

Grid model reduction

for large scale wind integration analyses

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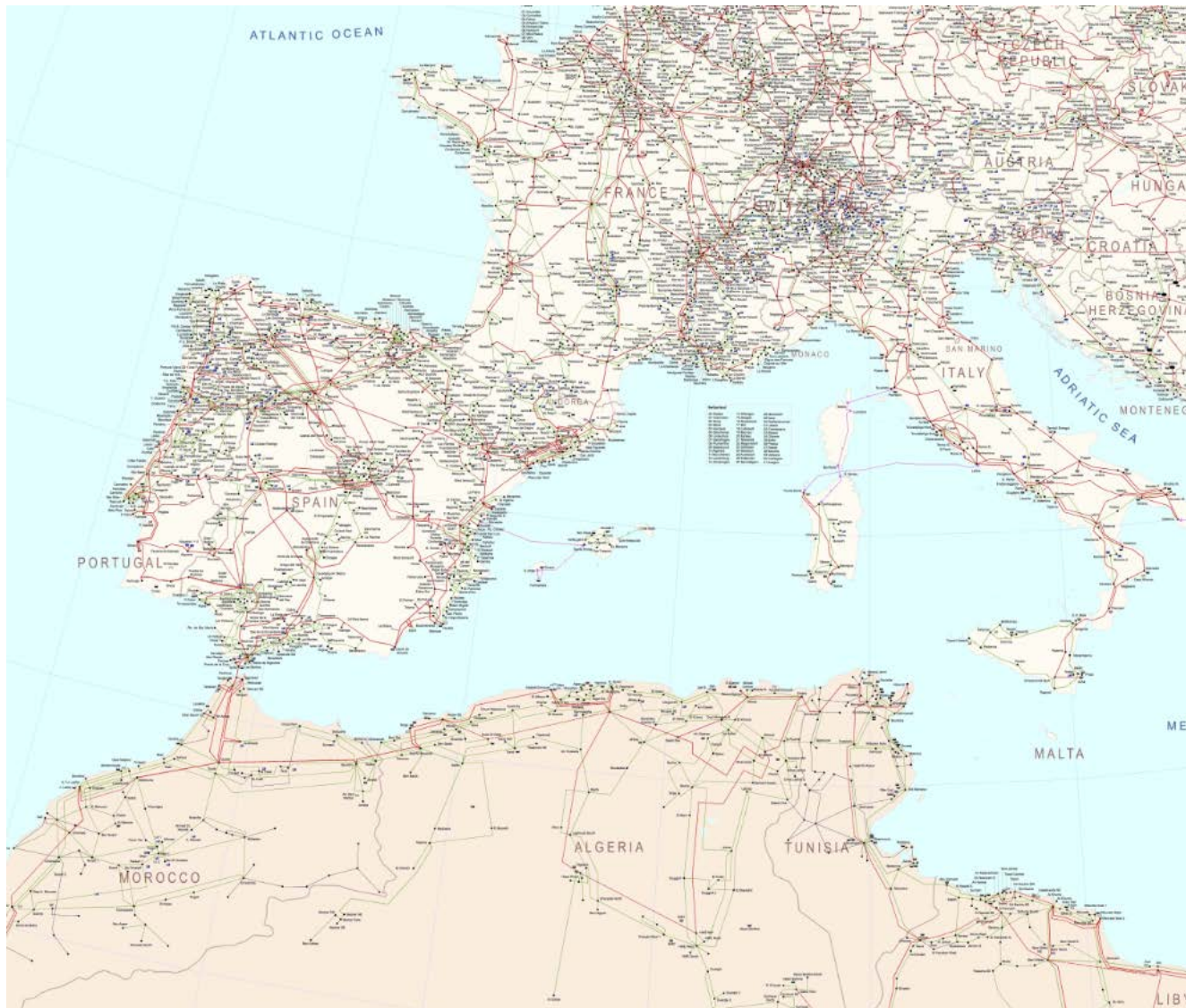
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How does a large, interconnected power system cope with large amounts of renewable energy?



Electricity grid: very big system

- hard to specify a consistent **data** set
- easy to get **lost in detail**
- computationally **expensive** simulations



Use reduced models

Summary

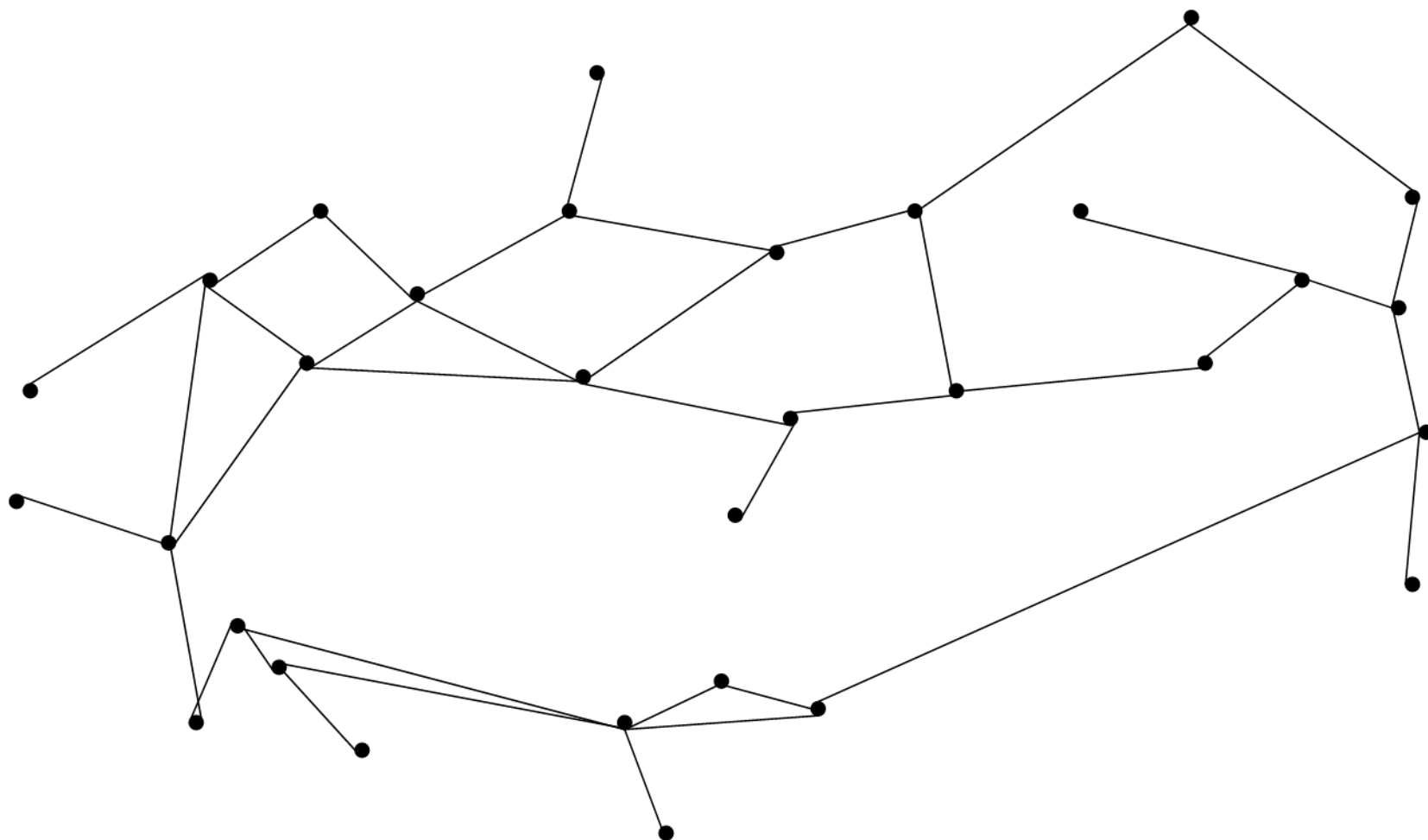
Implementation and application of a method to derive reduced, equivalent power flow models

- Reduction method
- Two examples: Norway, Morocco
- Use of reduced Morocco model

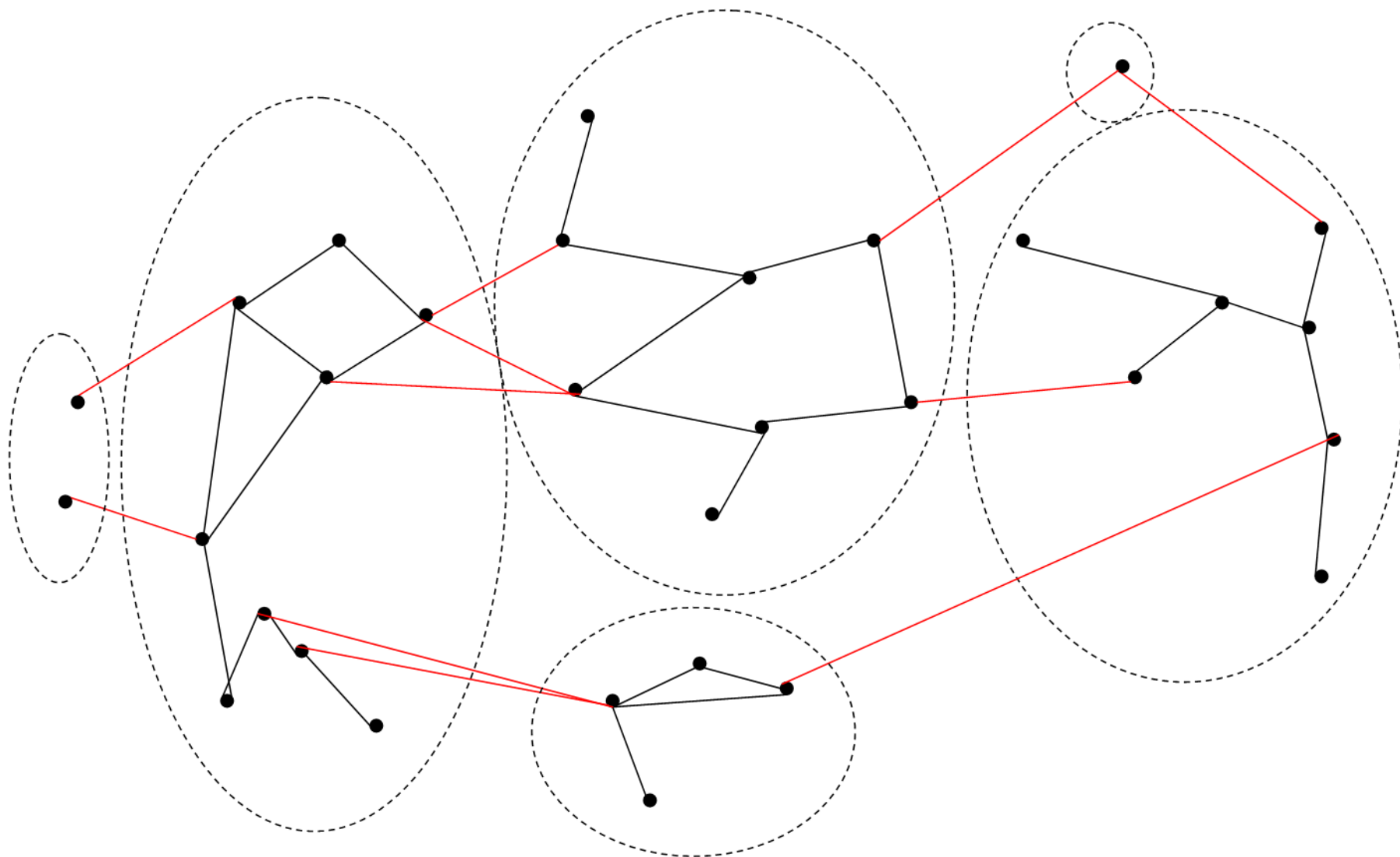
[1] X. Cheng, T. Overbye, Pdf-based power system equivalents, Power Systems, IEEE Transactions on 20 (4) (2005) 1868–1876. doi:10.1109/TPWRS.2005.857013.

[2] D. Shi, Power system network reduction for engineering and economic analysis, Ph.D. thesis, Arizona State University, <http://hdl.handle.net/2286/R.A.97598> (accessed 2014-06-24) (2012).

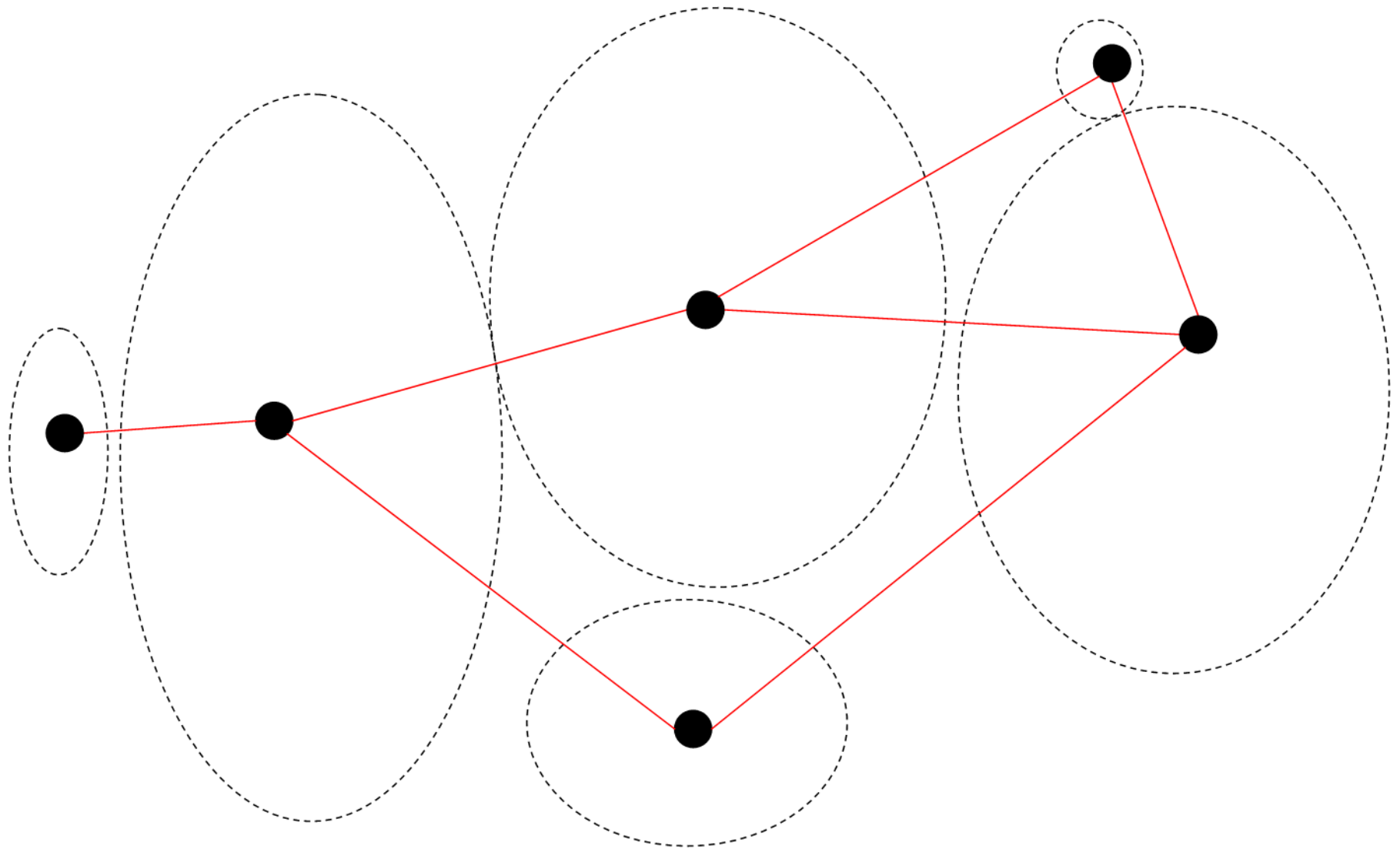
Original, detailed grid



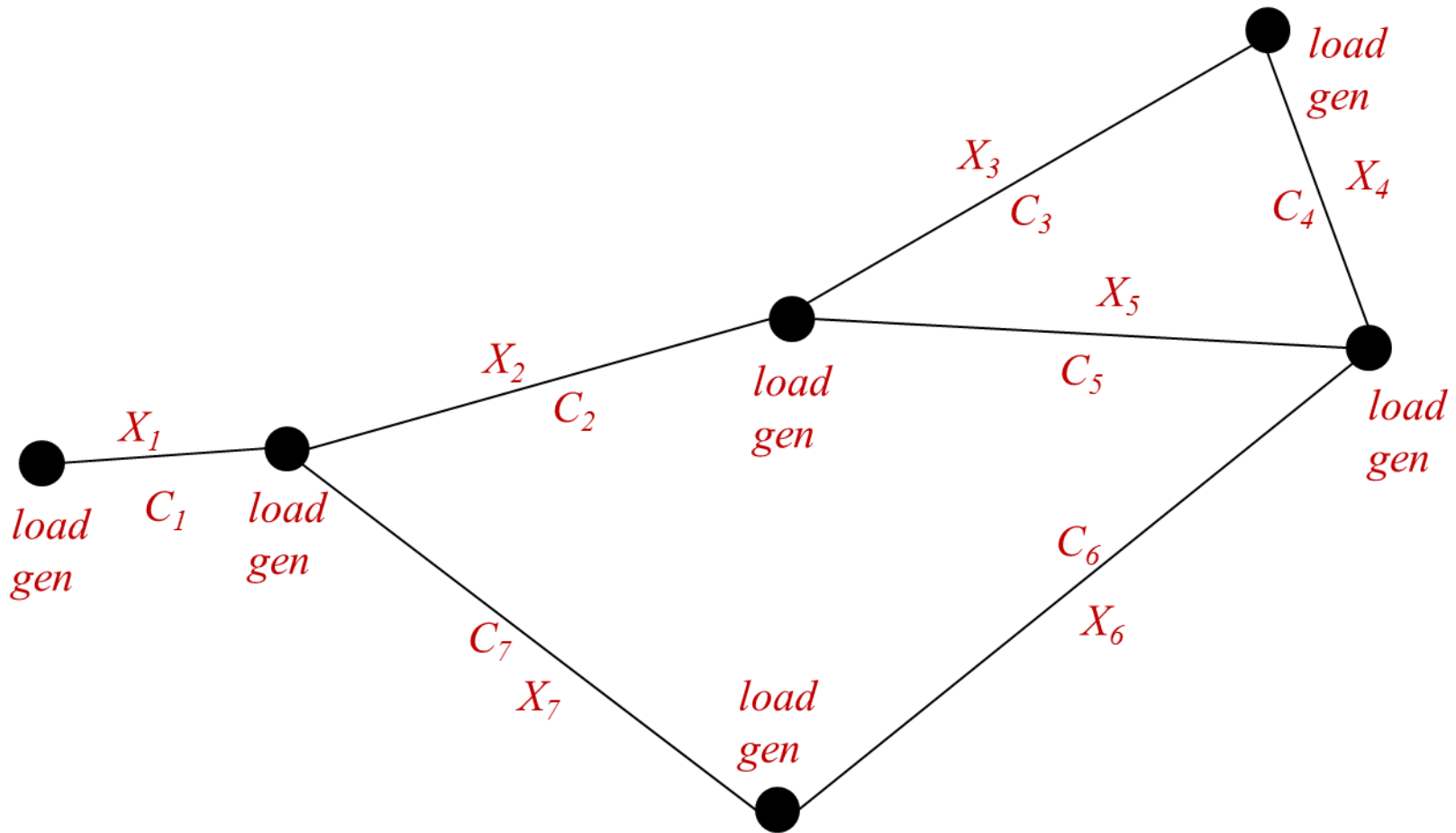
Clustering of nodes



Reduced model topology

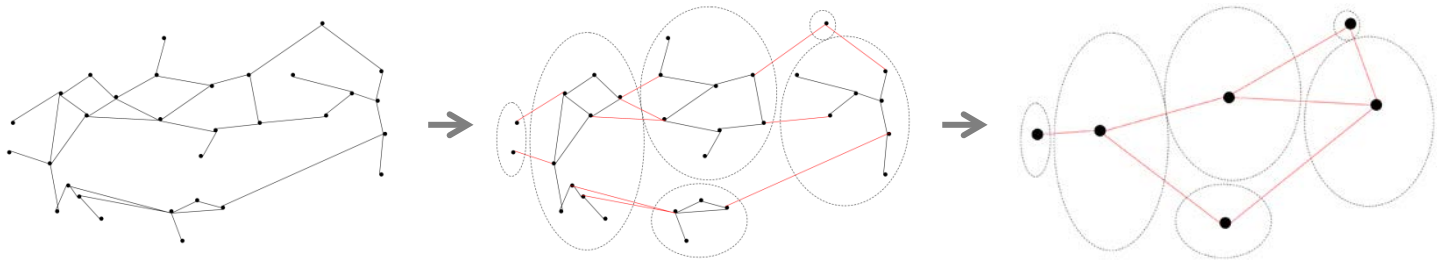


Reduced model parameters

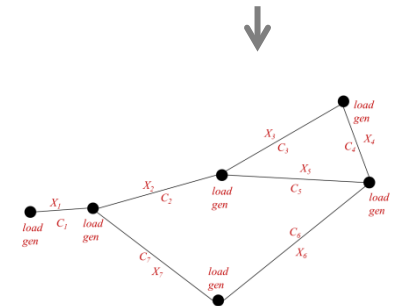


Reduced, equivalent grid

- Grid topology (nodes and connections)



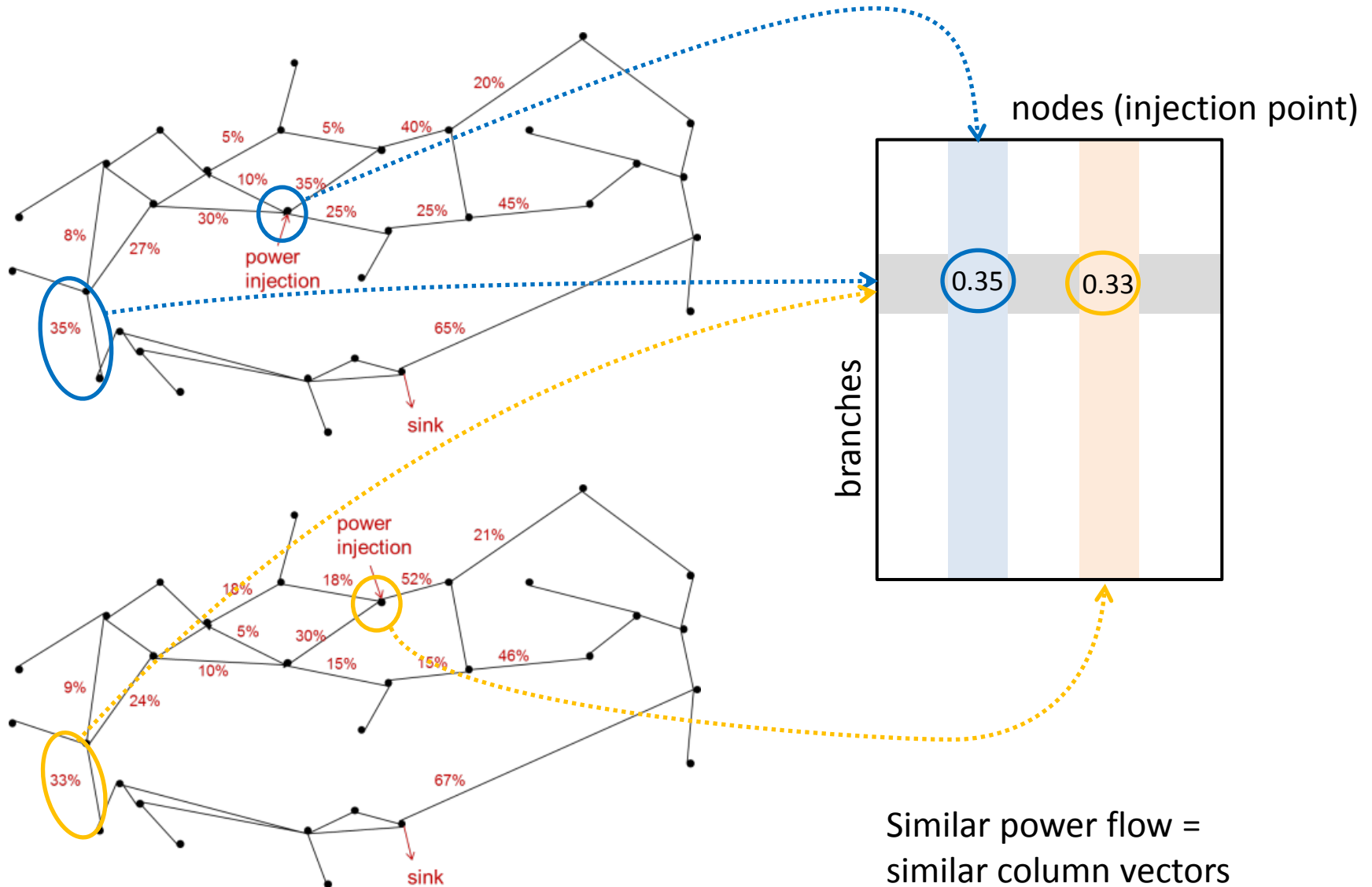
- Electrical parameters
 - Transmission capacity
 - Load and generation distribution
 - Impedance



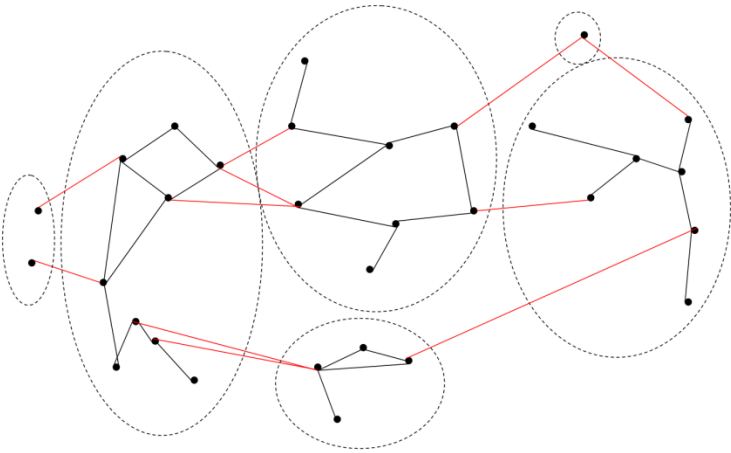
Grid topology – clustering

- Explicit clustering
- Automated clustering
 - Idea: If power injection at two nodes produce similar power flow distribution, these nodes are clustered together
 - Based on **Power Transmission Distribution Factors** (PTDF) and k-means clustering algorithm
 - Number of desired nodes given as input

PTDF matrix



Capacity, generation and load



- Transmission capacity
= sum of capacity of cluster-to-cluster connections in original model
- Load
= sum of load within cluster
- Generation
= sum of load within cluster
- Impedance:
 - Reduced model should exhibit **similar** power flow as original model

Equivalent impedance

Principle 1

- PTDF matrix is directly related to grid impedance (reactance)
- Equivalence between full and reduced model means
zonal PTDF from full model = PTDF from reduced model
- Use this to derive reduced model reactance

Principle 2

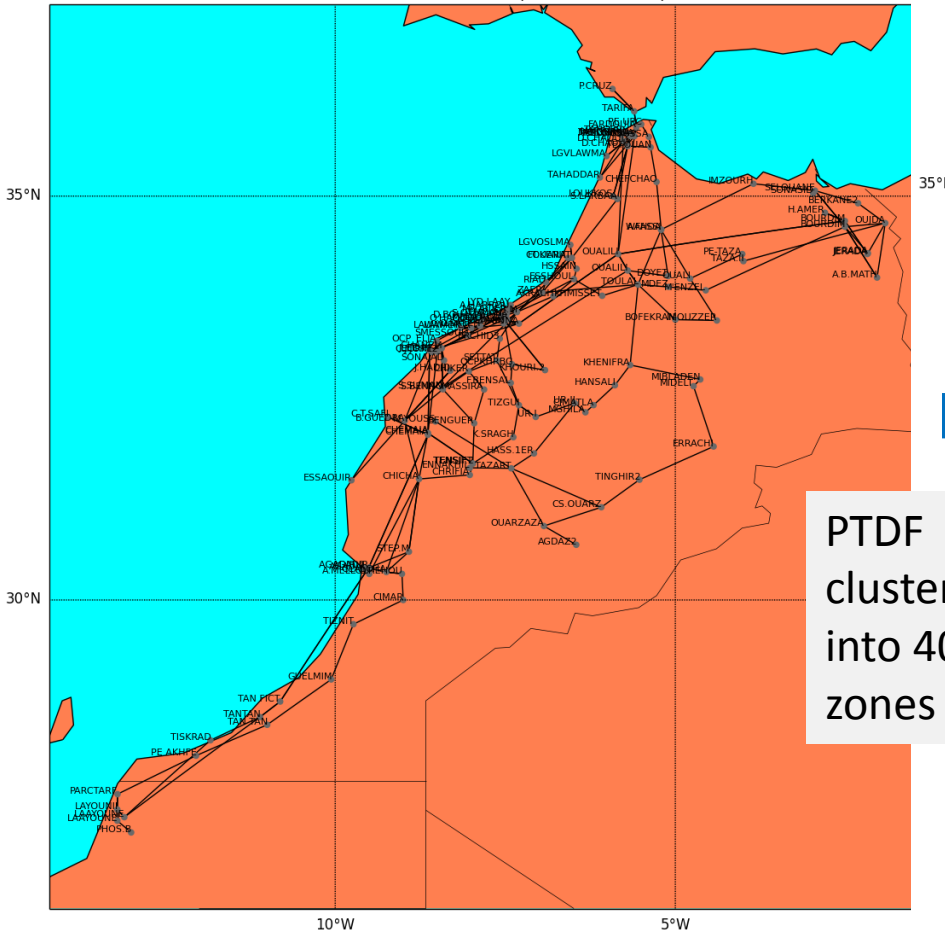
- A second condition is used to ensure that derived reactances have physical values:
Voltage angle differences in reduced model = differences between average voltage angles within clusters in full model

"=" equality in the sense of least error optimisation:

$$\min \{ w_1 | \text{PTDF}_{\text{zonal}} - \text{PTDF}_{\text{reduced}} |^2 + w_2 | \text{angle}_{\text{zonal}} - \text{angle}_{\text{reduced}} |^2 \} \Rightarrow X_{\text{reduced}}$$

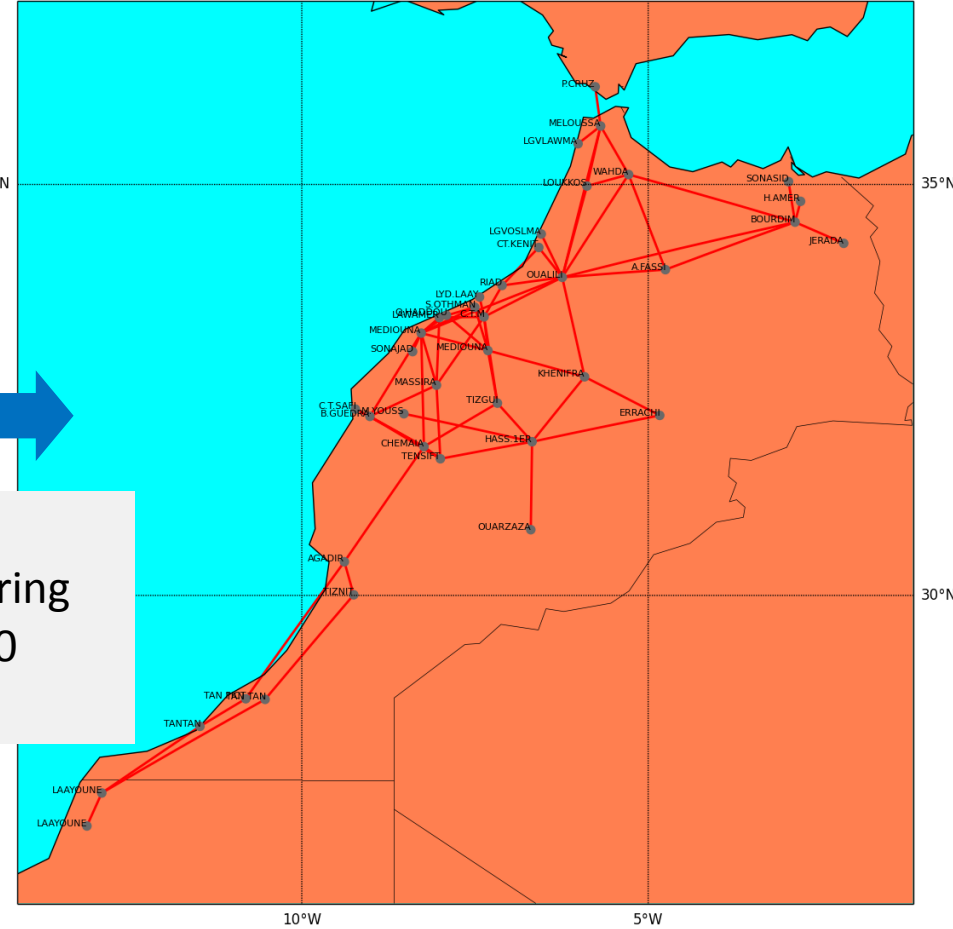
Morocco

Nodes and branches (400 and 225 kV)



Full grid (≥ 220 kV shown): 765 nodes

Nodes and branches



Reduced 40 bus model

PTDF
clustering
into 40
zones

Power flow

| from | to | X | full model | reduced model | from | to | X | full model | reduced model |
|------|----|---------|------------|---------------|------|----|--------|------------|---------------|
| 24 | 30 | 0.059 | 197.0 | 197.9 | 20 | 38 | 0.043 | 413.8 | 416.0 |
| 7 | 25 | 1.756 | -1.5 | -0.6 | 2 | 34 | 0.239 | 107.7 | 108.6 |
| 23 | 26 | 0.081 | -186.2 | -186.9 | 26 | 39 | 0.709 | -14.8 | -13.5 |
| 5 | 8 | 0.005 | 25.6 | 26.3 | 23 | 36 | -0.025 | 124.4 | 293.1 |
| 0 | 32 | -0.232 | 14.7 | 14.7 | 1 | 25 | 0.148 | -106.8 | -106.8 |
| 17 | 36 | -0.004 | -154.5 | -154.5 | 12 | 37 | -0.032 | 462.1 | 576.9 |
| 37 | 38 | 0.154 | 314.3 | 278.9 | 4 | 24 | 0.069 | 521.8 | 521.8 |
| 22 | 39 | 0.122 | -109.3 | -123.2 | 19 | 21 | 0.266 | -15.8 | -38.2 |
| 21 | 37 | 0.131 | -166.3 | -173.0 | 15 | 22 | 0.587 | 8.5 | 7.0 |
| 10 | 23 | -0.004 | -132.5 | 92.8 | 5 | 39 | 0.166 | -162.7 | -163.4 |
| 8 | 38 | 0.092 | 94.7 | 86.7 | 15 | 21 | 0.095 | 65.6 | 41.3 |
| 12 | 22 | 0.024 | 235.9 | 178.3 | 30 | 35 | -0.030 | 10.5 | 11.2 |
| 9 | 39 | 0.112 | -52.3 | -52.3 | 2 | 25 | 0.078 | -91.7 | -92.6 |
| 16 | 38 | -0.289 | -35.9 | -35.9 | 8 | 23 | -0.632 | 8.5 | 3.9 |
| 13 | 23 | 0.009 | -453.1 | -491.1 | 20 | 29 | 0.402 | 46.2 | 44.0 |
| 3 | 39 | -0.091 | -58.1 | -58.1 | 18 | 34 | -0.009 | 93.5 | 92.6 |
| 0 | 27 | -16.735 | 0.0 | 0.0 | 24 | 38 | 0.072 | 201.1 | 200.1 |
| 23 | 37 | 0.040 | -835.3 | -820.6 | 13 | 36 | -0.073 | 99.5 | 160.0 |
| 33 | 35 | 0.434 | -23.3 | -25.7 | 19 | 36 | 0.076 | -22.0 | -97.0 |
| 18 | 31 | 56.955 | -1.5 | -0.6 | 26 | 36 | 0.161 | 75.2 | 49.4 |
| 0 | 28 | 0.121 | -350.0 | -350.0 | 30 | 38 | -0.251 | -11.3 | -11.2 |
| 0 | 33 | 0.451 | 33.6 | 35.8 | 29 | 38 | -0.017 | -51.0 | -10.0 |
| 35 | 38 | -0.165 | -19.0 | -19.1 | 11 | 37 | 0.119 | -86.5 | -86.5 |
| 10 | 19 | 0.001 | -118.5 | -363.3 | 14 | 24 | -0.021 | -50.6 | -50.6 |
| 12 | 18 | 0.003 | 302.3 | 302.3 | 0 | 38 | 0.047 | 177.0 | 173.4 |
| 33 | 38 | 0.018 | -450.3 | -445.7 | 24 | 35 | 0.050 | 224.5 | 224.6 |
| 7 | 31 | 0.025 | 1.5 | 0.6 | 6 | 12 | 0.088 | 1320.0 | 1320.0 |
| 13 | 19 | 0.079 | -36.9 | -54.9 | 36 | 38 | 0.431 | 40.9 | 41.0 |
| 21 | 36 | 0.064 | 128.6 | 43.5 | 12 | 15 | 0.013 | 38.1 | 4.7 |
| 8 | 39 | 0.169 | -174.6 | -161.4 | 21 | 22 | 0.033 | -38.5 | 6.6 |
| 29 | 36 | 0.035 | -461.5 | -504.8 | 12 | 26 | 0.181 | 17.1 | -6.6 |
| 10 | 37 | 0.232 | -162.1 | -142.5 | 0 | 35 | 2.222 | 0.9 | 2.3 |
| 13 | 37 | 0.240 | -150.2 | -154.7 | 15 | 37 | 0.571 | -25.1 | -32.8 |
| 19 | 37 | 0.049 | -500.1 | -665.7 | | | | | |

OK!

Comparison

Voltage angles

OK!

| zone | full model | reduced model | zone | full model | reduced model |
|------|------------|---------------|------|------------|---------------|
| 0 | -24.7 | -24.2 | 20 | -19.2 | -18.7 |
| 1 | -2.2 | -5.0 | 21 | -15.2 | -17.2 |
| 2 | 2.8 | 0.0 | 22 | -14.5 | -17.3 |
| 3 | -3.9 | -5.7 | 23 | -21.5 | -22.9 |
| 4 | -0.6 | 0.0 | 24 | -21.3 | -20.6 |
| 5 | -24.3 | -24.2 | 25 | 6.9 | 4.1 |
| 6 | 54.4 | 51.7 | 26 | -13.1 | -14.2 |
| 7 | 5.3 | 3.5 | 27 | -1.8 | -24.2 |
| 8 | -24.4 | -24.3 | 28 | -0.6 | 0.0 |
| 9 | -10.2 | -12.1 | 29 | -28.9 | -28.8 |
| 10 | -21.2 | -23.1 | 30 | -27.8 | -27.3 |
| 11 | -8.6 | -10.1 | 31 | 5.3 | 3.5 |
| 12 | -11.3 | -14.9 | 32 | -22.7 | -22.3 |
| 13 | -23.9 | -25.5 | 33 | -34.0 | -33.5 |
| 14 | -20.7 | -20.1 | 34 | -11.3 | -14.9 |
| 15 | -11.5 | -14.9 | 35 | -27.7 | -27.1 |
| 16 | -23.5 | -23.0 | 36 | -19.8 | -18.8 |
| 17 | -19.5 | -18.5 | 37 | -2.7 | -4.2 |
| 18 | -11.8 | -15.4 | 38 | -29.4 | -28.9 |
| 19 | -21.2 | -23.0 | 39 | -6.9 | -8.7 |

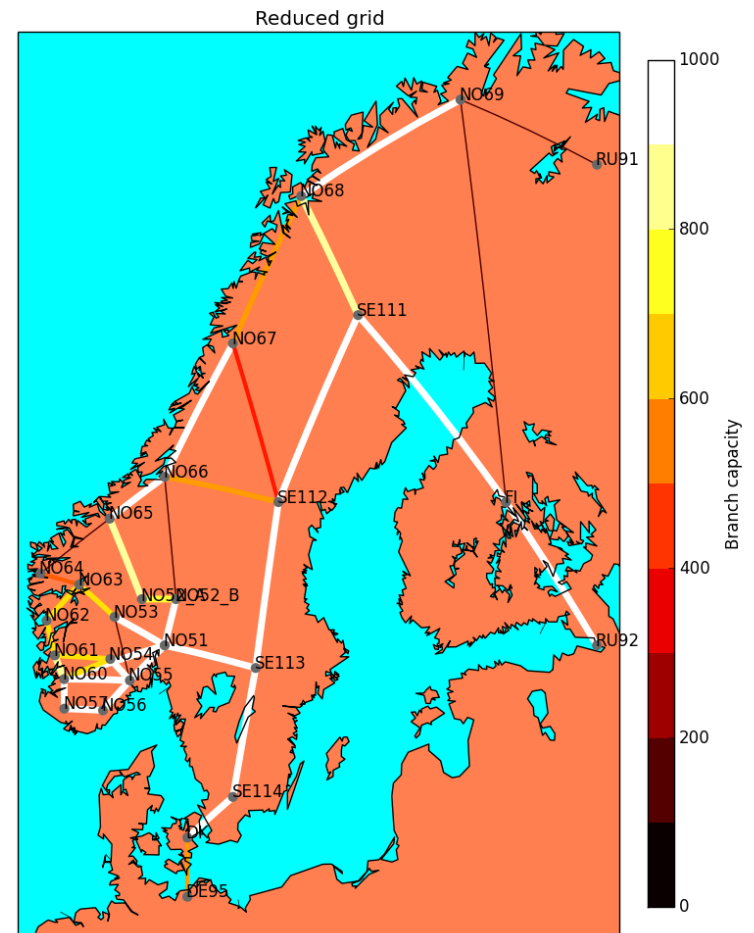
Norway



Full grid (>100 kV shown): 6133 nodes

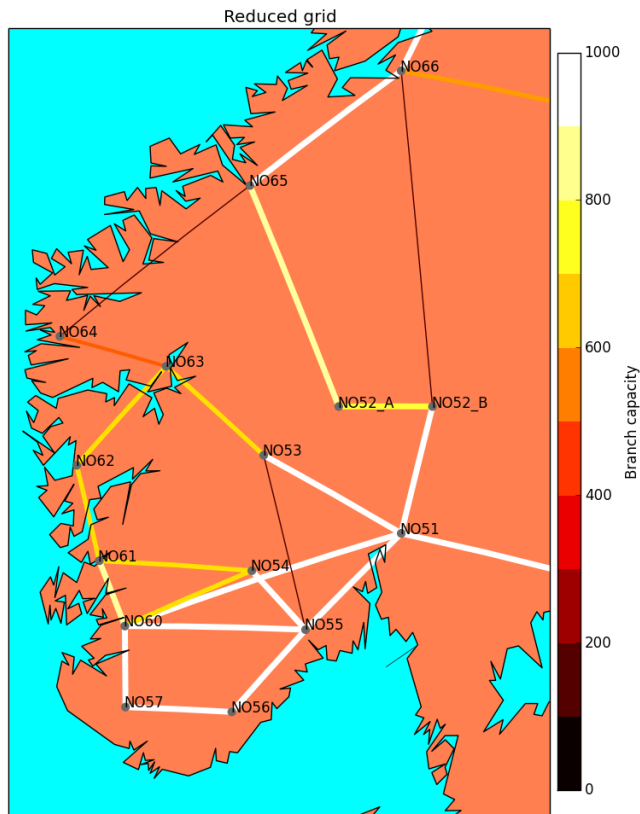


Explicit
separation
into 27
zones

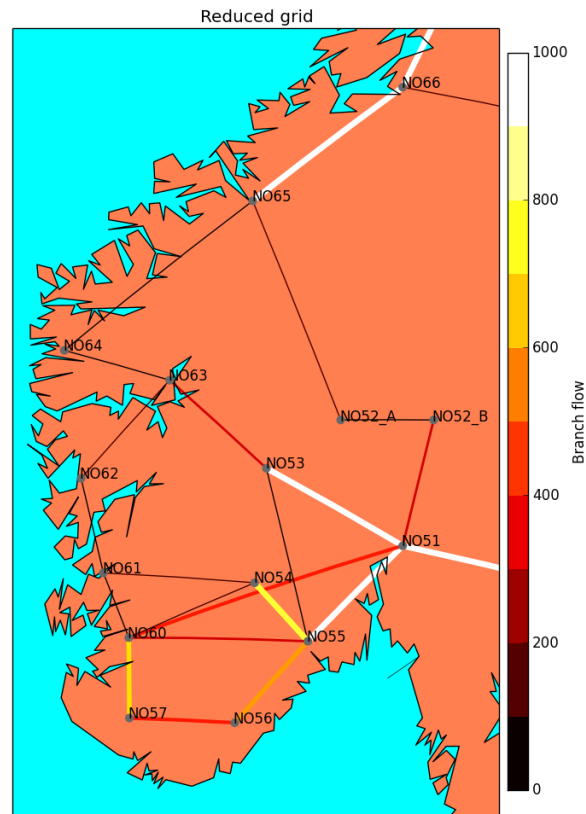


Reduced model: 27 nodes

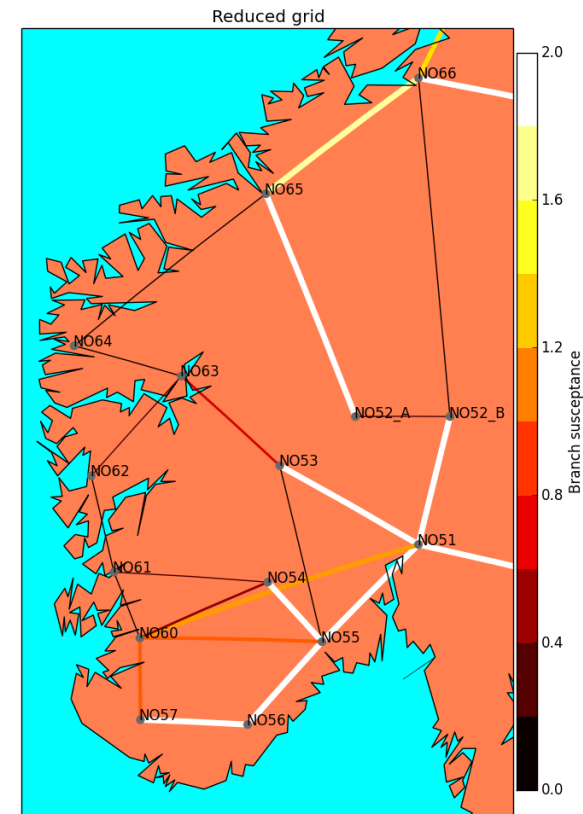
Norway – some details



Capacity



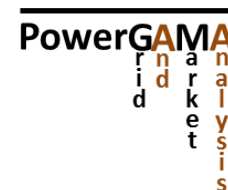
Power flow



Susceptance ($1/X$)

Application of reduced models

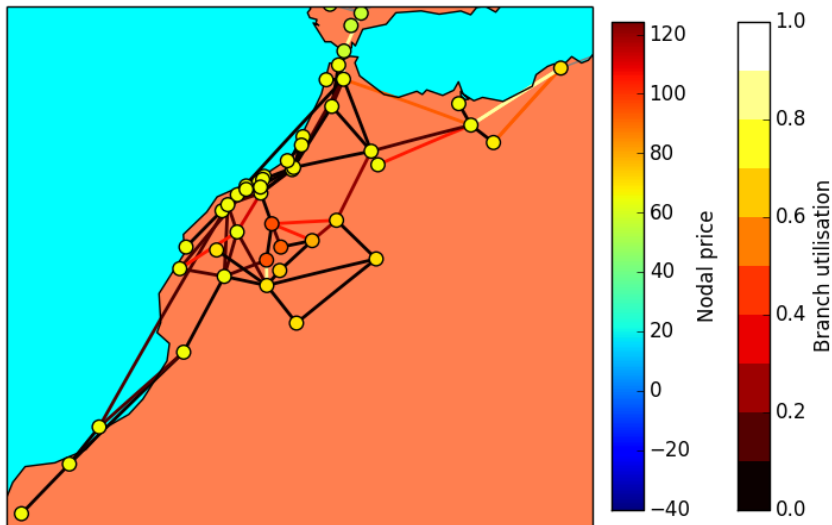
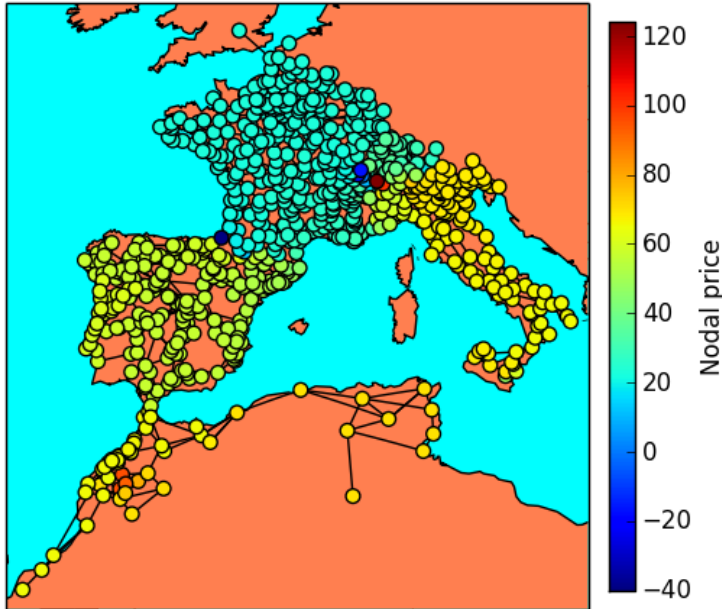
- **Idea:** Explore future scenarios of large-scale integration of renewable energy in interconnected power systems
 - Taking into account power flow constraints
 - Simplified market description
 - Simplified grid models
- Several previous studies focussing on North Sea offshore wind (TradeWind, OffshoreGrid, NOWITECH,...) using SINTEF's PSST tool
- EuroSunMed project:
 - Renewable energy in Mediterranean region
 - Open source tool PowerGAMA
(https://bitbucket.org/harald_g_svensden/powergama)



Western Mediterranean case study

An existing model of Europe has been extended to include North-Western Africa

Average nodal prices



Detail of Morocco part
Nodal prices
Branch utilisation

Conclusion

Method for automated grid model reduction
implemented as Matlab (and Python) scripts, taking PSSE
raw file as input

Applied to Morocco and Norway models

Reduced models are useful for power flow analyses in
large systems where there is need for simplifications

Result is dependent on the specific operating state
described by original full model