

INTRODUCTION

Floating Wind Turbine (FWT) prototypes and pilot farms are located in shallower zones than most of the studies in the literature about moored FWT.

- ➔ For water depth > 150m, studies have been successful in defining a conventional catenary mooring system with heavy chains.
- ➔ For shallower water depth, solutions like taut or semi-taut configurations using material elasticity of synthetic ropes could be attractive for Marine renewable energy devices [1].

Design and comparisons of conventional catenary mooring chain systems and Taut mooring systems using synthetic fibres are done at 65m.

- ➔ Comparisons in terms of **Key Performance Indicators**
- ➔ Importance of **mooring modelling hypotheses** for line tensions and floater horizontal motions.

Numerical model



5MW – CSC Semi-submersible [2]
NEMOH + OrcaFlex

Hydrodynamics :
Potential theory + Drag forces

Aerodynamics :
Drag forces on rotor and tower

Moorings :
Lumped-mass model and non-linear load-strain curve

METHODOLOGY

Key Performance Indicators (KPI)

- **CAPEX**
 - Procurement Cost
 - Installation Cost
- **Operation And Maintenance (OAM)**
 - Preventive maintenance
 - Heavy maintenance
- **Environmental Impact and risk (EI)**
 - Footprint on seabed
 - Touchdown point excursion
- **Station keeping performance**
 - Maximum floater excursion

k€

KPI range : 1 (Low score) to 5 (High score).

Design Methodology

Mooring configurations defined parametrically covering design space

- Several Checks for each mooring configuration :
- ✓ Admissible Draft in static position
 - ✓ Admissible eigen periods at steady positions
 - ✓ Tension criteria according to DNV – OS – J103

Static → Frequency Domain → Time Domain

Reduced number of **Design Load cases (DLC)** with operating and parked wind turbine cases.

	Dir. (°)	Hs (m)	Tp (s)	Uc (m/s)	Uw (m/s)	X 2 depth (EWLR) w/ and w/o Marine Growth
DLC 1	247.5	11	15	0.7	44	
DLC 2	187.5	7	15	0.6	44	
DLC 3	247.5	11	15	0.3	11.4	
DLC 4	187.5	7	15	0.2	11.4	

Table 1 : Limited number of Design Load Cases

Site conditions

Shallow water:
Representative of planned pilot wind farm site around Groix Island on Atlantic French Coast.
Depth : LAT ~62,5m; HAT ~67,5m
Waves conditions : 47° 30 N, 3° 30 W from HOMERE [3]
(H_s, θ_{wave})_{50 years} contour calculated with Peak Over Threshold (POT) and fitted Generalized Pareto Distribution (GPD)

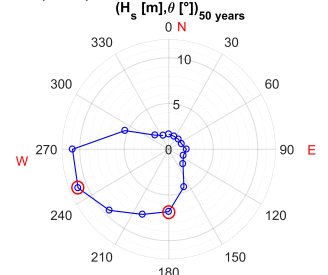


Figure 1 : (H_s, θ_{wave})_{50 years} contour from HOMERE with POT + GPD for point 47° 30N and 3° 30W

KPI Preliminary Evaluation

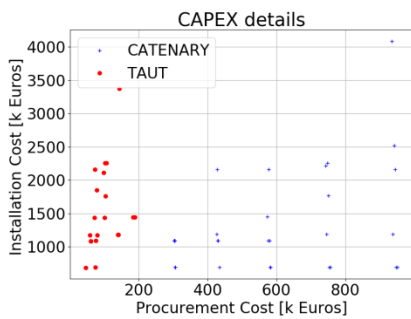


Figure 2 : Installation cost versus Procurement Cost for Taut and catenary mooring configurations.

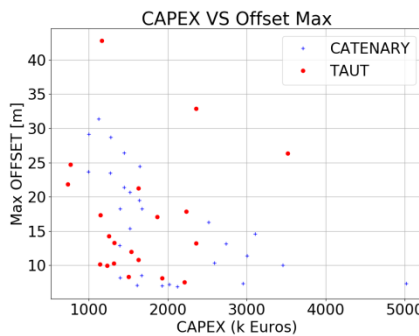


Figure 3 : CAPEX versus station keeping performance

Taut mooring configurations

Top and Bottom Chains:
L = 15m
Diam = 0,1m

Nylon
L = 30m
Diam = 0,1m

Catenary mooring chains

Chain
L = 15m
Diam = 0,1m

CONCLUSIONS

The main outcomes can be summarized by:

- Different wave directions could significantly change loads in the mooring lines
- A synthetic methodology with Key Performance Indicators has been defined
- When taking into account not only CAPEX but also Environmental impact and Station keeping performance, Taut mooring configurations appear efficient.
- Actual uncertainties on Marine Growth properties on site lead to a certain level of risk and unadapted mooring system.

REFERENCES

- [1] Ridge, I. M. L., S. J. Banfield, and J. Mackay. "Nylon fibre rope moorings for wave energy converters." *OCEANS 2010*. IEEE, 2010
- [2] Luan, C., Gao, Z., & Moan, T. (2016, June). Design and analysis of a braceless steel 5-mw semi-submersible wind turbine. In *ASME 2016 35th International Conference on Ocean, Offshore and Arctic Engineering*
- [3] Boudière, E., Maisondieu, C., Arduin, F., Accensi, M., Pineau-Guillou, L., & Lepesqueur, J. (2013). A suitable metocean hindcast database for the design of Marine energy converters. *International Journal of Marine Energy*, 3.

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