 - generator torque
 - collective blade pitch angle





Linearized FWT model

• Four structural DOFs

• Rigid blades

• Internal forces from dynamic equilibrium

• Valid for spar platforms (circular cross section) with catenary mooring

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Blade-pitch control strategies

- CS1: PI
- CS2: PI + platform pitch velocity feedback
- CS3: PI + nacelle velocity feedback
- CS4: PI + nacelle velocity feedback + WF low-pass filter

• Modified rotor speed reference in CS2-4:

$$\dot{\varphi}_0' = \dot{\varphi}_0 (1 + k_f \dot{x}_f)$$

Optimization problem

- Objective
 - Minimize cost of platform + tower
 - Material and manufacturing
- Design variables, structure
 - Tower/hull dimensions
 - Hull scantling design not considered

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 - PI gains $(k_p \text{ and } k_i)$
 - Velocity feedback gain (k_f)
 - Low-pass filter corner frequency (ω_f)
 - 47 design variables in total

Design variable	k_p	k _i	k_f	ω_f	
CS1	\checkmark	\checkmark			_
CS2	\checkmark	\checkmark	\checkmark		
CS3	\checkmark	\checkmark	\checkmark		
CS4	\checkmark	\checkmark	\checkmark	\checkmark	

Environmental conditions

- Long-term fatigue
 - 15 ECs
 - 1-30 m/s with 2 m/s step
 - Most probable H_s and T_p

- Short-term extreme response
 - 3 ECs
 - 50-year contour

Condition	1	2	3
Mean wind speed [m/s]	13.0	21.0	50.0
Significant wave height [m]	8.1	9.9	15.1
Spectral peak period [s]	14.0	15.0	16.0

Optimization problem

- Constraints, structure
 - Fatigue damage and buckling in tower
 - Maximum platform pitch angle, < 15°
 - Heave natural period, > 25 s
 - Most probable 1-h maximum value used as extreme response
- Constraints, control
 - Rotor speed variation (std.dev.), blade pitch actuator use (ADC)
 - Constraint values based on land-based DTU 10 MW
 - Weighted average of short-term values

$$ADC_{i} = \frac{1}{T} \int_{0}^{T} \frac{|\dot{\theta}_{i}(t)|}{\dot{\theta}_{\max}} dt, \qquad ADC = \sum_{i=1}^{N_{EC}} p_{i}ADC_{i}$$

- Gradient-based optimization
 - OpenMDAO framework
 - Analytic derivatives

Design solutions 125 120 CS1 CS2 CS3 100 100 CS4 Elevation relative to SWL [m] 80 75 60 50 Elevation relative to SWL [m] 40 25 20 7.5 10.0 12.5 15.0 0.02 0.04 0.06 0 Wall thickness [m] Diameter [m] -25 Below wave zone ٠

- Heighten CoB, lower CoG
- Increases pitch restoring stiffness
- Intersection platform/tower
 - Balance between wave loads and fatigue resistance

15

10

-50

-75

-15

-10

-5

0

Distance from platform center [m]

5

Structural response

- Controller primarily affects resonant pitch response
 - More aerodynamic damping
 - Tower base bending moment spectrum, 15 m/s mean wind speed

- Most critical extreme response found above cut-out
 - No impact from controller

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Cost and performance comparison

- Cost reduction mainly in tower due to lower fatigue loads •
 - Some reduction in platform costs, coupling with tower
- CS1 unable to fully utilize available actuator capacity •
- CS4 does not offer much additional reduction in cost, but •
 - Less rotor speed variation
 - Larger improvements likely for designs with more WF response
- Cost comparison strongly dependent on chosen constraint values ٠

Verification

- Comparison with nonlinear time domain simulations
- Mostly, trends are captured with reasonable accuracy
- Fatigue damage for CS1 significantly overpredicted
 - Optimal design has small aerodynamic damping in pitch
 - Does not occur with velocity feedback control
- Rotor speed variation quite consistently underestimated
 - Can be considered by lowering constraint value

Conclusions

- Integrated optimization of a spar FWT
 - Evaluation of trade-off effects in a lifetime perspective
- Linearized model captures trends, but
 - Overestimates pitch response if aerodynamic damping is low
- Controller mainly affects resonant pitch response
 - Cost reductions in tower due to lower fatigue loads
 - Actual values depend on rotor speed variation and ADC constraints
 - Alternative to use multi-objective approach
- No effect from controller on extreme response
 - Limited coupling effects
 - Small variations for the platform design

Limitations/future work

- Transient and nonlinear events
 - Extreme rotor speed excursions
- Consider impact of controller on
 - Blades
 - Drivetrain
 - Mooring system
- Additional modifications
 - Torque controller
 - IPC

Thank you for your attention!

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