

MODELING OF FULL SCALE OXY-FUEL CEMENT ROTARY KILN

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SINTEF Energi AS

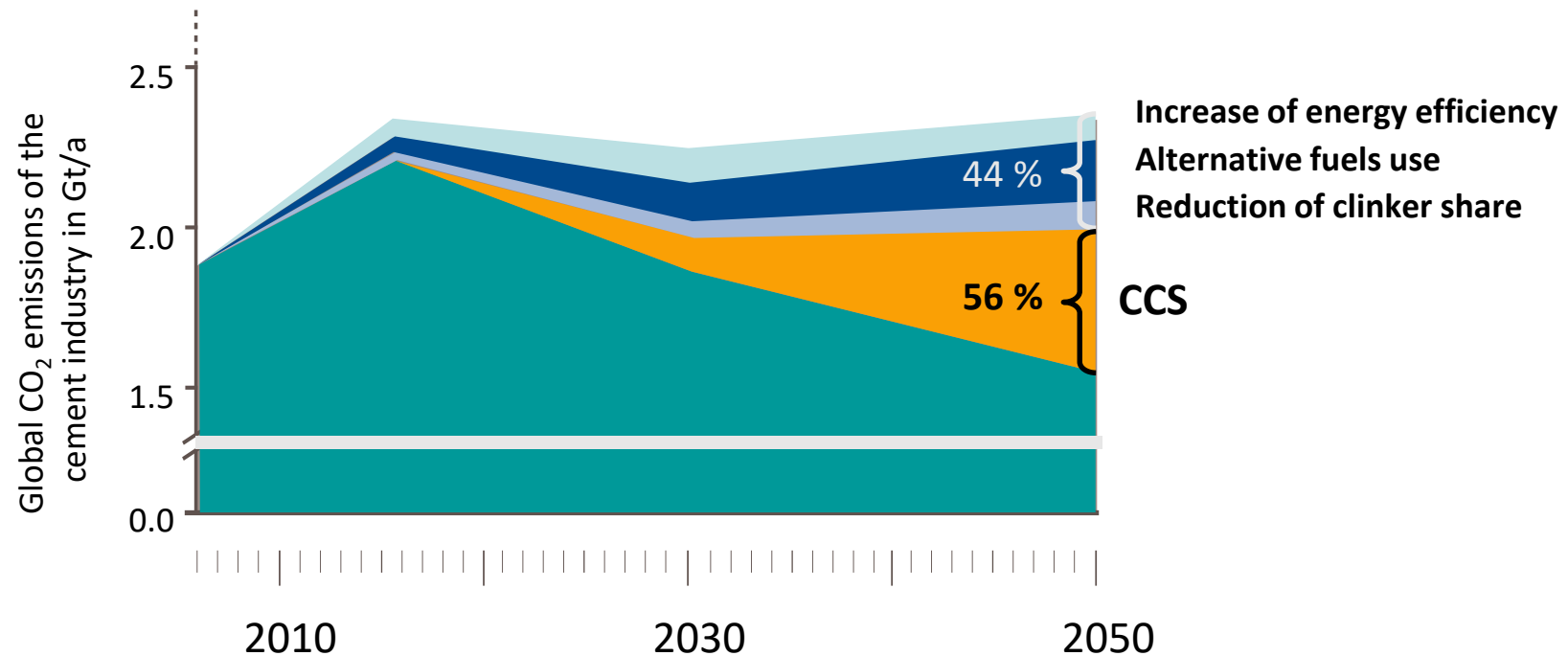
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- Methodology for optimization of the process modeling by integrating the CFD
- Full scale rotary cement kiln setup
- Results
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Introduction

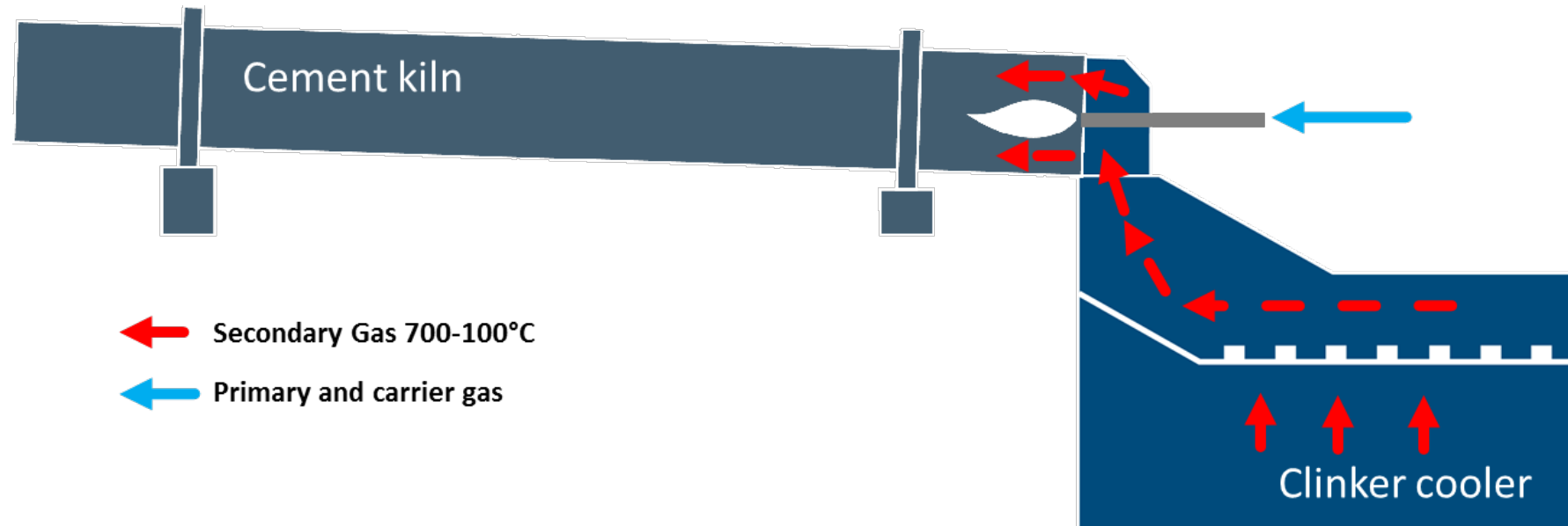
CO2 emissions reduction targets from cement production



Source: IEA Cement Roadmap

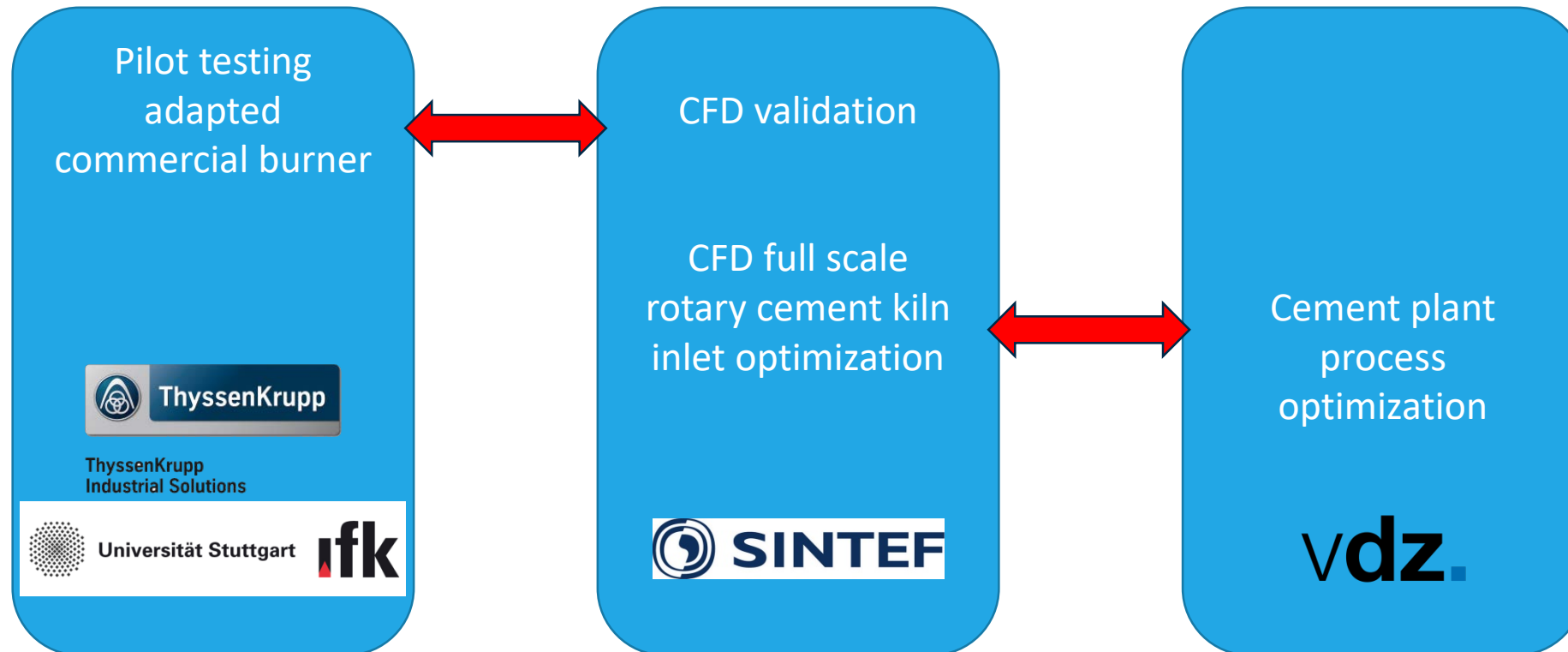
Introduction

Cement rotary kiln



- Preheating of secondary gas
- Dry secondary gas

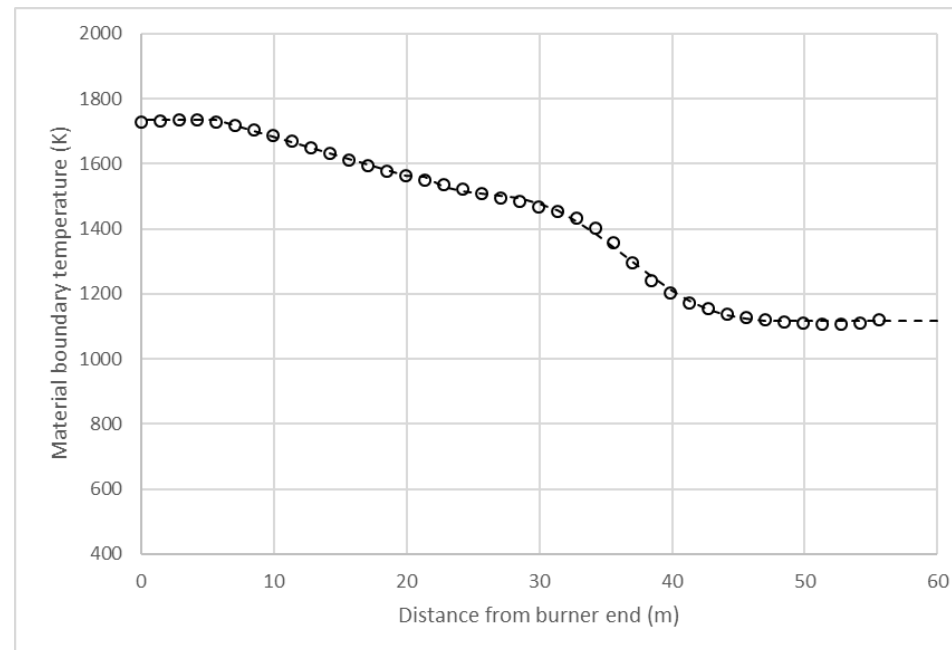
CEMCAP - oxy-fuel combustion



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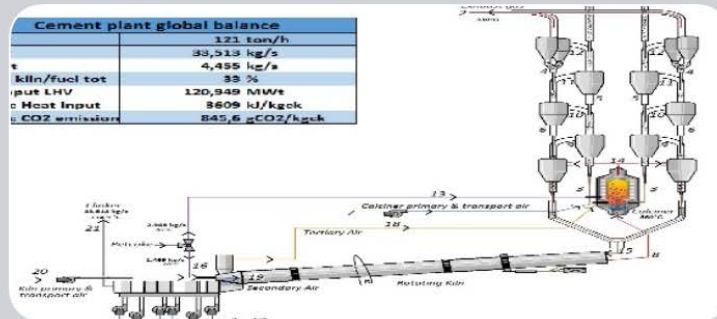
Optimization methodology

- Objective of optimization: achieve a flame generating a heat profile in the kiln comparable to that of the reference BAT case: the material temperature profile must be preserved
- Reference BAT case: AIR



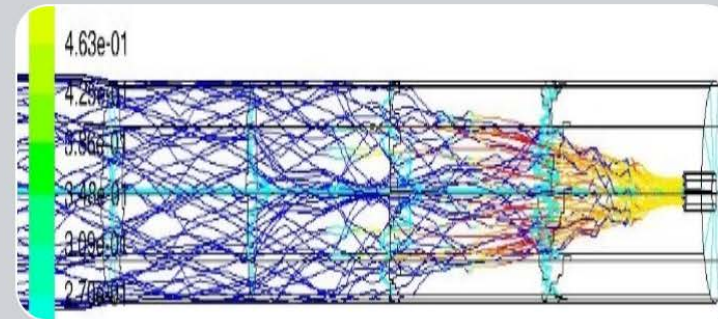
CEMCAP - oxy-fuel combustion

Optimization methodology



Process Modelling of Cement Plant (WP6)

- Kiln modelled as 1D with 40 cells
- Solves mass and energy balance, and material transformation across the whole plant

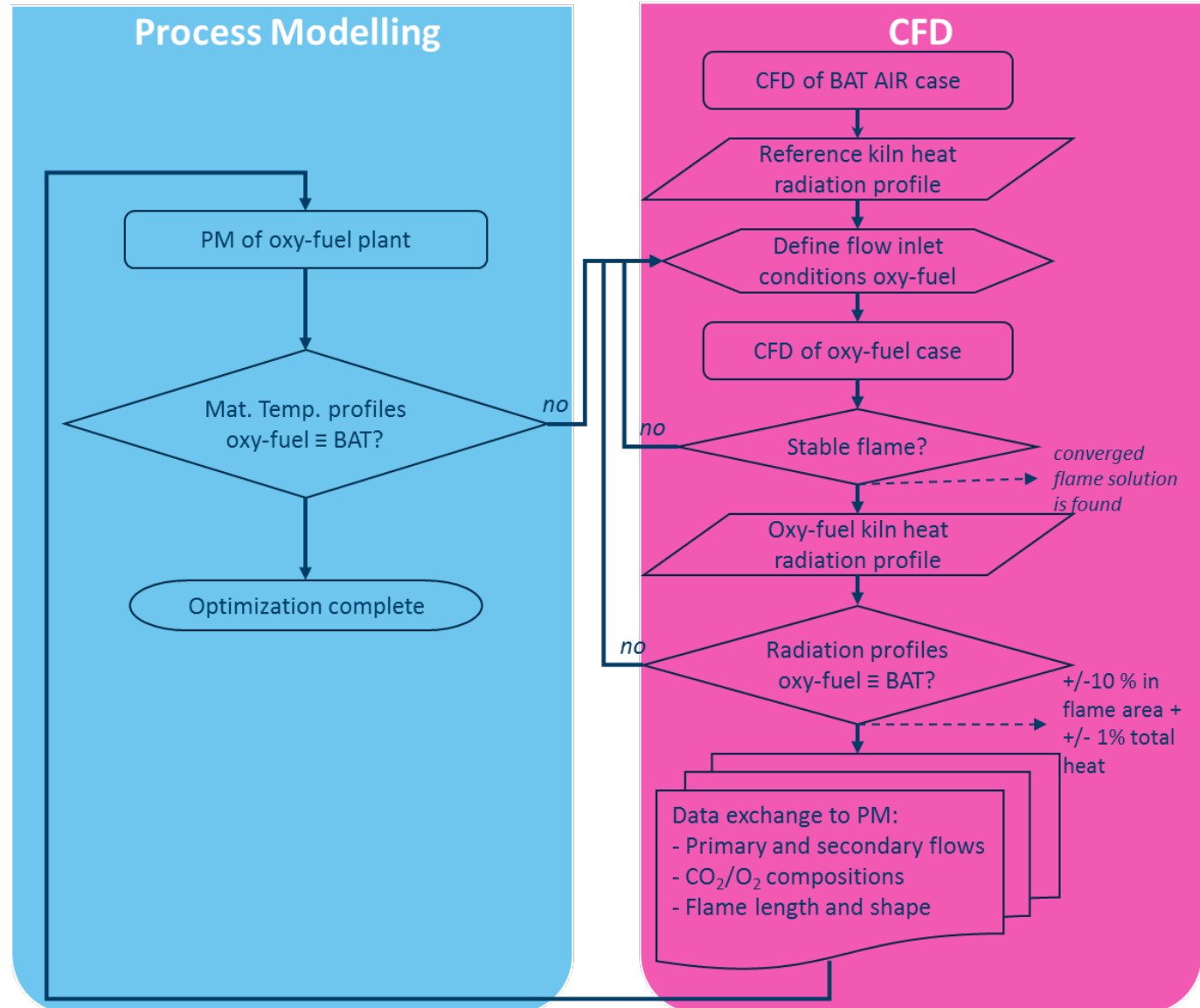


CFD of Rotating kiln (WP7)

- Kiln modelled as 3D with 16 millions cells
- Solves the turbulent fluid mechanic and combustion kinetic equations in the flame

CEMCAP - oxy-fuel combustion

Data exchange and process optimization



CEMCAP - oxy-fuel combustion

Constraints in the process optimization

Parameter	Constraint
O₂ % in primary stream	None
CO₂/O₂ composition in carrier stream	0% - 35 %
Primary / secondary flow	0.1 – 0.15
Primary CO₂ flow rate	No limitations, but overall efficiency will decrease with an increase of cold primary flow
Secondary CO₂ flow rate	34,000 to 40,000 Nm ³ /h
Total primary	None
Overall kiln lambda	1 - 3 % O ₂ in dry flue gases
Burner swirl angle	None
Velocities at burner outlets	
Nozzles	150 – 250 m/s, preferably greater than 200 m/s
Secondary	3 – 6 m/s
Carrier gas	15 – 20 m/s
Burner hardware	During the optimization step, a suggestion for burner hardware modification (nozzle size) may be made if a solution does not match the current burner specs

Full scale rotary kiln

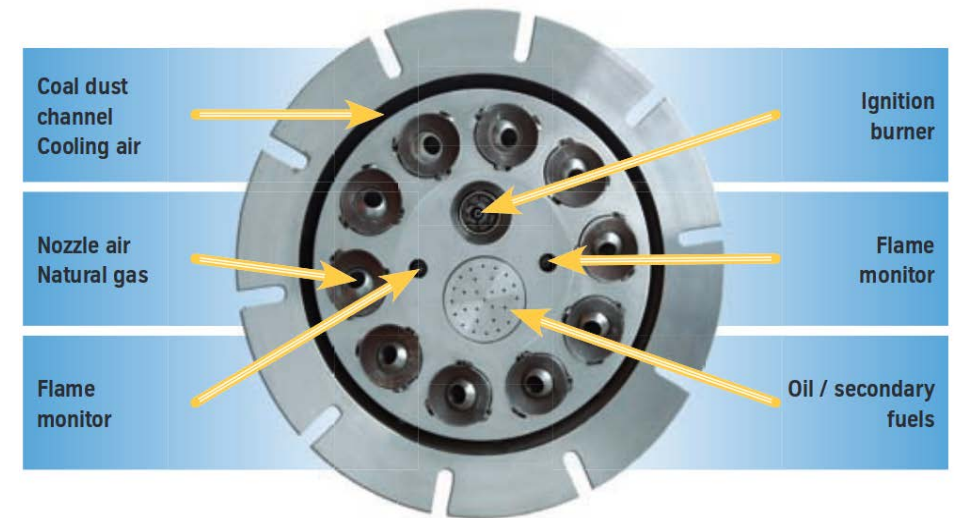
Burner

- Coal

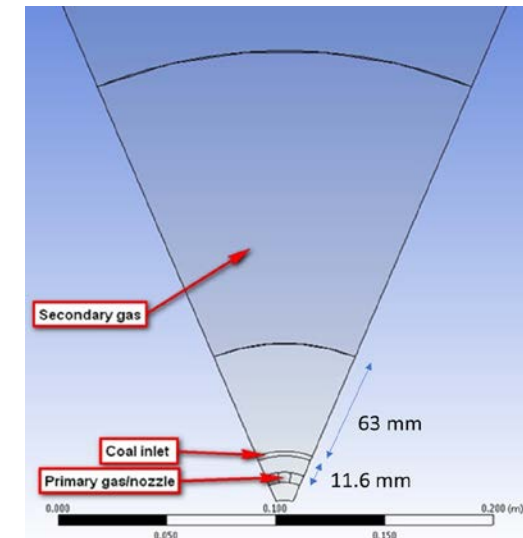
Property	Value
HCV (J/kg)	27,150
Volatiles (%)*	27
Fixed C (%)*	56
Ash (%)	16.5
Moisture (%)	0.5
Coal size (µm)*	100 - 400
Coal feed rate (kg/s)	1.47
Coal ultimate analysis (waf)	
C (%)	83.15
H (%)	4.82
O (%)	10.85
N (%)	0.58
S (%)	0.60

- Clinker dust

Property	Value
Density (kg/m ³)	1400
Cp (J/kg K)	Polynomial
Particle emissivity	0,9
Particle scattering factor	0,9
Inlet velocity (m/s)	Secondary flow
Particle diameter (µm)	150
Particle inlet temperature (K)	1073
Mass flow rate (kg/s)	0.28



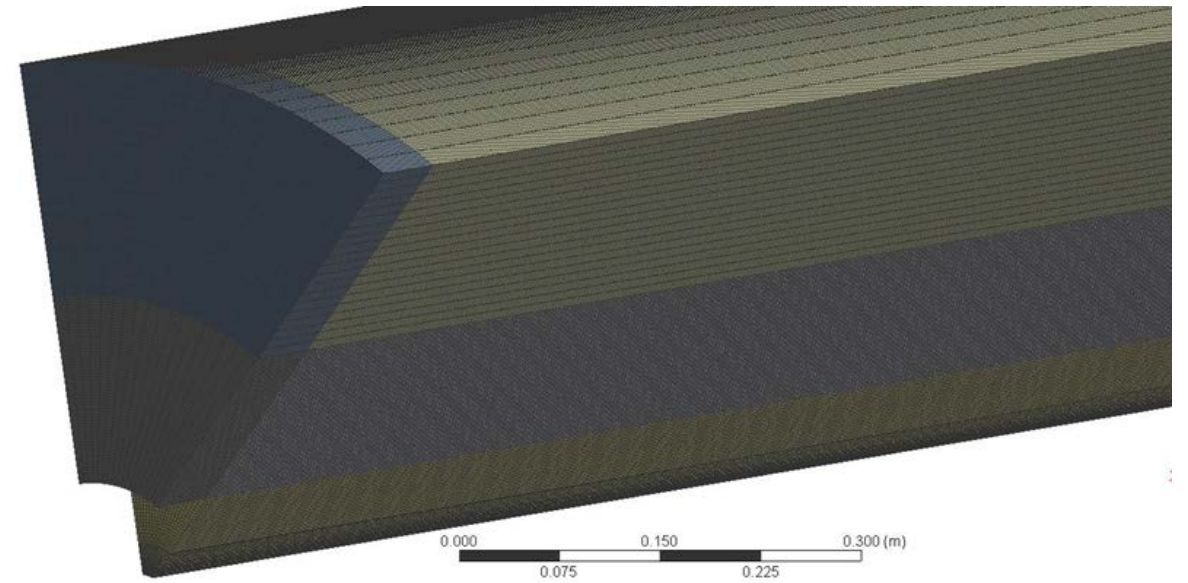
Source: ThyssenKrupp- POLFLAME



Full scale rotary kiln

CFD domain and setup

- Code: Fluent 17.2
- 3D domain 1/10th symmetry
- Mesh: of 1,648,500 cells
- Turbulence: k-omega SST
- Chemistry: Species transport, Finite rate/Eddy-Dissipation, 7-step reaction model
- Radiation model: Discrete Ordinates and WSGGM for gas radiation
- Geometry: 60 m long, \varnothing 3.76 m and \varnothing 3.56 m in the sintering zone
- Wall boundary: Forced temperature profile as in BAT profile
- Rotary kiln capacity: 3,000 t/d



Full scale rotary kiln

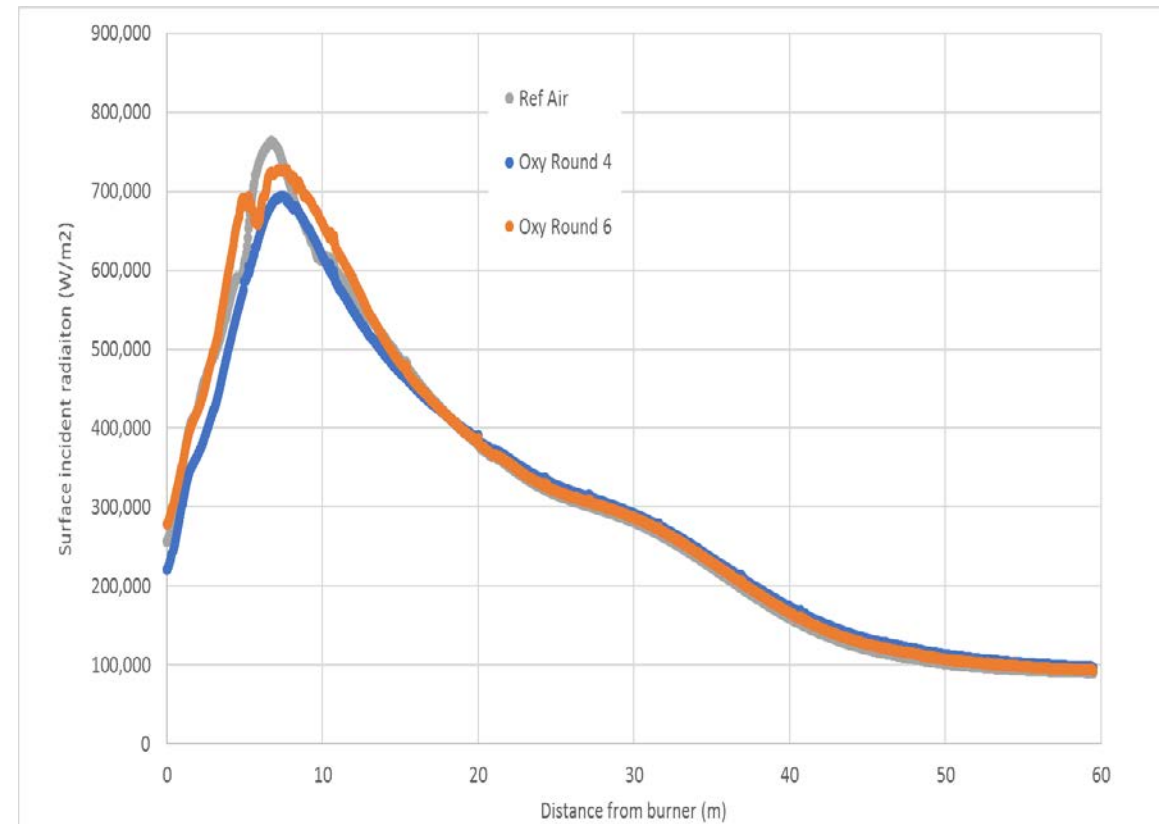
Inlet streams

- Constraint priority: retrofit (i.e. burner hardware)
- Total available gas in the primary stream is one third lower in the oxy-fuel case, compensated by higher swirl

Combustion cases:		AIR-Ref.	OXY-Round 3	OXY-Round 4	OXY-Round 6
Primary gas					
Volume flow rate	Nm ³ /h	5,100	4,068	4,500	4,500
Temperature	K	323	323	323	323
Composition					
N2 or CO2		N2	CO2	CO2	CO2
O2	% by vol.	21	60	60	60
N2 or CO2	% by vol.	79	40	40	40
Swirl degree	angle	20° tangential	40° tangential	30° tangential	30° tangential
Velocity	m/s	250	200	221	221
Carrier gas					
Volume flow rate	Nm ³ /h	4,040	1,600	1,600	1,050
Temperature	K	323	323	323	323
Composition					
N2 or CO2		N2	CO2	CO2	CO2
O2	% by vol.	21	30	30	18
N2 or CO2	% by vol.	79	70	70	82
Velocity	m/s	38.3	15.2	15.2	10.0
Fuel					
type		coal	coal	coal	coal
mass flow rate	kg/s	1,469	1,469	1,469	1,469
stoichiometric O2 mass	g_O2/g_fuel	2.070	2.070	2.070	2.070
Primary + Carrier					
Volume flow rate	Nm ³ /h	9,140	5,668	6,100	5,550
Temperature	K	323	323	323	323
Composition					
N2 or CO2		N2	CO2	CO2	CO2
O2	% by vol.	21.0	51.5	52.1	52.1
N2 or CO2	% by vol.	79.0	48.5	47.9	47.9
O2	Nm ³ /h	1,919	2,921	3,180	2,889
CO2 or N2	Nm ³ /h	7,221	2,747	2,920	2,661
available combustion O2	g_O2/g_fuel	0.518	0.789	0.859	0.780
Secondary gas					
Volume flow rate	Nm ³ /h	29,090	32,714	36,000	28,126
Temperature	K	1073	1073	1073	1273
Composition					
N2 or CO2		N2	CO2	CO2	CO2
O2	% by vol.	21.0	18.0	18.0	20.8
N2 or CO2	% by vol.	79.0	82.0	82.0	79.2
Velocity	m/s	3.7	4.2	4.6	4.3
Flue gas composition					
O2	% dry by vol.	1.1	2.8	4.6	3.0
N2	% dry by vol.	80.8	0.1	0.0	0.1
CO2	% dry by vol.	18.1	97.1	95.3	96.9
H2O	% wet by vol.	6.0	6.1	5.5	6.9

Clinker incident heat radiation

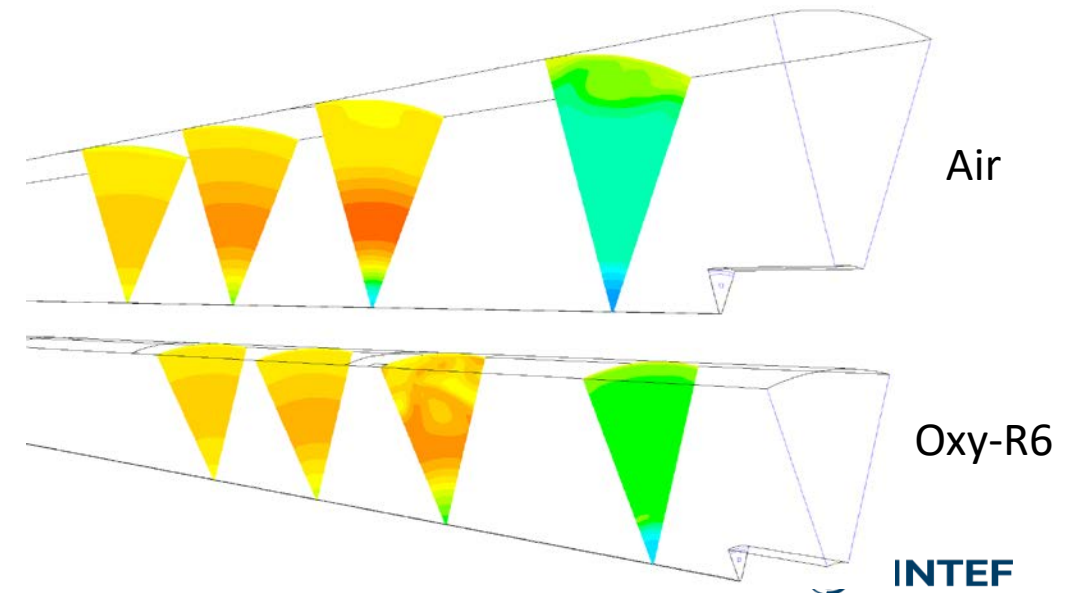
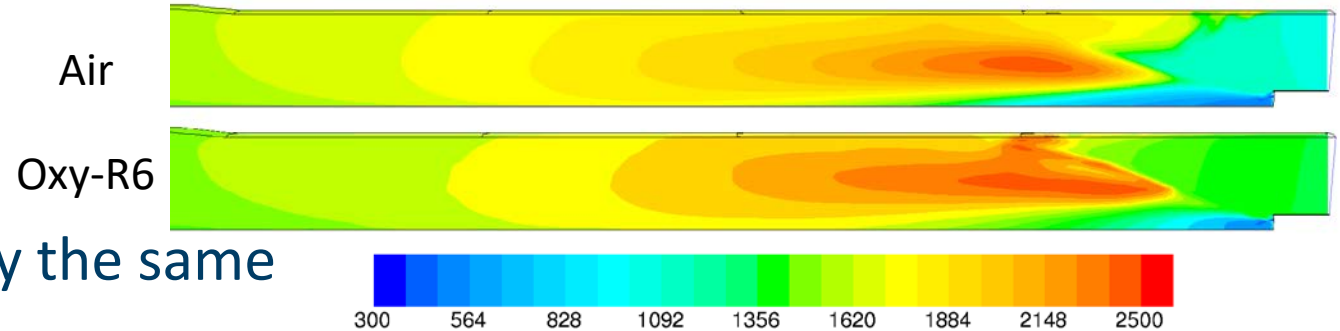
- Max deviation total heat: -0.8% and 2.1%
- Max deviation in near flame: -7.9 % and 2%
- Deviation O₂ flue gas +1.6 %-pt and 0
- Further matching peak radiation by:
 - enrich primary stream oxygen
 - increase swirl
 - decrease the carrier flow velocity
 - (Burner hardware modifications)



Flame field characteristics

Temperature

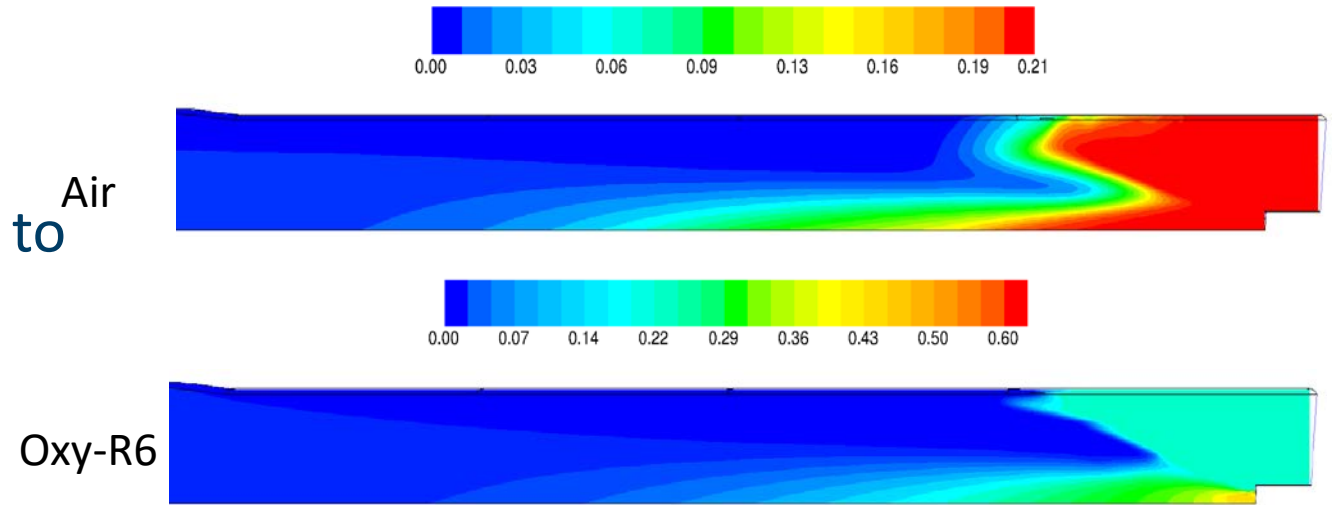
- Flame stabilization at approximately the same distance from the burner
- Flame front slightly more expanding in the oxy-fuel case
- Field homogeneity reached sooner in air
- Temperature paradox:
 - peak temperature in air 2360 K against 2239 K in oxy, although the primary gas $O_2 = 60\%$



Flame field characteristics

Oxygen

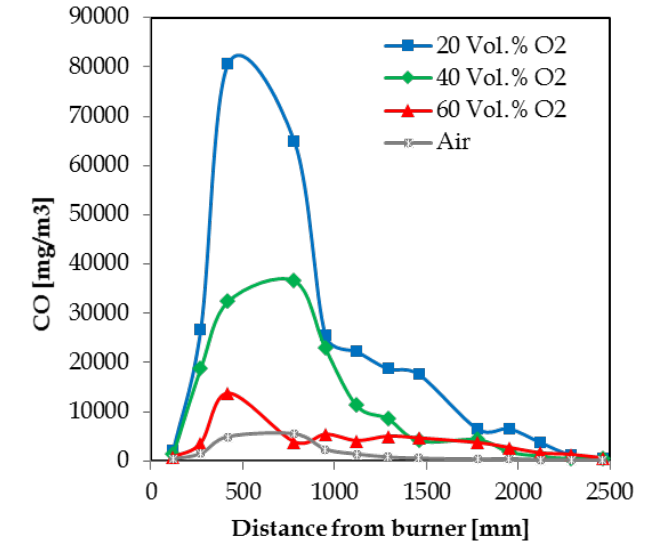
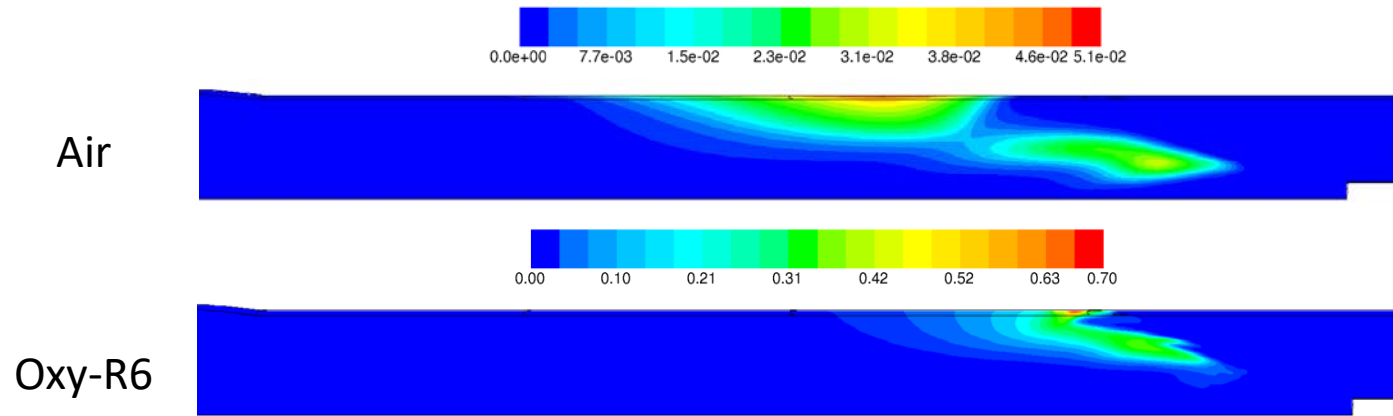
- Complex O₂ pattern in oxy-fuel due to varying inlet compositions of the three gaseous mixtures (primary, carrier, and secondary streams)



- oxygen concentration of 60 % only at the primary gas outlet plan
- At flame anchoring position the O₂ concentration is in fact ca. 25-29 % explaining the low temperature peak

Flame field characteristics

CO



- Heterogeneous reactions of char (3) used are strong producers of CO with CO₂ at large partial pressures (Boudouard reaction's net production reaction rate is two orders of magnitude larger in oxy-fuel)
- Also observed in the Univ. Stuttgart 500 kW pilot tests at varying oxygen concentration in the primary gas

Conclusions

- Study based on a defined reference BAT case and optimization methodology
- Most sensitive parameters to shape the required heat radiation profile:
 - Velocity at high speed nozzle
 - Swirl degree
- Least sensitive: carrier stream conditions (velocity and composition)
- Albeit similar heat radiation profile, the oxy-fuel flame characteristics in the kiln are different than in the reference air case
- Swirl angle at the burner (modulable in TKIS design) is a proper retrofitting tool when shifting from air to oxy-fuel mode



Acknowledgements

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