

Evaluation of fatigue loads of horizontal up-scaled wind turbines

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Aim:

- Identify key influences on fatigue and extreme loads

- Develop a general trend (Ideally in the form of simple power law curves)

- Reveal and quantify effects

- Develop

Key factors

- Wind conditions (mean wind speed, wind shear and turbulence intensity)

- Operational parameters (design tip speed, TSR, operational modes – pitch, stall, variable speed etc.)

- Structural parameters (mass and stiffness)

- Scale (size)

How do fatigue loads change due to the up-scaling?

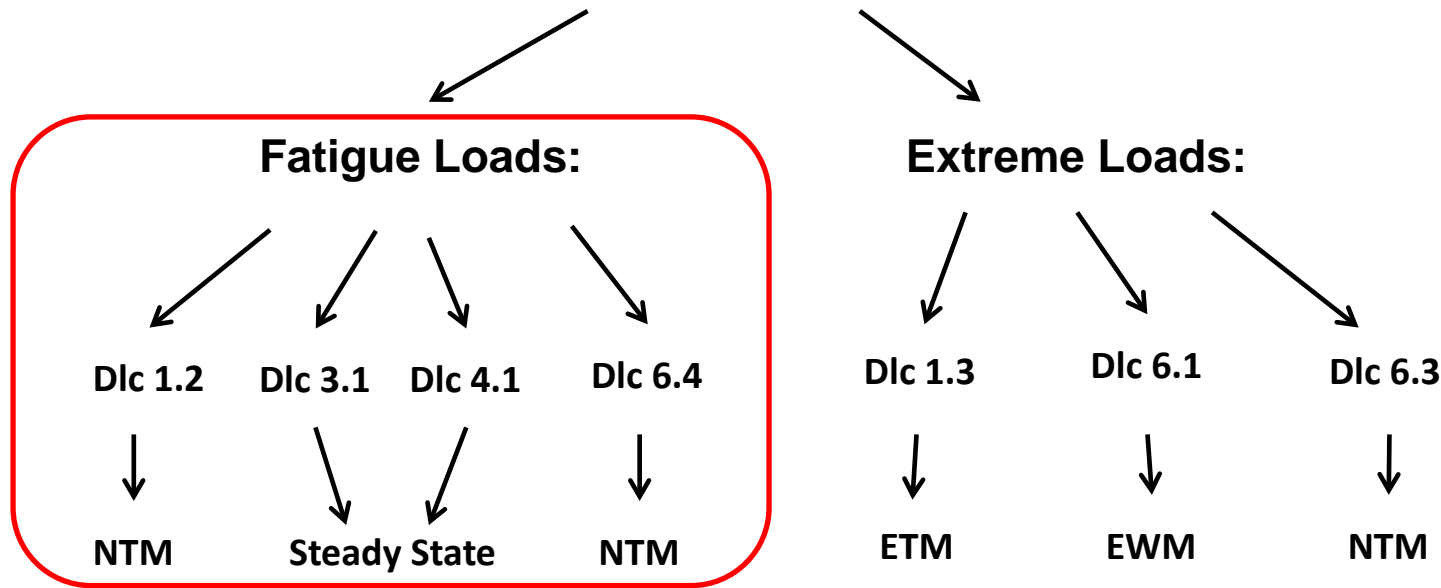
Boundaries of study:

- Reference WT is 3MW rated power, upwind, variable speed, and pitch regulated wind turbine
- Linear scaling method is applied to up-scale the reference model
 - Preserve the original tip speed ratio,
 - Geometry modifies linearly,
 - Aerofoils and materials are unchanged

Technology challenges:

- Changes of WT scale will require redesign of the control systems. It is important this can be done relatively quickly and efficiently perhaps in simplified way.
- However commercial designs will seek to reduce weight and cost using the new technology to avoid the mass penalties from scaling with similarity.
- This may be considered by looking at a few designs in 7-10 MW range using parameters considered representative of commercial designs.

Calculations:



- **Dlc 1.2** – design load case, WT is at power production range and connected to the electrical load at normal turbulence model (**NTM**). Wind speed $\in [4:2:24]$ with a mean yaw misalignment of $\pm 8^\circ$.
- **Dlc 1.3** – WT is running and connected to the electrical load at extreme turbulence model (**ETM**). Wind speed $\in [9.2, 11.2, 13.2, 20, 25]$.
- **Dlc 3.1** – WT starts up from standstill or idling to power production conditions.
- **Dlc 4.1** - WT normal shut downs from power production to a standstill or idling to conditions.
- **Dlc 6.1** – WT is at an idling condition (50 m/s) with a mean yaw misalignment of $\pm 8^\circ$ using the turbulent extreme wind model (**EWM**).
- **Dlc 6.3** – WT is at an idling condition (40 m/s) with extreme yaw misalignment of $\pm 30^\circ$ using the turbulent extreme wind model (**EWM**).
- **Dlc 6.4** – WT is at an idling condition (3, 30, 35 m/s) with a yaw misalignment of $\pm 8^\circ$ using the turbulent normal wind model (**NTM**).

Wind condition:

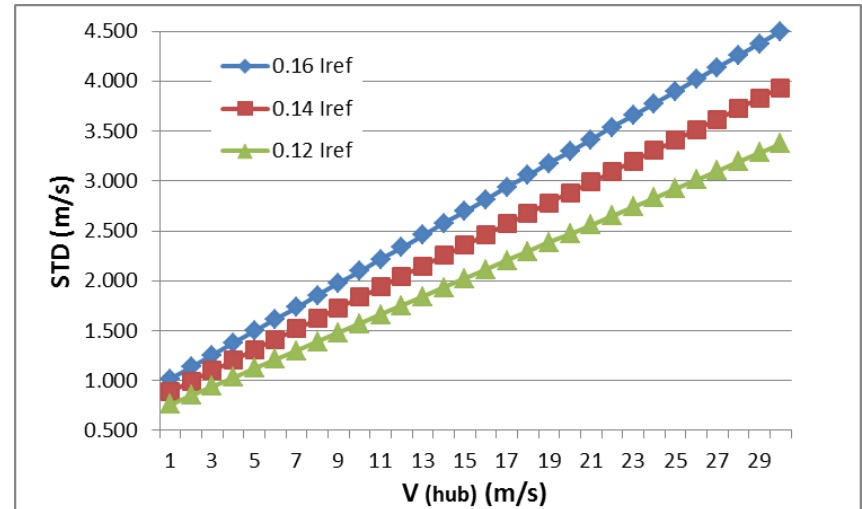
Wind turbulence was based on Kaimal:

Where, β is longitudinal scale parameter. $\beta = 0.7 * z$ if $z \leq 60m$ or $\beta = 42 m$ if $z > 60m$

- XLu is longitudinal direction or along the average wind flow velocity
- XLv is lateral or perpendicular to the longitudinal direction
- XLw is upward direction or perpendicular to both above mentions directions.

Axis components	XLu	XLv	XLw
Standard deviation	σ	$0.8 * \sigma$	$0.5 * \sigma$
Length scale	$8.1 * \beta$	$2.7 * \beta$	$0.66 * \beta$
Coherence decay constant	12		
Coherence scale parameter	$8.1 * \beta$		

Determination of parameters for Kaimal model



Normal Turbulence model (NTM):

$$\sigma_1 = I_{ref}(0.75V_{hub} + b); \quad b = 5.6 \text{ m/s}$$

Where, V_{hub} is wind speed at the hub height, σ_1 is a fixed turbulence standard deviation, I_{ref} is expected value of turbulence intensity at 15 m/s.

$I_{ref} = 0.16$ for high turbulence characteristics

$I_{ref} = 0.14$ for medium turbulence characteristics

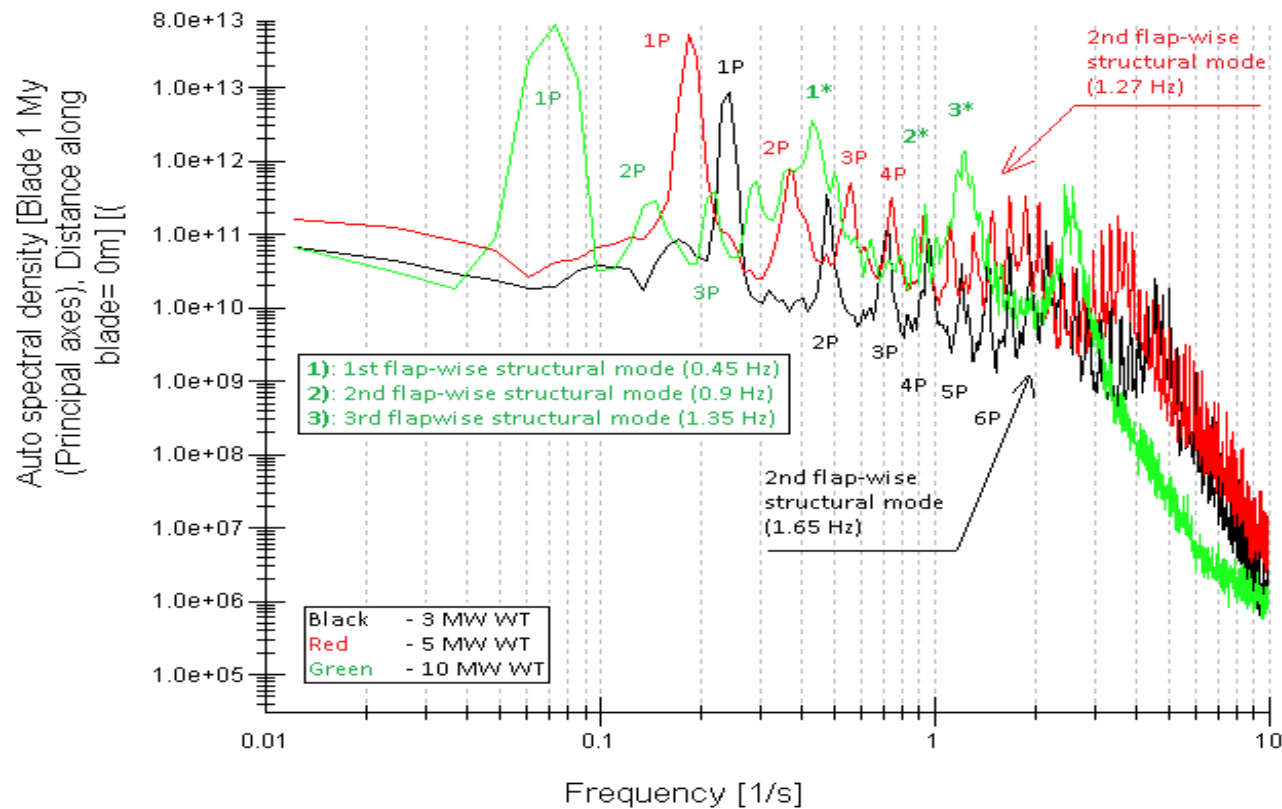
$I_{ref} = 0.12$ for low turbulence characteristics

Wind turbulence class	I	II	III
V_{ref} (m/s)	50	42.5	37.5

Accuracy of up-scaling

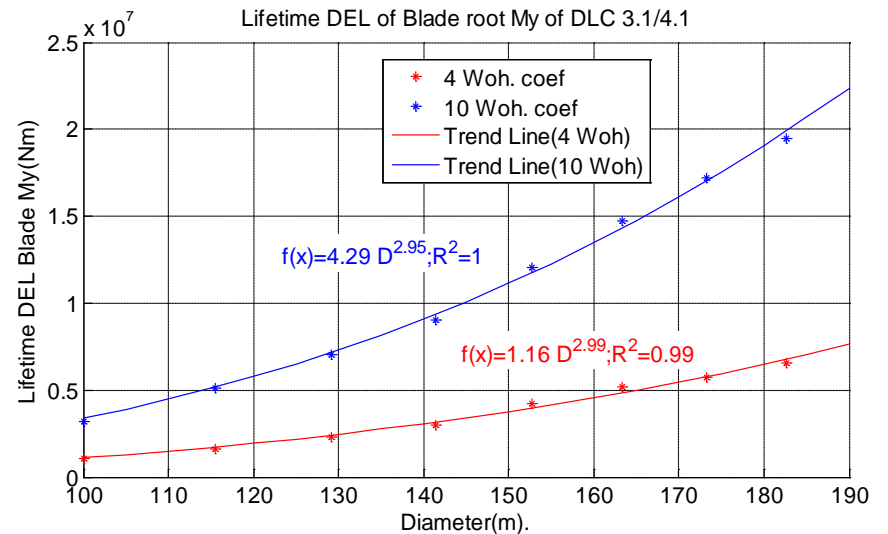
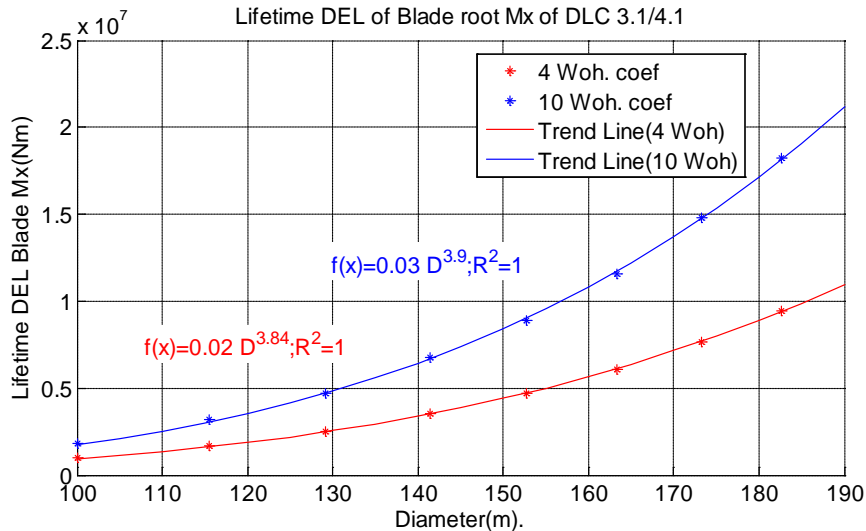
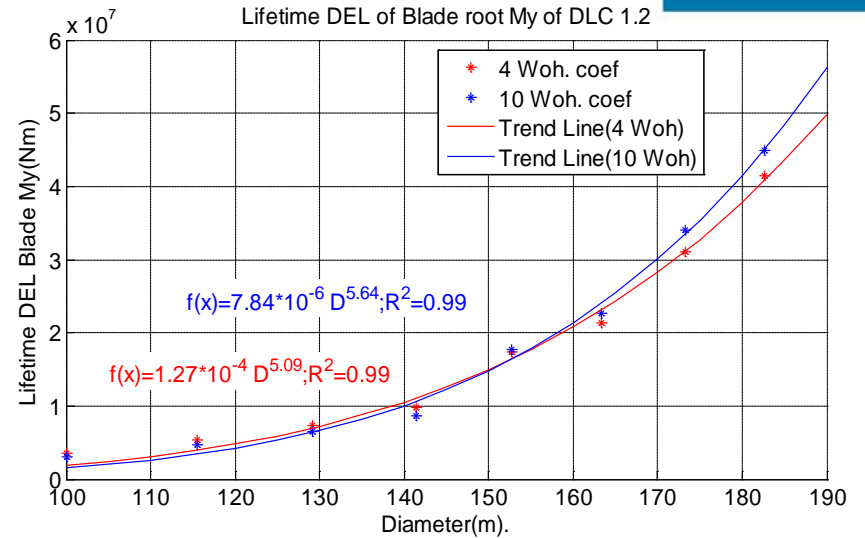
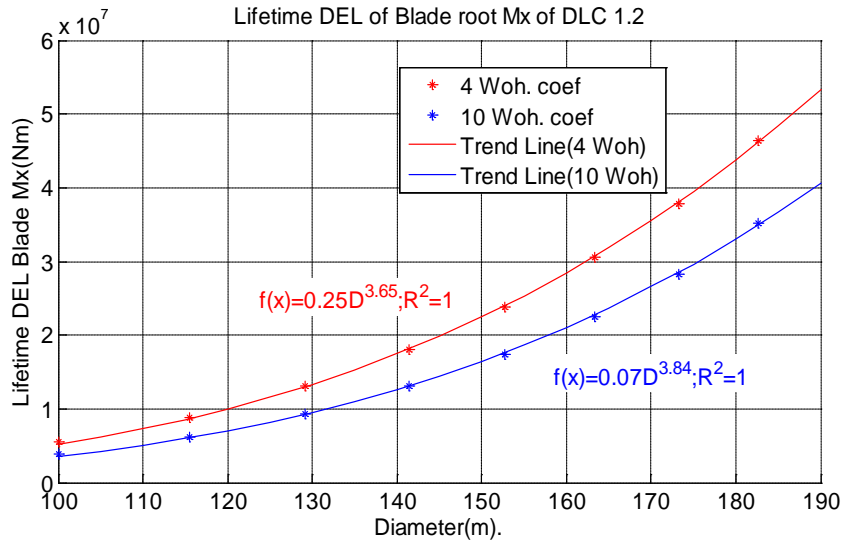
- Steady state and Auto spectra density

Fatigue calculations : **Dlc 1.2;**



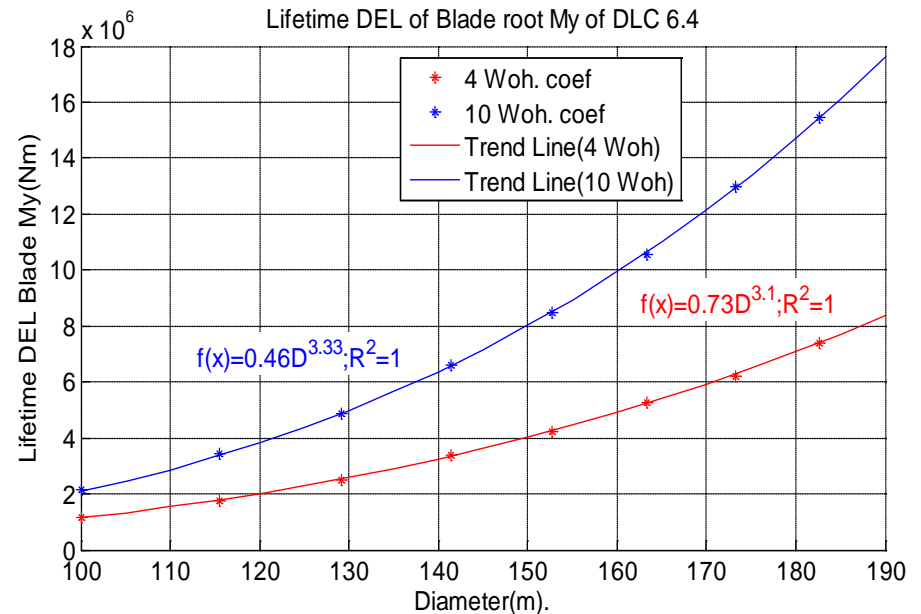
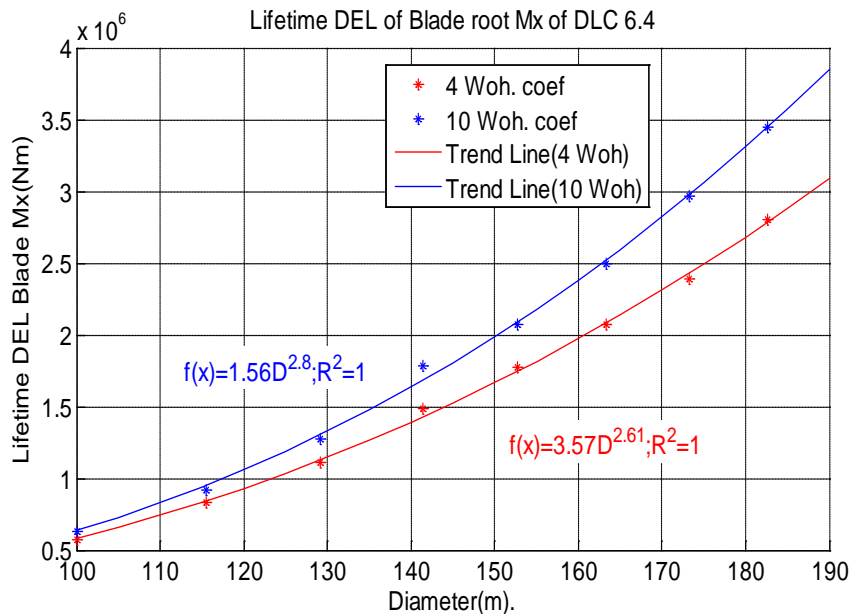
Lifetime DELs:

Fatigue loads calculations are **Dlc 1.2 , 3.1/4.1** ;



Lifetime DELs and Extreme Loads:

Fatigue loads (**Dlc 6.4**) ;



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Conclusion:

- The variation of the exponents of trend equations is reasonable at different DLCs , because the exponent is a product of the deterministic and stochastic loads. As a result the future work is required to divide the value exponent onto deterministic and stochastic parts by switching off one part loads in the simulations of DLCs .

Future work:

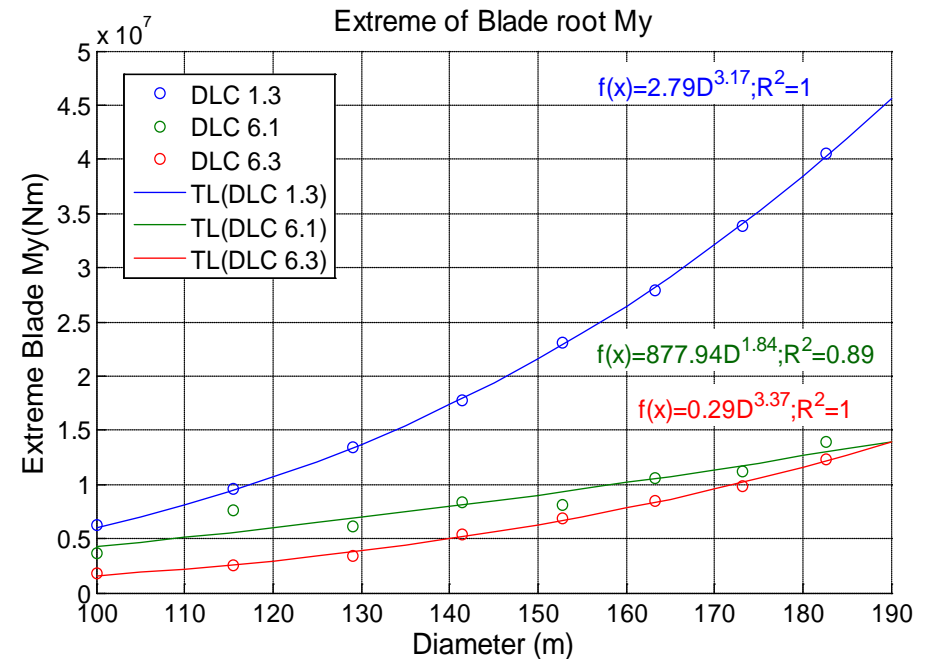
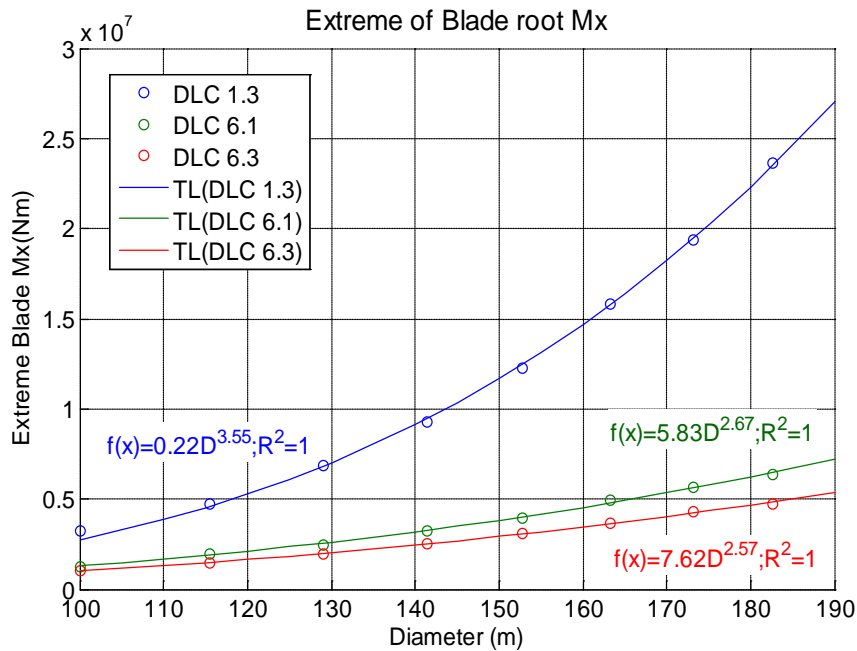
- Run simulations without the deterministic part of loads.
- Investigate the impact from:
 - Wind conditions
 - TSR
 - Rotor solidity



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Lifetime DELs and Extreme Loads:

Extreme (Dlc 1.3, 6.1, 6.3)



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