Multi-level hydrodynamic modelling of a 10MW TLP wind turbine

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Introduction

The design of floaters for offshore wind turbines relies on aero-hydro-servoelastic numerical models, which must be validated against tests. In these models there is a trade-off between accuracy and computational cost.

In the present work three numerical models are applied to a scaled version of the DTU 10MW wind turbine mounted on a Tension Leg Platform (TLP). The results for a set of load cases are benchmarked against test data. Finally, the advanced models are employed to enhance the performance of the simple model.

Loads acting on a TLP WT

Models and load cases

Model

Domain

DoF (total, floater) 2, 1

acceleration anac.

Wave kinematics

Wave forcing

Moorina

The three numerical models are

developed based on an experimental,

Froude-scaled 1:60 TLP wind turbine:

1st order

Morison

A set of load cases without wind is chosen including irregular and focused waves, and corresponding to rated operation and storm condition. The wave loads are integrated by stretching up to $z=\eta$. The

Linear

models are compared to the tests in terms of surge ξ_1 and nacelle fore-aft

calibrated using the Flex5 models.

The calibration is done by comparison of the surge decay response. The nacelle damping in the *Matlab* model is further

Frequency Time

Matlab Flex5-1st Flex5-2nd

28.6

1st order

Morison

Nonlinear

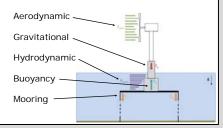
Time

28.6

2nd order

Morison

Nonlinear



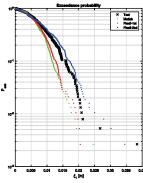
Results

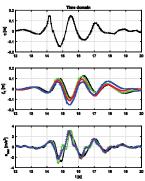
Response to irregular waves Full-size: $H_s = 4.68$ m, $T_p = 7.36$ s

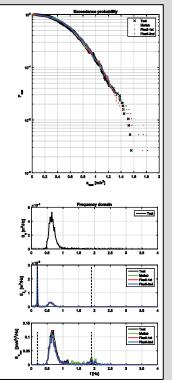
The *Matlab* model underpredicts the surge motion and predicts well the nacelle acceleration. The **J** first-order *Flex5* model is similar to the *Matlab* model in surge, while the second-order *Flex5* model shows larger surge response. The nacelle acceleration is well predicted by both *Flex5* models.



Surge motion is influenced by its natural frequency (0.19 Hz). The second-order wave kinematics introduce subharmonic forcing at the surge frequency, perhaps due to the difference between second-order theory and test conditions. The *Matlab* and first-order *Flex5* models agree better with the test in surge. Nacelle acceleration is well predicted by all models.







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Conclusions

The *Matlab* model underpredicts surge in some cases, but often matches nacelle acceleration.

The second-order wave kinematics did not affect the nacelle acceleration significantly (due to large inertia of the TLP wind turbine). However, it induces an important subharmonic forcing at surge frequency (which leads to overprediction).

The *Matlab* model was enhanced by compensating the absent pitch motion with tower flexibility. After enhancement, its performance is comparable to that of more advanced models.

Further information

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