Dynamic Analysis of Power Cable in Floating Offshore Wind Turbine

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Presentation Highlights



Part 1. Motivation and Background

Between 1971 and 2015, global energy consumption more than doubled from 61,900 TWh to 160,000 TWh (EIA, 2017; IEA, 2017a).



- Hydropower 16.6%
- Wind power 4.0%
- Bio-power 2.0%
- Solar PV 1.5%
- Ocean, CSP, and geothermal power 0.4%

Figure 1. Estimated renewable energy share of global electricity production at the end of 2016; data extracted from REN21 (2017).

Part 1. Motivation and Background

Europe installed 11.7 GW (10.1 GW in EU-28) of new wind energy in 2018. This is a 32% decrease on 2017. Europe decommissioned 0.4 GW of wind turbines. So the net increase in Europe's wind energy capacity in 2018 was 11.3 GW.



Figure 2. Total power generation capacity in the European Union 2008-2018

Figure 3. Renewable energy investments in 2018 (€bn)14

Wind energy accounted for 63% of Europe's investments in renewable energy in 2018, compared to 52% in 2017. Onshore wind projects alone attracted 39% of the total investment activity in the renewable energy sector

Part 2. Offshore Wind Technology Development



Figure 4. Natural progression of substructure designs from shallow to deep water(source NREL)

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Part 2. Offshore Wind Technology Developement

✓ Barge

✓ Spar-Buoy

✓ Tension Leg Platform (TLP)



Figure 5. Floating platform concepts for offshore wind turbines

Part 2. Complexity of Infrastructure of FOWTs



Layout of Horns Rev 2 Wind Farm







Source NREL

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Part 2. Fatigue as an issue for FOWTs

Source of Failure

- Fatigue
- Corrosion
- Fishing



Source: Floating Offshore Wind: Market and Technology Review



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Modeling

Part 3. Numerical Modeling



FAST

Is a tool for simulating the coupled dynamic response of wind turbines.



Figure 6. Model of FOWT in FAST code



ANSYS AQWA

Is an engineering analysis suite of tools for the investigation of the effects of wave, wind and current on floating and fixed offshore and marine structures,.



Figure 7. Model of FOWT in Ansys AQWA

Part 3. Global Dynamics and Loads



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Part 3. Benchmark for Validation





Structural Properties of Mooring Lines

| Description | Unit | | |
|--|-----------|--|--|
| the mass per unit length of the line (kg/m) | 77.7066 | | |
| the line stiffness, product of elasticity modulus and cross-sectional area (N) | 384.243E6 | | |
| Diameter (m) | 0.09 | | |
| | | | |

Hydrodynamic Properties of Model

| | Description | Unit | | |
|---|---|--|--|--|
| | Water density (kg/m^3) | 1025 | | |
| | Water depth (meters) | 320 | | |
| | Displaced volume of water when the | 8029.21 | | |
| | platform is in its undisplaced position (m^3) | | | |
| | Incident wave kinematics model | Regular | | |
| | Analysis time for incident wave calculations (s) | 3630 | | |
| | Time step for incident wave calculations | 0.25 | | |
| | Significant wave height of incident waves (meters) | 6 | | |
| ~ | Peak-spectral period of incident waves | 10 | | |
| | Range of wave directions(degrees) | 90 | | |
| | Wave Type | Stokes 2 nd -order wave theory | | |
| | Low frequency cutoff used in the summation-frequencies (rad/s) | 0.1 | | |
| | | | | |
| | High frequency cutoff used in the summation-frequencies (rad/s) | 1.9132 | | |
| | High frequency cutoff used in the summation-frequencies (rad/s) Current profile model | 1.9132 No Current | | |
| | High frequency cutoff used in the summation-frequencies (rad/s) Current profile model Analysis time for wave (s) | 1.9132 No Current 1000 | | |
| | High frequency cutoff used in the summation-frequencies (rad/s) Current profile model Analysis time for wave (s) Time step for wave (s) | 1.9132 No Current 1000 0.0125 | | |
| | High frequency cutoff used in the summation-frequencies (rad/s) Current profile model Analysis time for wave (s) Time step for wave (s) Additional Linear Damping in Surge N/(m/s) | 1.9132 No Current 1000 0.0125 100,000 | | |
| | High frequency cutoff used in the summation-frequencies (rad/s) Current profile model Analysis time for wave (s) Time step for wave (s) Additional Linear Damping in Surge N/(m/s) Additional Linear Damping in Sway N/(m/s) | 1.9132 No Current 1000 0.0125 100,000 100,000 | | |
| | High frequency cutoff used in the summation-frequencies (rad/s) Current profile model Analysis time for wave (s) Time step for wave (s) Additional Linear Damping in Surge N/(m/s) Additional Linear Damping in Sway N/(m/s) Additional Linear Damping in Heave N/(m/s) | 1.9132 No Current 1000 0.0125 100,000 100,000 130,000 | | |
| | High frequency cutoff used in the summation-frequencies (rad/s) Current profile model Analysis time for wave (s) Time step for wave (s) Additional Linear Damping in Surge N/(m/s) Additional Linear Damping in Sway N/(m/s) Additional Linear Damping in Heave N/(m/s) Additional Linear Damping in Yaw Nm(rad/s) | 1.9132 No Current 1000 0.0125 100,000 100,000 130,000 13,000,000 | | |
| | High frequency cutoff used in the summation-frequencies (rad/s) Current profile model Analysis time for wave (s) Time step for wave (s) Additional Linear Damping in Surge N/(m/s) Additional Linear Damping in Sway N/(m/s) Additional Linear Damping in Heave N/(m/s) Additional Linear Damping in Yaw Nm(rad/s) Hydrostatic Restoring in Heave (N/m) | 1.9132 No Current 1000 0.0125 100,000 100,000 130,000 13,000,000 332,941 | | |
| | High frequency cutoff used in the summation-frequencies (rad/s) Current profile model Analysis time for wave (s) Time step for wave (s) Additional Linear Damping in Surge N/(m/s) Additional Linear Damping in Sway N/(m/s) Additional Linear Damping in Heave N/(m/s) Additional Linear Damping in Yaw N/(m/s) Additional Linear Damping in Yaw Nm(rad/s) Hydrostatic Restoring in Heave (N/m) Hydrostatic Restoring in Roll (Nm/rad) | 1.9132 No Current 1000 0.0125 100,000 100,000 130,000 13,000,000 332,941 -4,999,180,000 | | |

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Part 3. Load Case for Validation

| DOF | Wind Condition | Wave Condition | Analysis Type |
|-----------------|---------------------------------|-----------------------------|----------------------|
| Platform, Tower | Steady, Uniform Vhub = 8 m/s | Regular Airy: H=6m T=10S | Time-Series solution |

| Description | Unit |
|------------------------------|--------------|
| Total run time (s) | 1000 |
| Time steps for Analysis (s) | 0.0125 |
| Time step for tabular output | : (s) 0.1 |
| Compute structural dynamic | cs ElastoDyn |
| Compute hydrodynamic | HydroDyn |
| Compute mooring system | MoorDyn |
| Compute inflow wind veloci | ties Off |
| Compute aerodynamic load | s Off |
| Compute control and elect | rical- Off |
| drive dynamics | |
| Compute sub-strue | ctural Off |
| dynamics | |
| Compute ice loads | Off |

Part 3. Flowchart of modeling in FAST



Source NREL

Part 3. Result Validation

Platform Heave



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Part 3. Result Validation



Figure 9. Jonkman Report Surge

Part 3. Result Validation



Part 3. Motion in Ansys AQWA



Part 4. Flowchart for fatigue analysis of electrical cable



Part 4. Properties of Electrical Cable



Standard flexible riser configurations for floating offshore structures

Part 4. Properties of Electrical Cable

Parameter of short-term sea state (South China Sea)

5.6 0.675 0.168 2.24096 4 6 0.675 5 0.180 8.68372 7 1.050 4 0.210 1.96084 7.80 1.050 0.234 14.006 6 8.5 1.550 0.255 4 1.4006 9 1.550 5 0.270 10.36444 9.40 1.550 6 0.282 20.16864 2.175 0.324 5.32228 10.8 5 11.2 2.175 6 0.336 15.4066 12 2.875 0.360 8.96384 6 13.2 3.625 6 0.396 3.08132 14.5 0.432 0.56024 4 6 15.0 4.5 0.450 3.64156 7 16.1 5 7 0.483 0.84036 16.7 4.5 10 0.501 0.84036 17.2 4.5 11 0.516 0.28012 5.5 0.522 17.4 10 0.56024 18 5.5 0.540 0.56024 11 19.1 6.750 10 0.573 0.84020 20 3.625 12 0.6 0.280

S – N Curve Used for Cable Section



Source: Karlsen, S., Slora, R, Heide, K., Lund, S. Eggertsen, F. and Osborg, P.A. Dynamic Deep Water Power Cables. 2009 RAO/CIS Offshore, pp.184-203.

Part 4. Cable tension in different sea states



Stress Time History in Different Sea States and Rainflow Cycles

Part 4. Fatigue Life estimation

| Vw (m/s) | total damage (1000 sec) | total damage (1 day) | P (%) | Yearly Damage |
|----------------------|----------------------------|-------------------------|--------|---------------|
| 5.6 | 3.60407E-09 | 3.11392E-07 | 2.241 | 2.54703E-06 |
| 6 | 4.37E-09 | 3.77725E-07 | 8.6837 | 1.19722E-05 |
| 7 | 2.64145E-09 | 2.28221E-07 | 1.9608 | 1.63339E-06 |
| 7.8 | 3.95964E-09 | 3.42113E-07 | 14.006 | 1.74894E-05 |
| 8.5 | 1.87E-09 | 1.61391E-07 | 1.4006 | 8.2506E-07 |
| 9 | 3.9601E-09 | 3.42152E-07 | 10.364 | 1.29437E-05 |
| 9.4 | 5.12178E-09 | 4.42522E-07 | 20.169 | 3.25765E-05 |
| 10.8 | 6.85957E-09 | 5.92667E-07 | 5.3223 | 1.15133E-05 |
| 11.2 | 7.69934E-09 | 6.65223E-07 | 15.407 | 3.74082E-05 |
| 12 | 8.92858E-09 | 7.71429E-07 | 8.9638 | 2.52396E-05 |
| 13.2 | 1.01E-08 | 8.68329E-07 | 3.0813 | 9.76594E-06 |
| 14.5 | 1.06209E-08 | 9.17649E-07 | 0.5602 | 1.87648E-06 |
| 15 | 3.07823E-08 | 2.65959E-06 | 3.6416 | 3.53505E-05 |
| 16.1 | 1.74282E-08 | 1.5058E-06 | 0.8404 | 4.61876E-06 |
| 16.7 | 2.41503E-08 | 2.08658E-06 | 0.8404 | 6.4002E-06 |
| 17.2 | 2.81661E-08 | 2.43355E-06 | 0.2801 | 2.48816E-06 |
| 17.4 | 3.74334E-08 | 3.23425E-06 | 0.5602 | 6.61364E-06 |
| 18 | 5.1396E-08 | 4.44061E-06 | 0.5602 | 9.0805E-06 |
| 19.1 | 9.12866E-08 | 7.88716E-06 | 0.8402 | 2.41878E-05 |
| 20 | 3.61286E-08 | 3.12151E-06 | 0.28 | 3.19018E-06 |
| Sum of yearly damage | | | | 0.000257721 |
| Safety Factor | | | | 10 |
| Lifetime | | | | 388 years |



$$FD = \sum \frac{ni}{Ni}$$

Yearly Damage = P * Total Windy Days

In Process

- More Sea States and Different Seed Numbers
- Considering Bending Stiffness
- Modeling Lazy Wave Configuration for the cable

Future

• Using Irregular sea states

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Thanks for Your Attention

Dynamic Anaysis of Power Cable in FOWT

16 January 2020