



KATHOLIEKE UNIVERSITEIT
LEUVEN



Modeling and control of Multi-terminal VSC HVDC Systems

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- PhD projects
 - VSC HVDC in AC meshed grids (Stijn Cole, finished 2010)
 - Integration of Multi-terminal VSC HVDC (Jef Beerten)
 - Optimal investment strategies for offshore wind (Hakan Ergun)
 - ...

- Projects (2006 – ...)
 - Randstad HVDC (2006 – 2007)
 - BelGer – Nemo (2006 – 2007)
 - Imera power (2007 – 2009)

- Member of CIGRE WG on HVDC (2006 – ...)
 - B4.46 – Economic Aspects of VSC HVDC
 - B4.52 – DC Grids Feasibility Study
 - B4.58 – Load flow and Direct Voltage Control in a HVDC Grid
 - B4/B5.59 – Control and Protection of HVDC Grids
 - C4/B4/C1 - Influence of Embedded HVDC Transmission on System Security and AC Network Performance

- Master thesis (2008 - ...)
 - Loss minimization (Gilles Daelemans*)
 - Economics of AC and DC wind farm connections (Bram Van Eeckhout*)
 - MTDC protection (Kenny De Kerf*)
 - Connecting Belgium and the UK (Frederik Leung Shun*)
 - VSC HVDC Connected variable speed operated wind farms (Pieter Hellings)
 - DC voltage control (Carlos Dierckxsens*)
 - HVDC connected large-scale solar plants (Philippe Hoylaerts*)
 - Multi-terminal HVDC and wind (Stijn Vandenbroucke*)

*: *in cooperation with ABB Sweden*

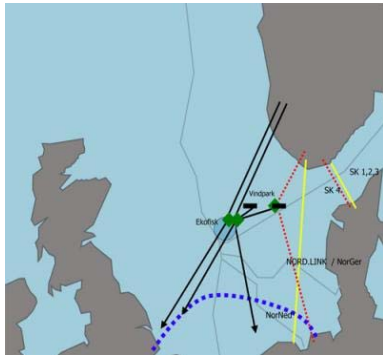
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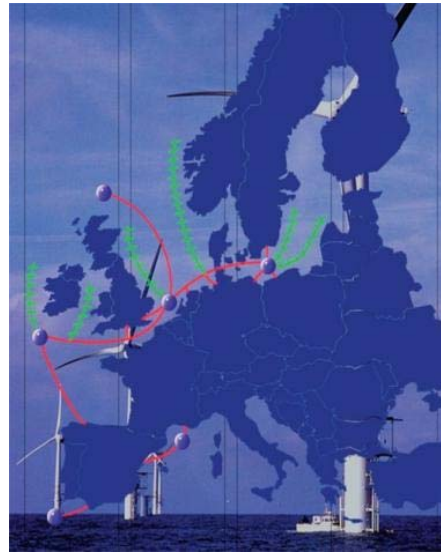
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Offshore grids and supergrid ...

What will the future grids look like?

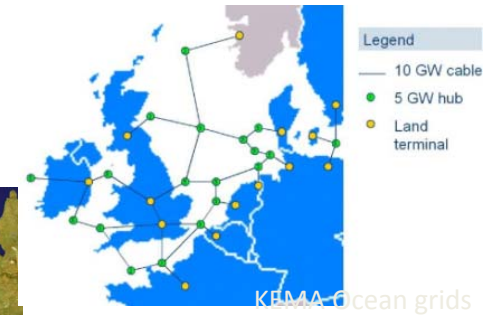
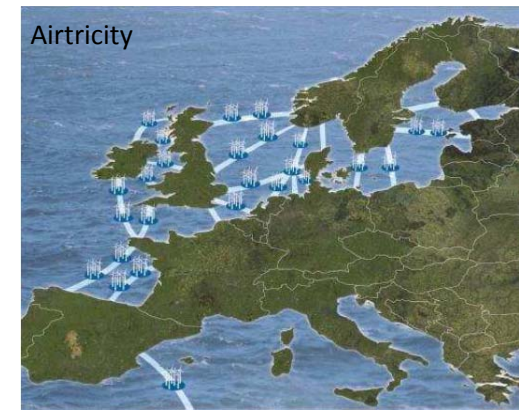
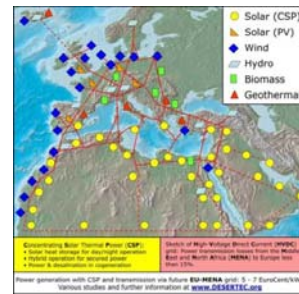


Offshore Grid Proposal by Statnett
(Source Statnett, 2008)



Vision of High Voltage Super Grid
(Source: Dowling and

FIGURE (22): Possible meshed HVDC (meshed 2) connection of offshore wind farms. Dotted lines are HVDC interconnectors. NorHed2 and NorGer are replaced by a HVDC connections between Norwegian and German offshore wind farms.



Offshore Grid examined in the Greenpeace study
(Source: Woyte et al, 2008)

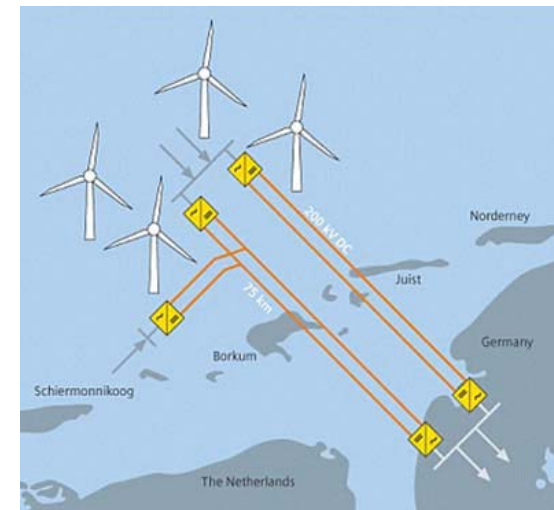
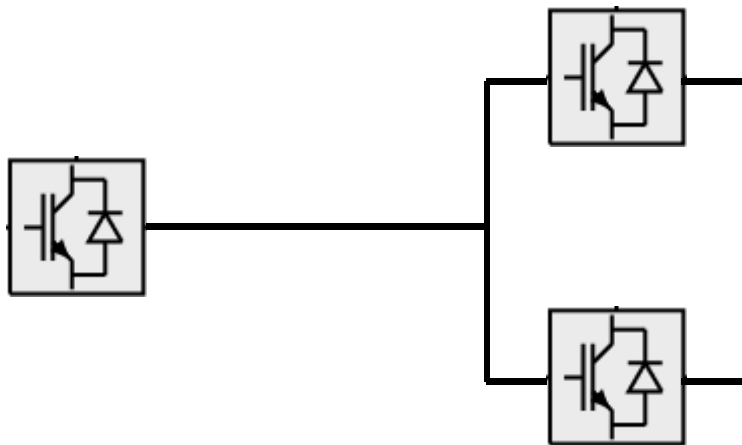


Czisch – Supergrid for renewable energies



Desertec

- VSC HVDC only developed for point-to-point, but...
- ...looks very promising for future DC grids
 - Converter's DC side has constant voltage → converters can be easily connected to DC network.
- Extension to 'pseudo-multi-terminal' systems straightforward: e.g. star-connections



- DC Voltage \approx AC frequency
 - Changes when ‘consumption’ \neq ‘production’

- Can different converters contribute to the DC voltage control?



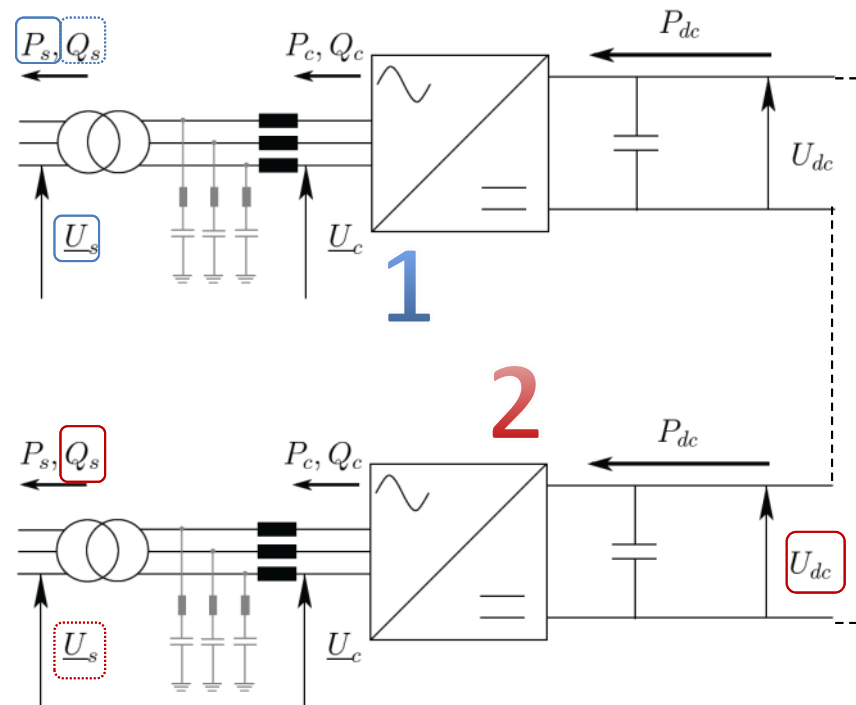
Converter control principles

- **2-terminal scheme**

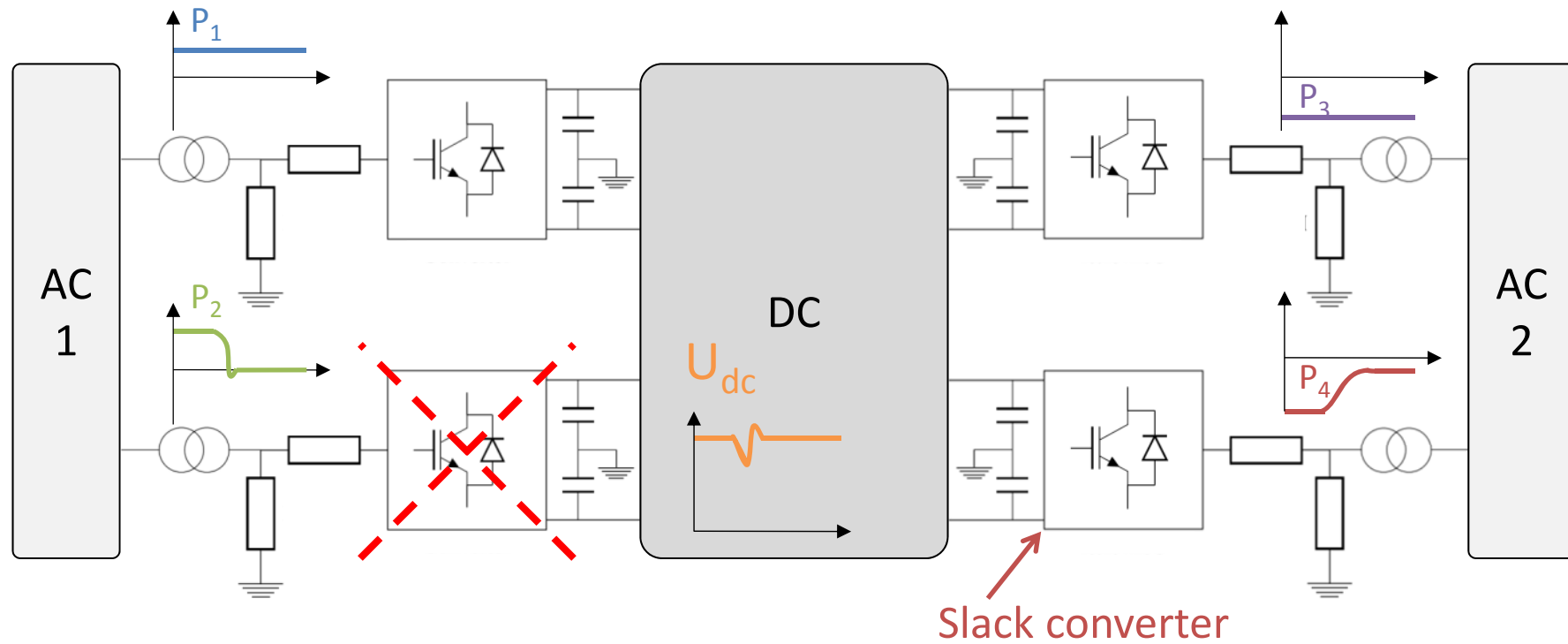
- Active power control
 - converter 1
- DC voltage control
 - converter 2

- Reactive power control
 - converter 1 and/or 2
- AC voltage control
 - converter 1 and/or 2

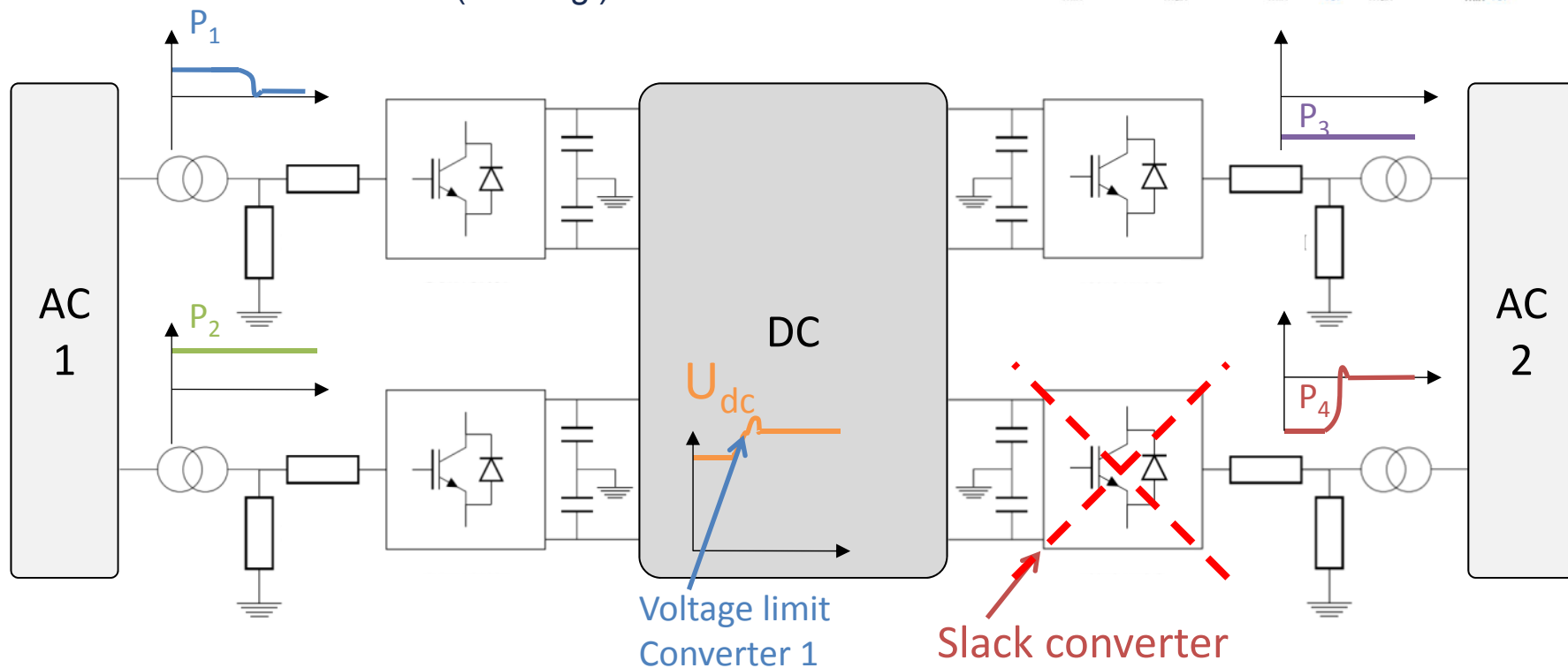
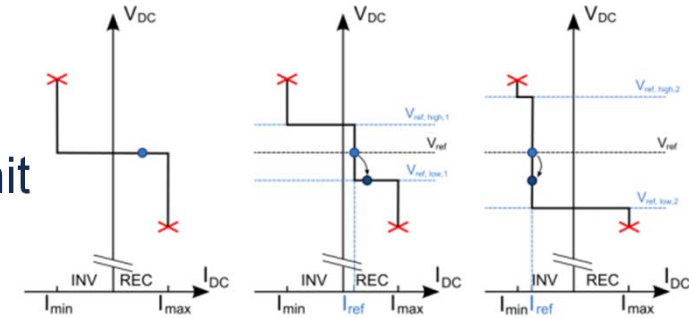
Example:



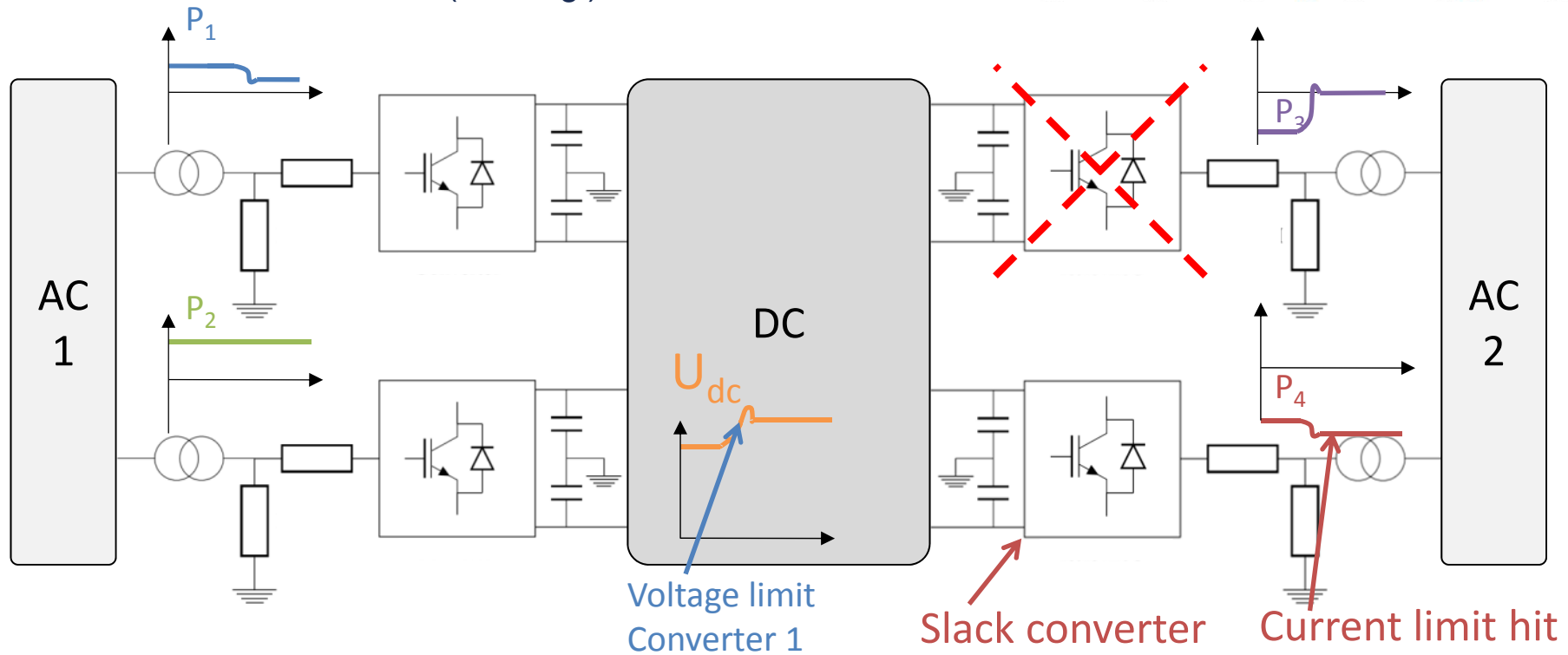
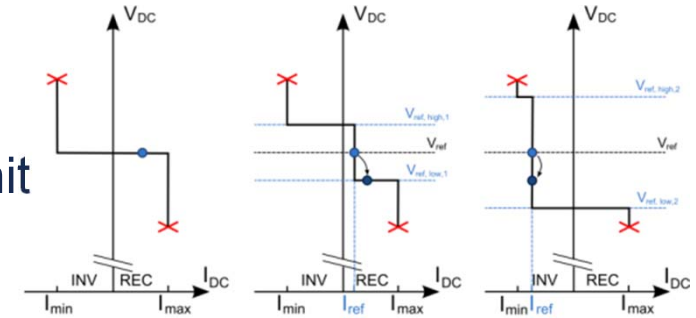
- 1 DC voltage controlling converter
 - Converter has to deal with all DC grid events
 - What if this converter fails?
 - Which TSO wants this ‘DC slack bus’?



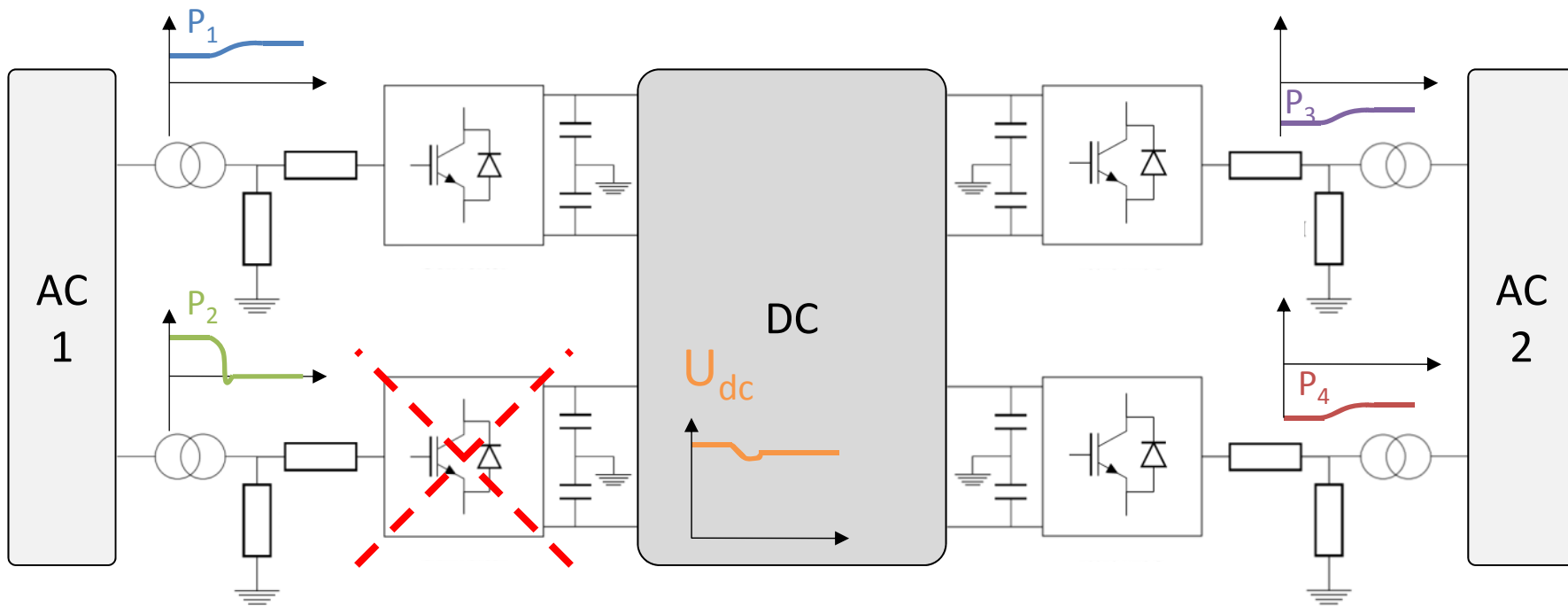
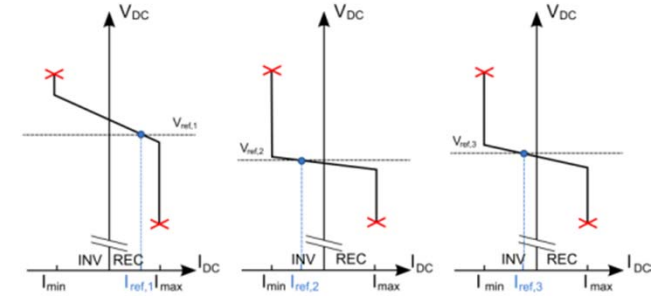
- Improved master-slave approach
 - 1 DC voltage controlling converter at a time
- Converter takes over when margins/limits hit
 - Voltage limits (slack outage)
 - Current limits ('sharing')



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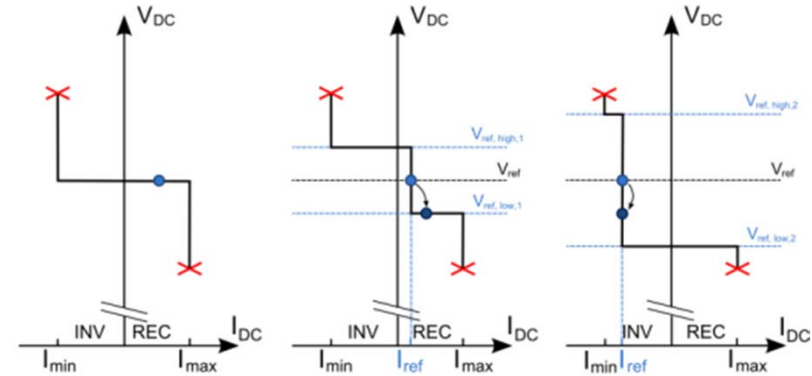
- Distributed DC voltage control
 - Often referred to as ‘distributed slack bus’
 - Based on DC voltage droop



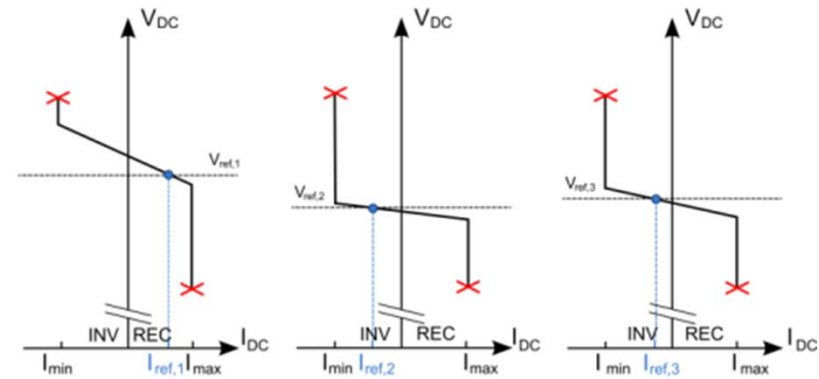
Power or DC voltage control?

Control objectives

- P_{ac} constant
- P_{dc} constant
- U_{dc} constant



- U_{dc} distributed control
 - $U_{dc} - I_{dc}$ droop
 - $U_{dc} - P_{dc}$ droop
 - $U_{dc} - P_{ac}$ droop



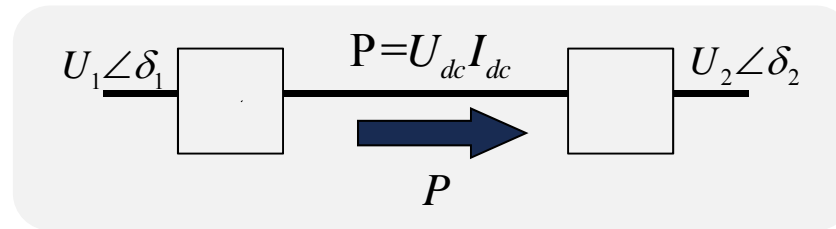
- ...

- Steady-state (power flow control)
 - Effect on AC and DC power flows
 - Overall grid state after disturbance
 - N-1 contingency analyses
 - DC voltage droop settings (primary control)
 - Starting point for restorative actions (secondary control)

- Dynamics
 - AC and/or DC system interactions (transient stability)
 - Fast converter dynamics + switching (EMTP)

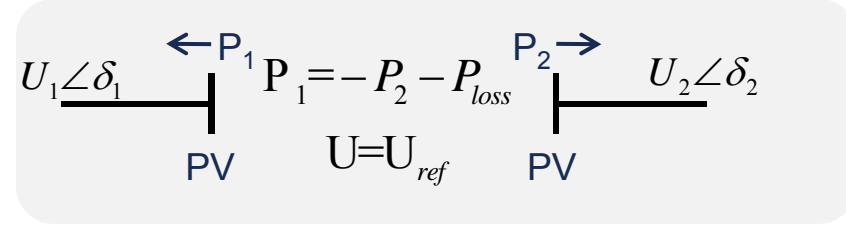
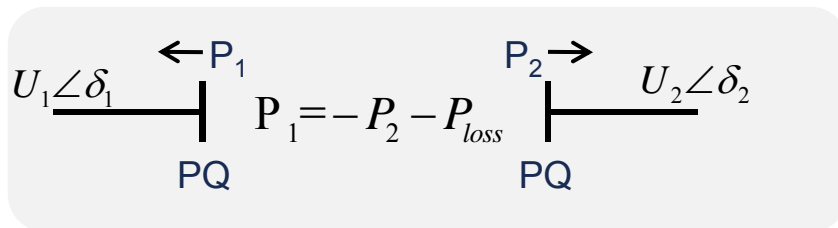
Different time scales

→ different programs and modeling requirements



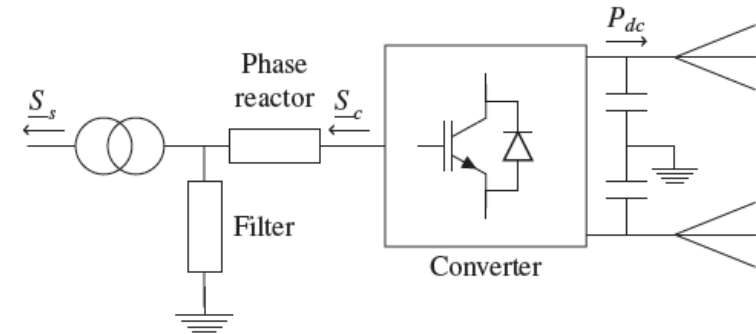
Simplified model

- represent converter as PQ or PV node
- one converter positive active power, second one negative active power



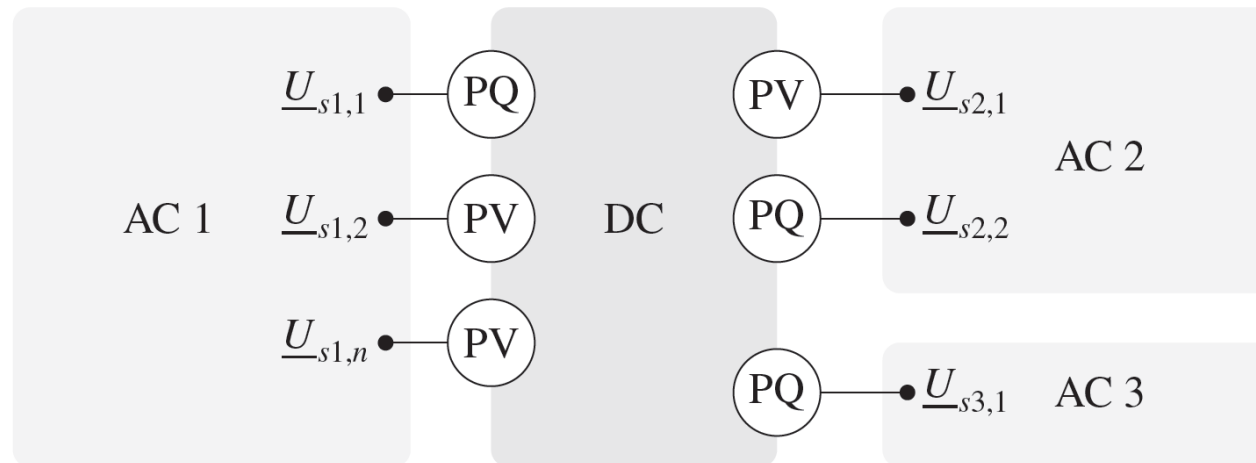
- **Combined/unified approach (AC+DC)**

- Solution of AC and DC grid together
- Extension of Jacobian matrix
- *Only one iterative problem*



- **Sequential approach (AC, DC)**

1. Use DC grid variables as inputs to solve the AC equations
 2. Use AC grid variables as inputs to solve the DC equations
- *Easy extension of existing power flow programs*



- DC grid power flow equations:

$$P_{dc_i} = 2 U_{dc_i} \sum_{\substack{j=1 \\ j \neq i}}^n Y_{dc_{ij}} \cdot (U_{dc_i} - U_{dc_j})$$

with power-voltage droop

$$P_{dc_i} = P_{dc,0_i} - \frac{1}{k_i} (U_{dc_i} - U_{dc,0_i})$$

$$I_{dc_i} = \sum_{\substack{j=1 \\ j \neq i}}^n Y_{dc_{ij}} \cdot (U_{dc_i} - U_{dc_j})$$

with current-voltage droop:

$$I_{dc_i} = I_{dc,0_i} - \frac{1}{k_i} (U_{dc_i} - U_{dc,0_i})$$

- Defining modified active power vector,

$$X_{dc} = [\underbrace{P_{dc_1}}_{\text{slack}}, \underbrace{P_{dc_2} \dots P_{dc_k}}_{P\text{-control}}, \underbrace{I_{dc,0_{k+1}} \dots I_{dc,0_l}}_{U-I \text{ droop}}, \underbrace{P_{dc,0_{l+1}} \dots P_{dc,0_m}}_{U-P \text{ droop}}, \underbrace{0 \dots 0}_{\text{outage}}]^T$$

- the set of equations can be solved using a NR iteration.

$$\left(U_{dc} \frac{\partial X_{dc}}{\partial U_{dc}} \right)^{(j)} \cdot \frac{\Delta U_{dc}^{(j)}}{U_{dc}} = \Delta X_{dc}^{(j)} \quad \Delta X_{dc}^{(j)} = \begin{cases} P_{dc_i}^{(k)} - P_{dc_i}(U_{dc}^{(j)}) & \forall i: 2 < i \leq k \\ I_{dc,0_i} - I_{dc,0_i}(U_{dc}^{(j)}) & \forall i: k \leq i \leq l \\ P_{dc,0_i} - P_{dc,0_i}(U_{dc}^{(j)}) & \forall i: l \leq i \leq m \\ -P_{dc_i}(U_{dc}^{(j)}) & \forall i: m < i \leq n \end{cases}$$

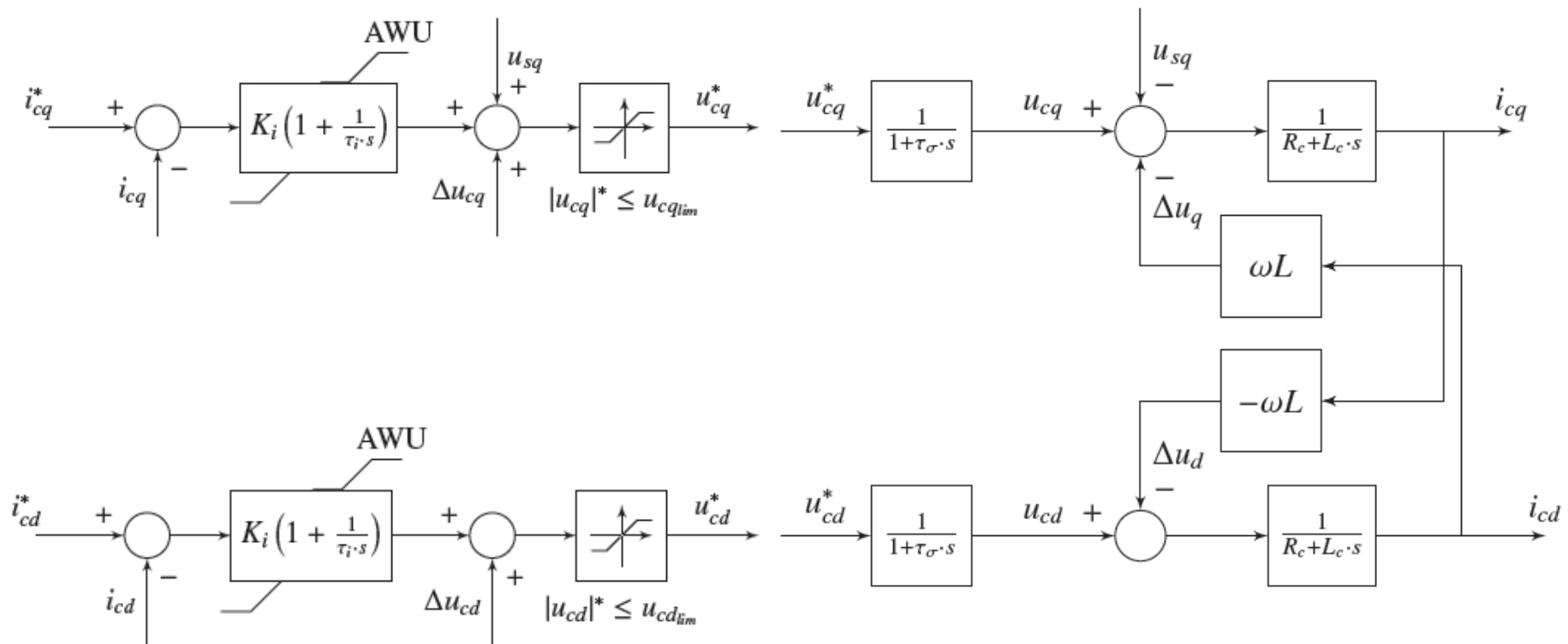
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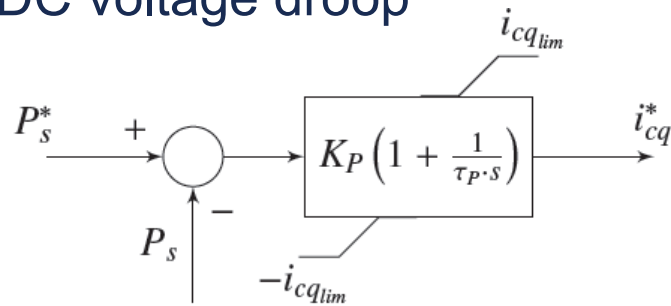
Different time scales

→ different programs and modeling requirements

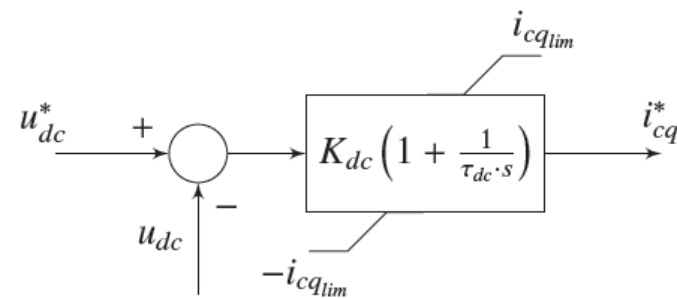
- Converter dynamics
- Power electronics time delay
- Decoupled current control (limits and AWU)



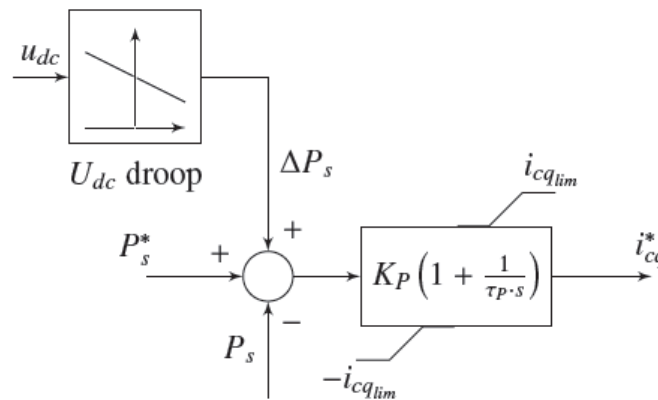
- Outer q control loop
 - Constant active power control
 - Constant DC voltage control
 - DC voltage droop



(a) Constant P_s controller

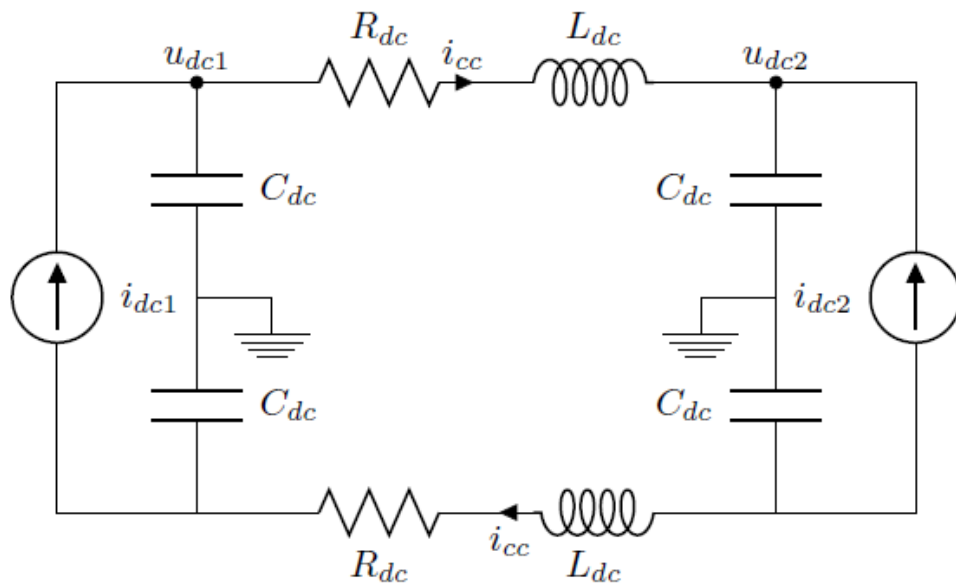


(b) Constant U_{dc} controller



(c) U_{dc} droop controller

- DC grid model
 - Pi equivalent with lumped parameters

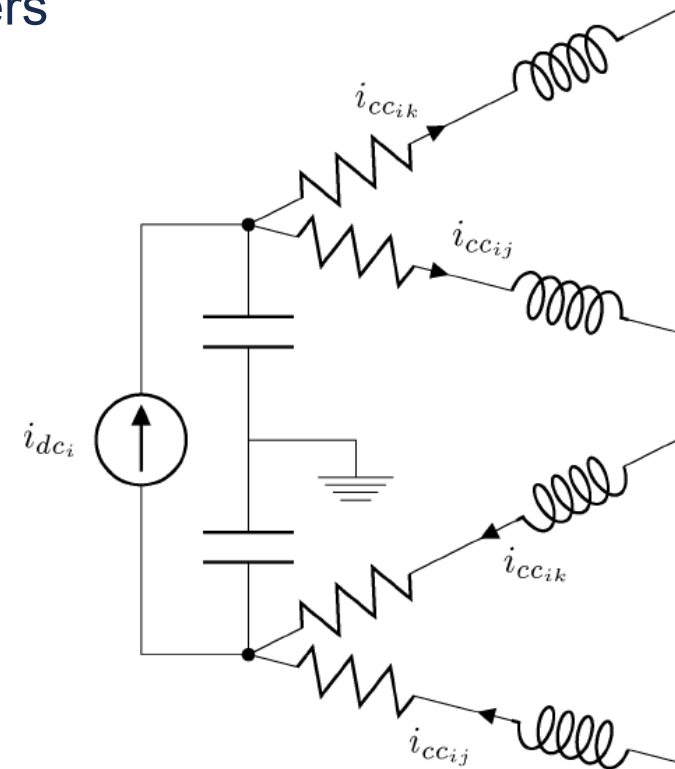


$$C_{dc} \frac{du_{dc1}}{dt} = i_{dc1} - i_{cc},$$

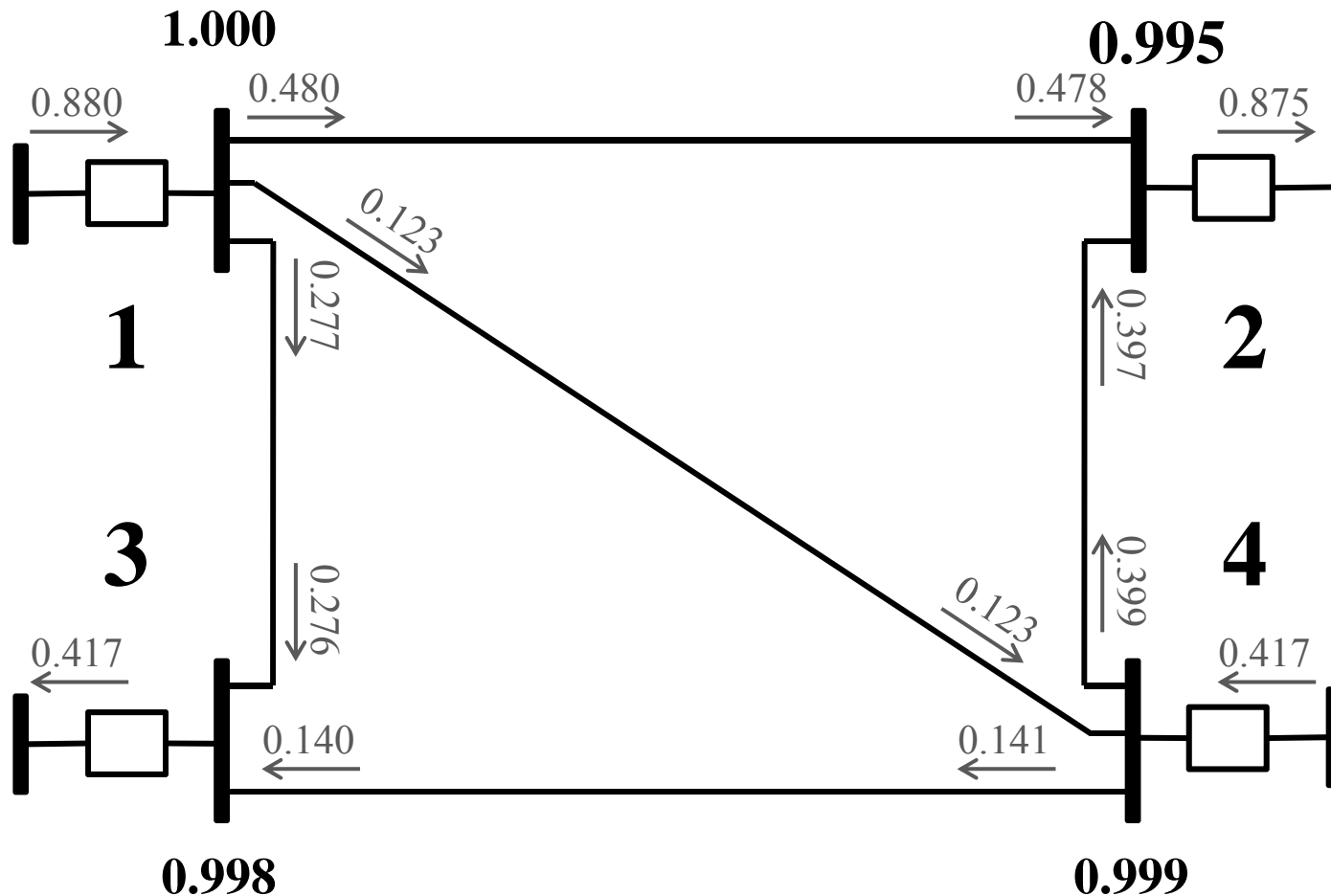
$$C_{dc} \frac{du_{dc2}}{dt} = i_{dc2} + i_{cc},$$

DC line dynamics:

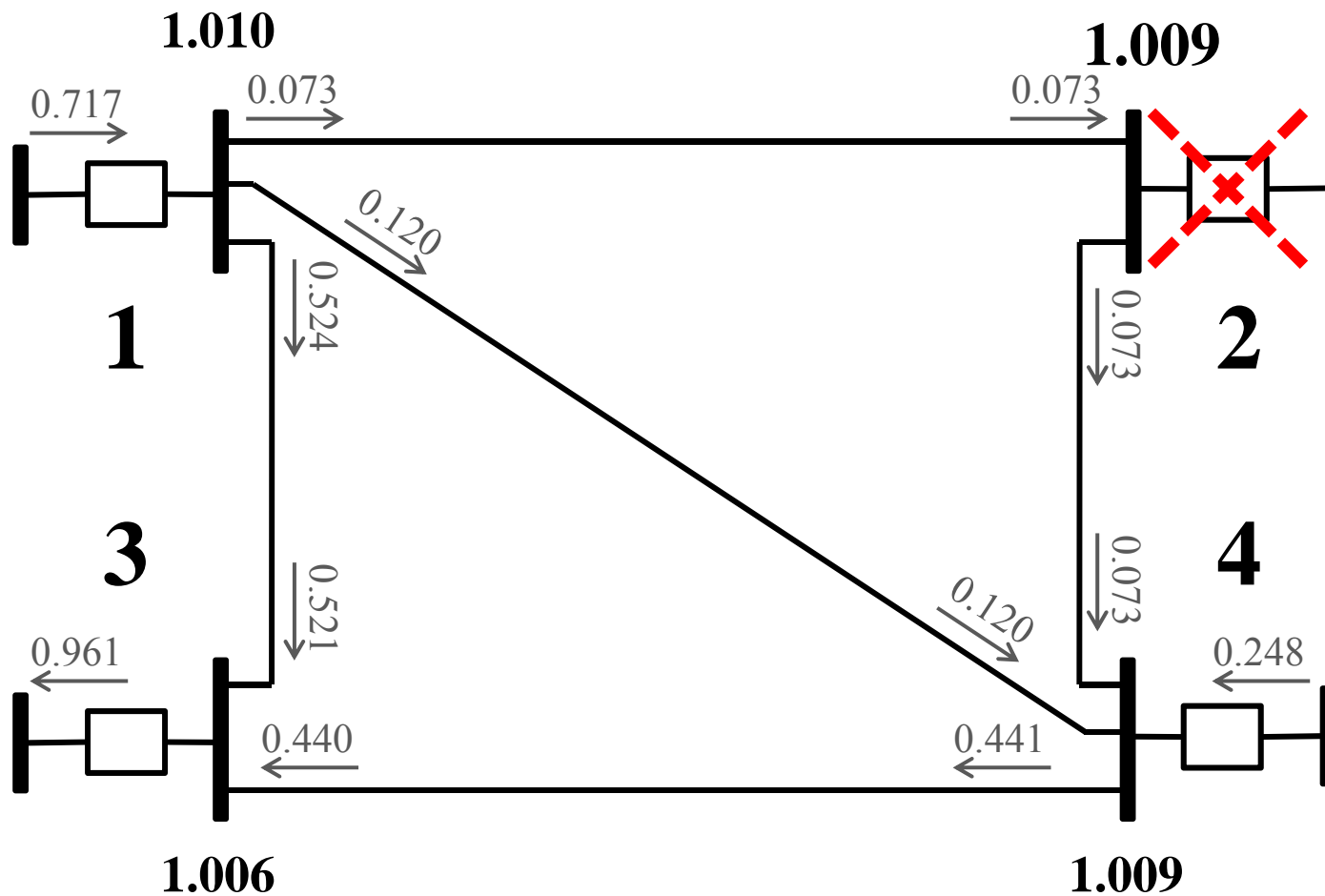
$$L_{dc} \frac{di_{cc}}{dt} = u_{dc1} - u_{dc2} - R_{dc}i_{cc}.$$

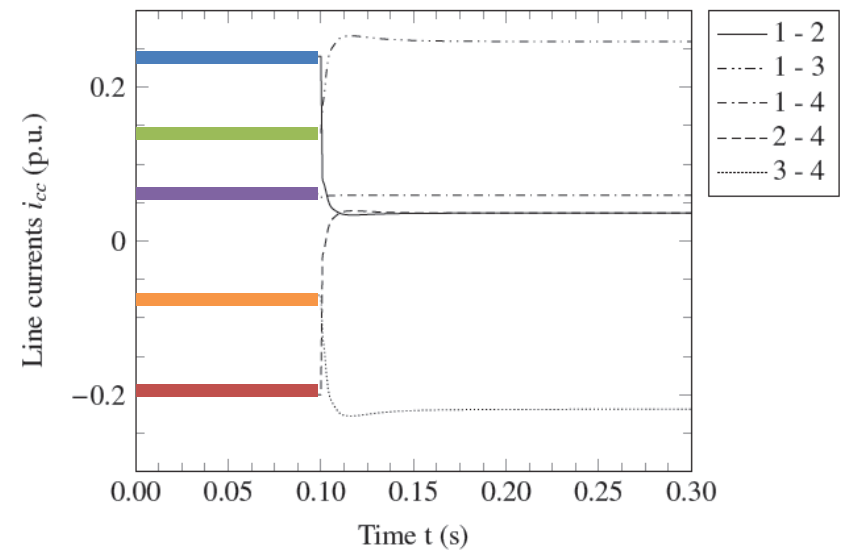
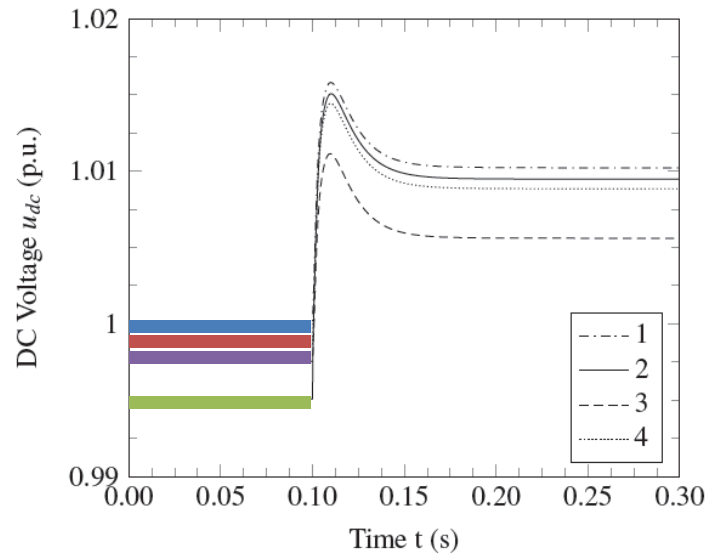
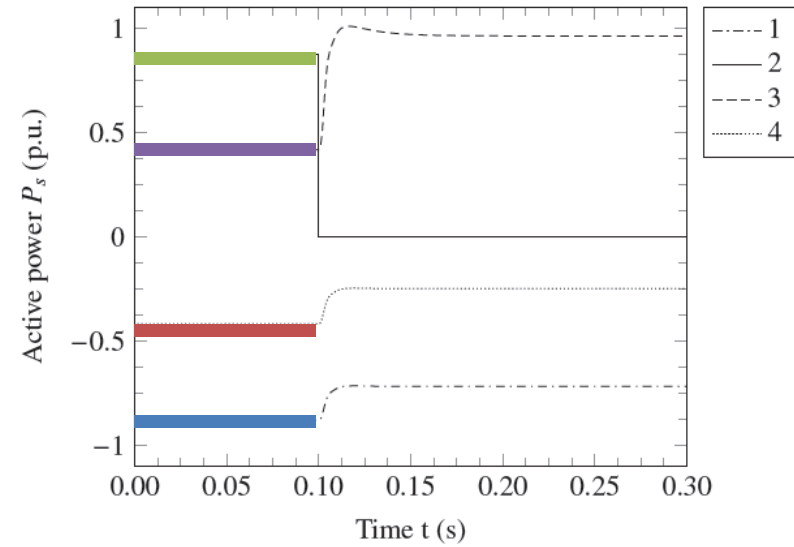
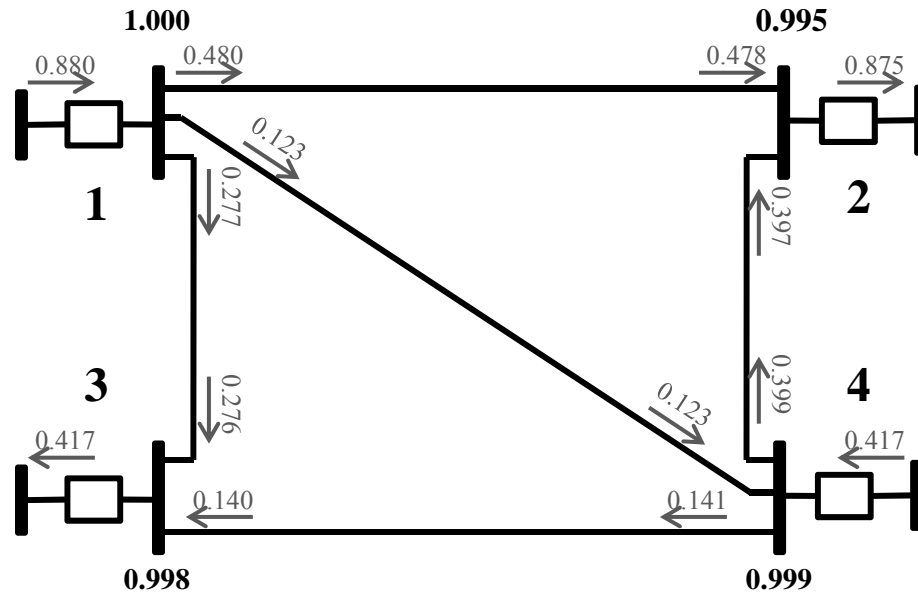


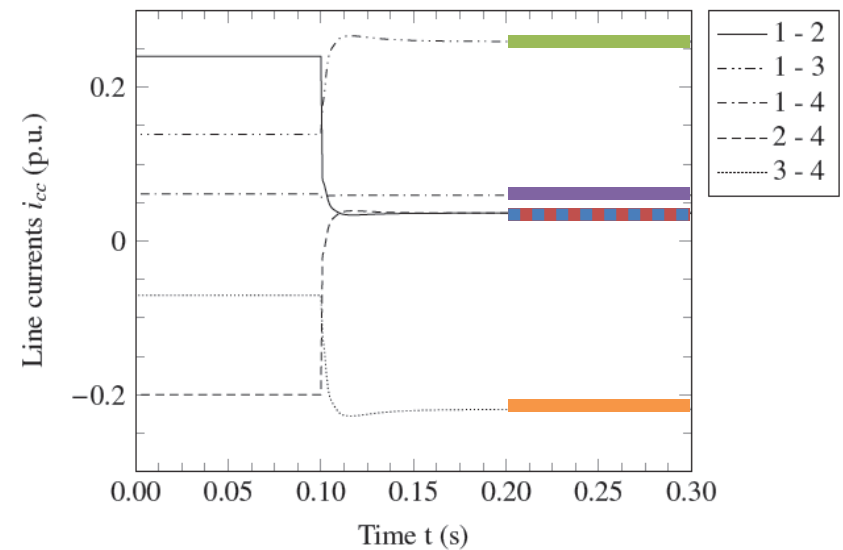
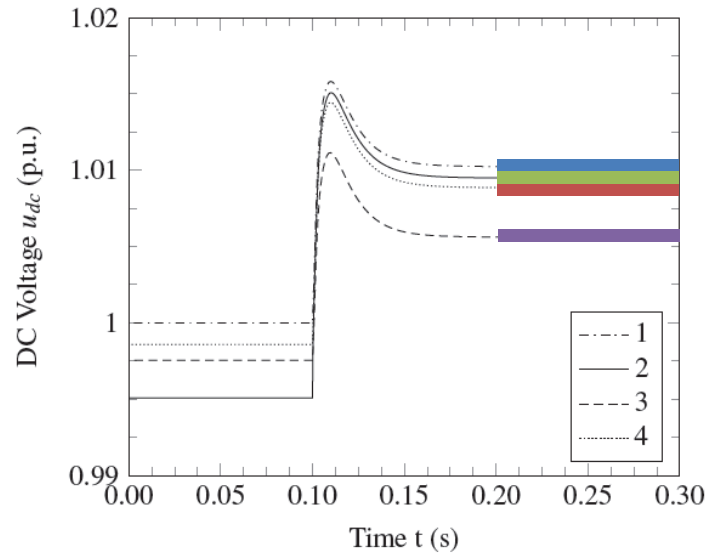
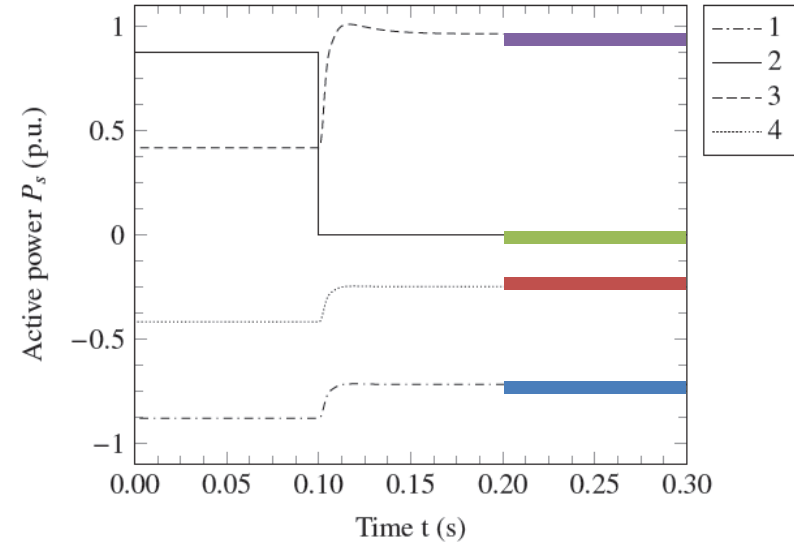
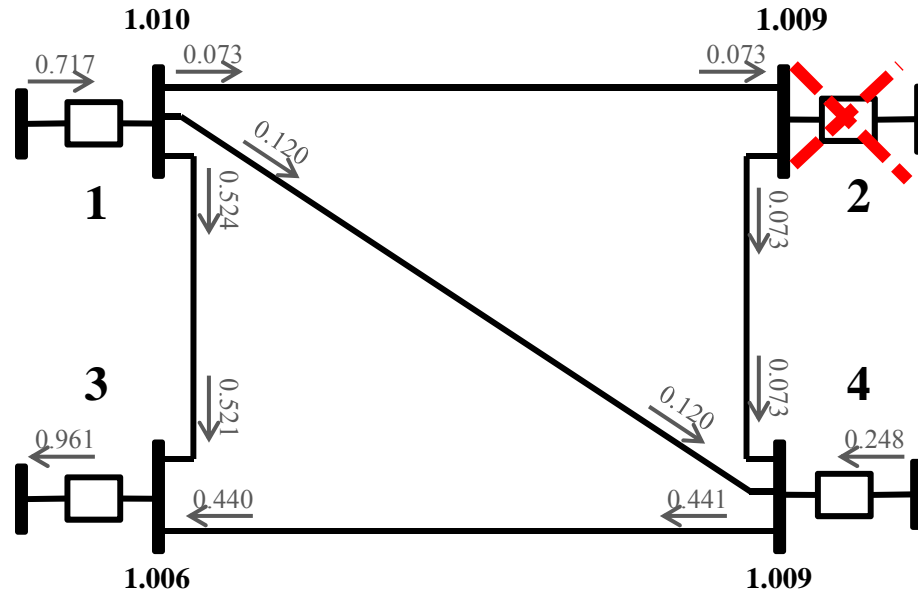
- DC power flow before converter outage



- DC power flow **after** converter outage







- Steady-state and dynamic models serve different purposes
 - Power flow algorithms allow to study the post-disturbance effect of control strategies, droop values, limits, ... on the steady-state powers and voltage.
 - Transient models allow to study the dynamic interactions between the converters and the dynamic effect of control schemes, droop values, limits, ...
- When properly modeled, the results of the power flow analysis are in line with the steady-state post-disturbance dynamic results.