

Drivetrain Optimization in Multi-megawatt Offshore Wind Turbines

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Outline of the Presentation

- 1 Introduction
- 2 Proposed drivetrain optimization approach
- 3 Generator optimization
- 4 Gearbox optimization
- 5 Numerical results
- 5 Conclusion



Introduction

Drivetrain Most Conventional Technologies

- High-speed induction generator

- Advantages: cheap
- Disadvantages: sensitive to transients & dynamics, low efficiency

- High speed doubly fed induction generator

- Advantages: cheap, fractional converter
- Disadvantages: brushes, sensitive to transients, low efficiency

- Direct drive self-excited synchronous generator

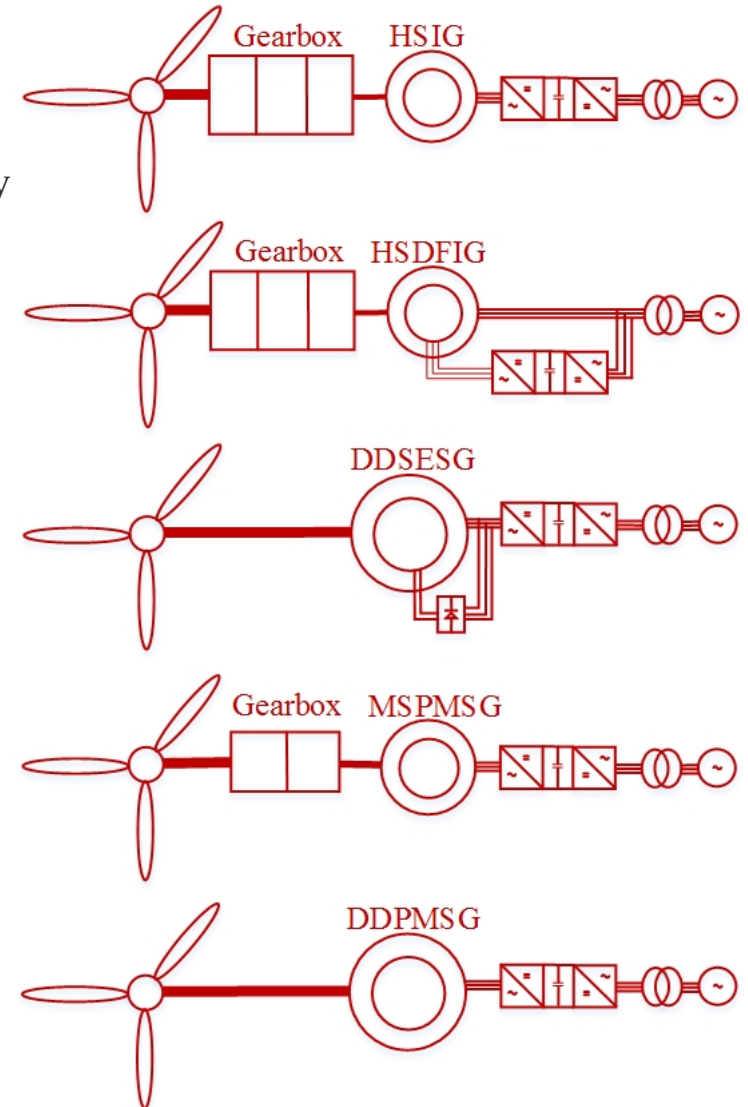
- Advantages: cheap
- Disadvantages: brushes, low efficiency, higher weight

- Medium speed permanent magnet synchronous generator

- Advantages: high efficiency, less weight
- Disadvantages: expensive

- Direct drive permanent magnet synchronous generator

- Advantages: high efficiency
- Disadvantages: expensive



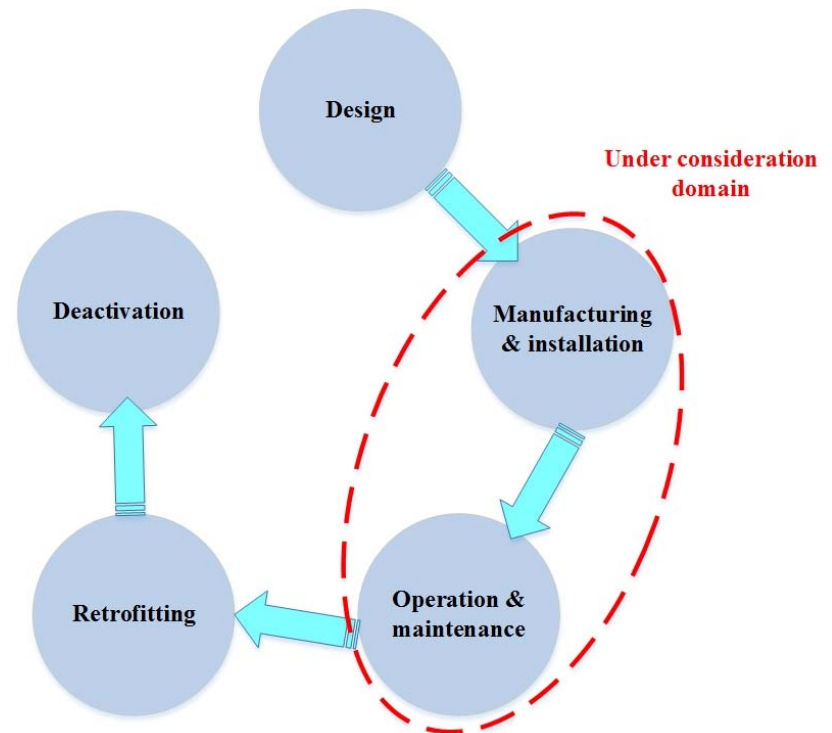
A Glance at Wind Turbine Industry

Most popular in offshore

IG	DFIG	DDSESG	DDPMSG	MSPMSG
SWT-4.0-130	GE 5.3-158	EN136-4.2	SG 8.0-167 DD	V164-10.0MW
Siemens	General Electric	Envision	Siemens	Vestas
4MW	5.3MW	4.2MW	8MW	10MW
Off-/onshore	onshore	Off-/onshore	offshore	offshore
1 : 119	geared	direct drive	direct drive	>41
V136-4.2 MW	SG 4.5-145	E-126 7.580	YZ150/10.0	SCD 8.0/168
Vestas	Siemens	Enercon	Swiss Electric	Aerodyn
4MW	4.5MW	7.6MW	10MW	8MW
onshore	onshore	onshore	offshore	offshore
geared (3 stages)	geared (3 stages)	direct drive	direct drive	1:27

Permanent Magnet Synchronous Generator

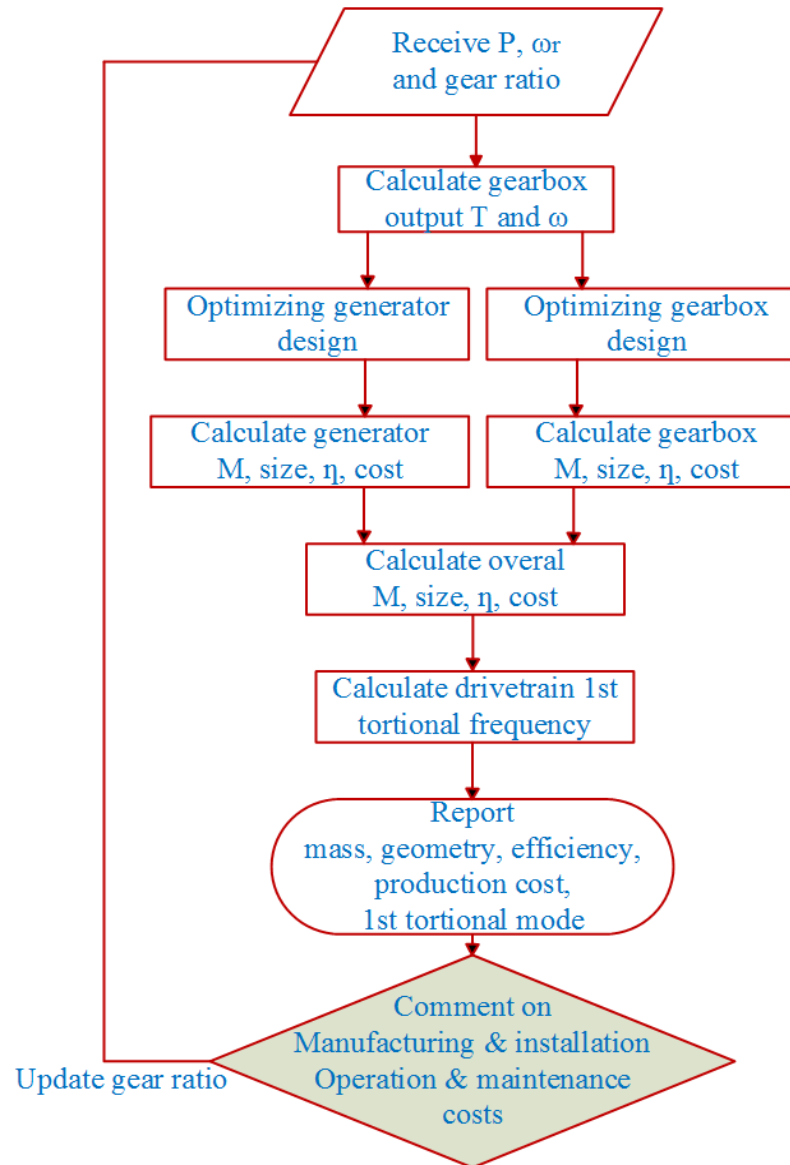
- Most popular technology for offshore wind turbines
 - High efficiency
 - Low maintenance
- Direct drive
 - Gearbox removal
- Medium speed
 - Smaller generator
 - Less manufacturing efforts
 - Easier installation and maintenance
- Research problem:
 - Which topology gives the highest benefits?
- To answer, we need to see the performance over the life cycle
- We will focus more on
 - Production cost
 - Efficiency
 - Operation





Proposed Drivetrain Optimization

Proposed Drivetrain Optimization Approach





Generator Optimized
Design

Generator Optimized Design

- Cost function

$$C_{Gen}^{Act} = c_{Fe}m_{Fe} + c_{Cu}m_{Cu} + c_{PM}m_{PM},$$

where c_{Fe} , c_{Cu} and c_{PM} are the unit costs, and m_{Fe} , m_{Cu} and m_{PM} are the weight of active materials.

- Optimization variables

- Air gap diameter (Ds), Stack length (Ls), Slot width (bs), Slot height (hs), Magnet height (hm)
- The other design variables are either a function of optimization variables or constant

- Constant design variables

- The values will change using an external loop, but will take a constant value in each optimization:
Slot per pole per phase, Magnet width to pole pitch ratio, Air gap

- Dependent design variables

- Air gap/teeth/stator yoke/ rotor yoke flux densities, stator/rotor yoke lengths, teeth width/height

- Subject to

- A wide range of electrical loading, magnetic loading, insulation requirements, and mechanical forces mitigation, and efficiency based constraints to ensure a secure operation.

- Outputs:

- Geometry, Weight, Cost, Efficiency

- Constrained nonlinear multi-variable nonconvex problem.

- Using Matlab Fmincon solver to find local optimizers.

Generator Optimization Results

- DTU 10MW PMSG realisation
 - Direct drive
 - Medium speed ($G/R= 50$)
 - High speed ($G/R= 156$)
- The following has been modelled
 - Carter impact
 - Iron fill factor
 - Insulation
 - 2-layers, full pitch
- Structure weight
 - Cooling
 - Beams
 - Cylinder
 - Shaft
 - Modeled as a function of design variables

Generator parameters	DDPMSG	MSPMSG	HSPMSG
<p>Results will be reported in the paper.</p>			



Gearbox Optimized Design

Gearbox Optimized Design

- Cost function for a three-stages gearbox

$$C_{Gearbox}^{Gears} = c_{Fe} (m_{Gear}^1 + m_{Gear}^2 + m_{Gear}^3),$$

where c_{Fe} is the unit cost of gears, and m_{Gear}^1, m_{Gear}^2 and m_{Gear}^3 are the weight of 1st, 2nd and 3rd stages .

- Parallel stage: $m_{Gear}^{Parallel} = K_{AG} \frac{2Q_p}{k} (1 + \frac{1}{U_s} + U_s + U_s^2)$
- Planetary stage: $m_{Gear}^{Planetary} = K_{AG} \frac{2Q_s}{K} (\frac{1}{B} + \frac{1}{BU_{SN}} + U_{SN} + U_{SN}^2 + K_r \frac{(U_s-1)^2}{B} + K_r \frac{(U_s-1)^2}{BU_{SN}})$

The overall cost function for a sample three-stages gearbox with two planetary and one parallel will be:

$$V = \frac{2Q_0}{K} \frac{1}{U_1} \left[\frac{1}{B_1} + \frac{1}{B_1(\frac{U_1}{2}-1)} + (\frac{U_1}{2} - 1) + (\frac{U_1}{2} - 1)^2 + K_{r1} \frac{(U_1-1)^2}{B_1} + K_{r1} \frac{(U_1-1)^2}{B_1(\frac{U_1}{2}-1)} \right] \\ + \frac{2Q_0}{K} \frac{1}{U_1 U_2} \left[\frac{1}{B_2} + \frac{1}{B_2(\frac{U_2}{2}-1)} + (\frac{U_2}{2} - 1) + (\frac{U_2}{2} - 1)^2 + K_{r2} \frac{(U_2-1)^2}{B_2} + K_{r2} \frac{(U_2-1)^2}{B_2(\frac{U_2}{2}-1)} \right] \\ + \frac{2Q_0}{K} \frac{1}{U_1 U_2 U_3} \left[1 + \frac{1}{U_3} + U_3 + U_3^2 \right]$$

where U is gear ratio, B is number of planets, Kr is ring scaling factor, Q is input torque.

- Subject to
 - Constraints related to gear ratio of each stage, and the overall gear ratio, concerning with the mechanical design limitations.
- Outputs: Optimized gear ratios, Weight, Cost, Efficiency
- Constrained nonlinear multi-variable nonconvex problem. Matlab Fmincon solver is used.

Gearbox Optimization Results


- DTU 10MW gearbox realisation

- Direct drive
- Medium speed ($G/R= 50$)
- High speed ($G/R= 156$)

- Structure weight

- Bearings
- Housing
- Carriers
- Modeled as a fraction of gears weight

Gearbox parameters	MSPMSG	HSPMSG
Results will be reported in the paper.		



Concluding Remarks

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- Results show that medium speed drivetrain seems to be a better option for offshore wind turbines.
- It would help to have a safe distance from the external excitations frequencies, and is recommended for offshore floating applications.
- Reduction of drivetrain weight, and consequently reduction of nacelle weight potentially reduces the required nacelle, tower and platform costs.
- Impacts on reliability, operation and maintenance costs will be investigated in future works.